

Numerical Optimization of Electroactive Actuator Position for Optical Mirror Applications



CENTRE DE RECHERCHE ASTROPHYSIQUE DE LYON

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Project #ANR-18-CE42-0007-01 (Live-Mirror project)

Numerical Optimization of Electroactive Actuator Position for Optical Mirror Applications

Outline

- I. Background – Objectives
- II. Modelling and Numerical Model
 - a) Curvature Computation
 - b) Mechanical Problem
 - c) Optimization Procedure
- III. Main Results
- IV. Conclusions – Perspectives

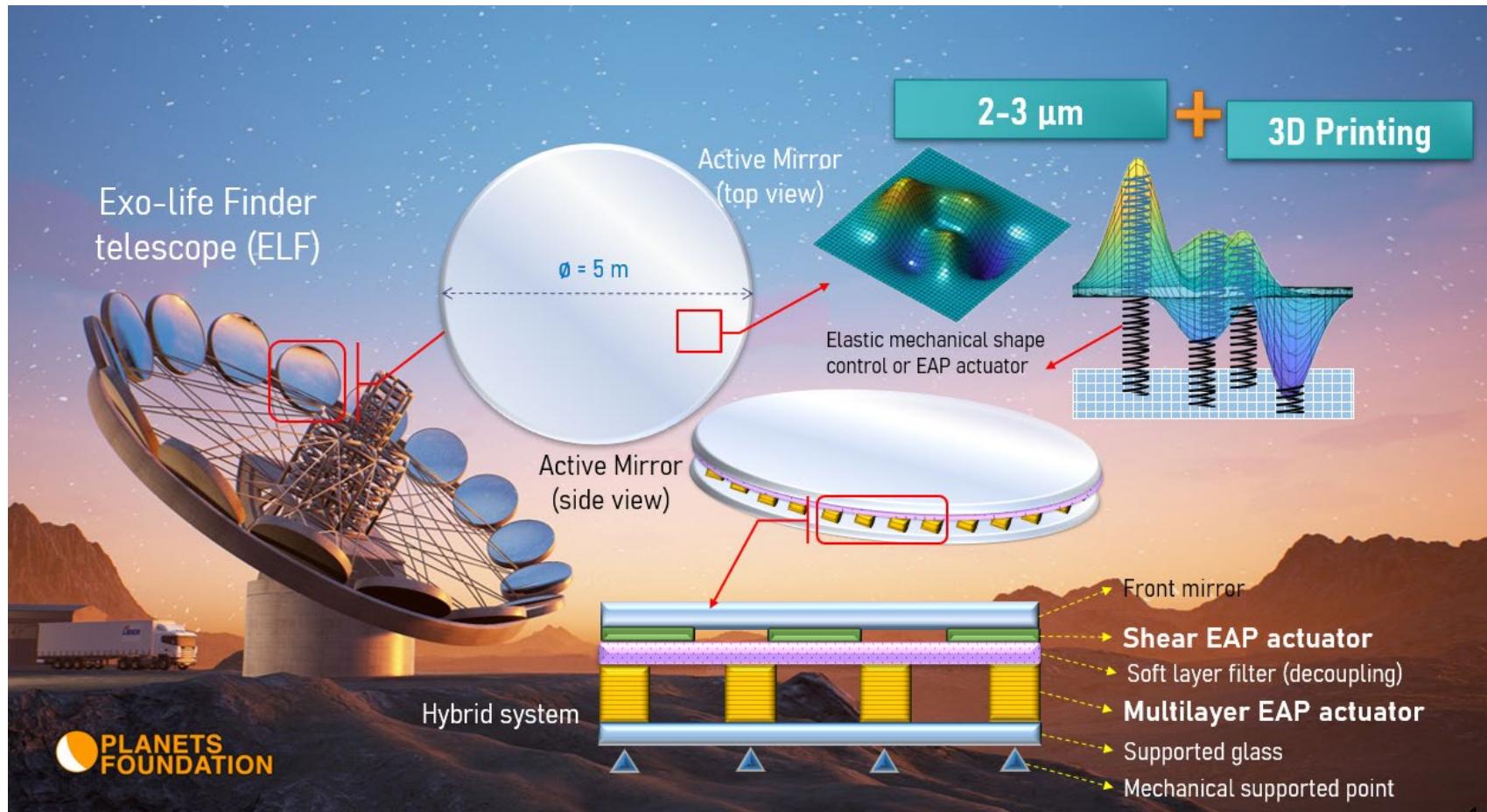
Before starting, who we are... www.simtecsolution.fr

SIMTEC : Fundamentals

- French Numerical modelling consultancy
- Leader in France of the COMSOL Certified Consultants, key partner worldwide
- 7 members Eng.D. + Ph.D.
- Main partners:
 - big international companies
 - laboratories
- Involved in the Research projects like EU FP (SHARK, SisAl)/ PhD supervision

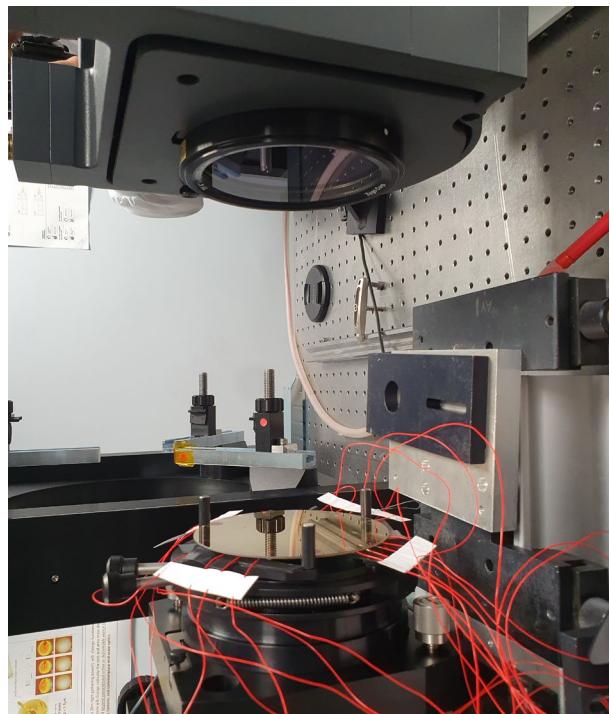


I. Background – Objectives



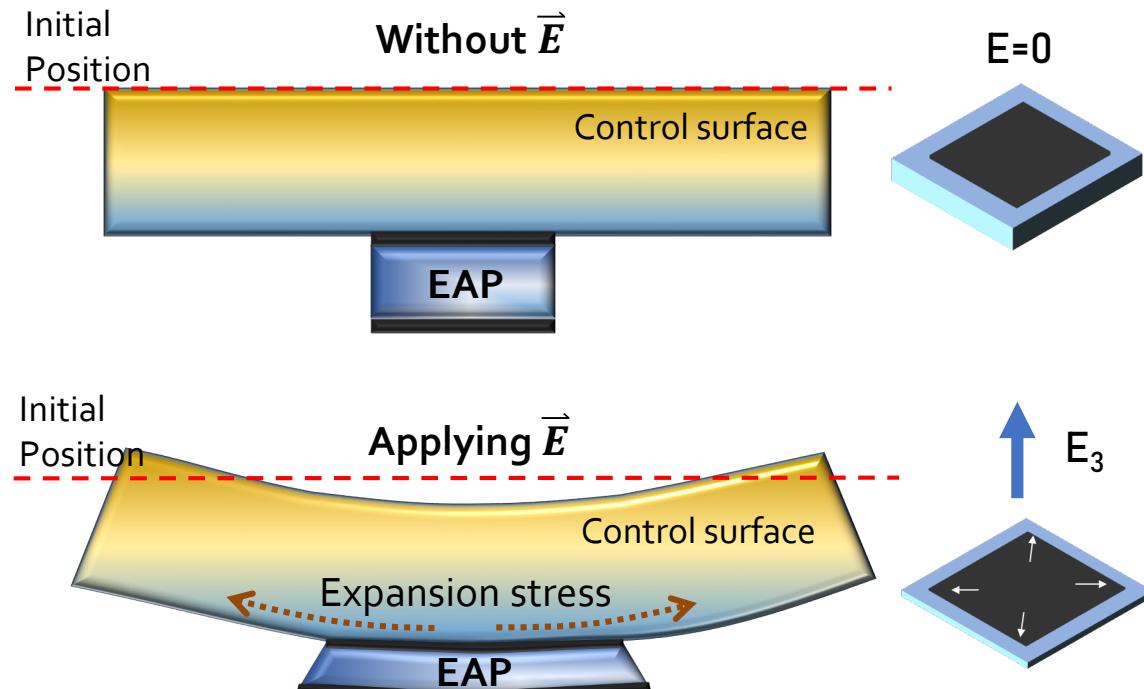
EAP = Electro Active Polymer

I. Background – Objectives



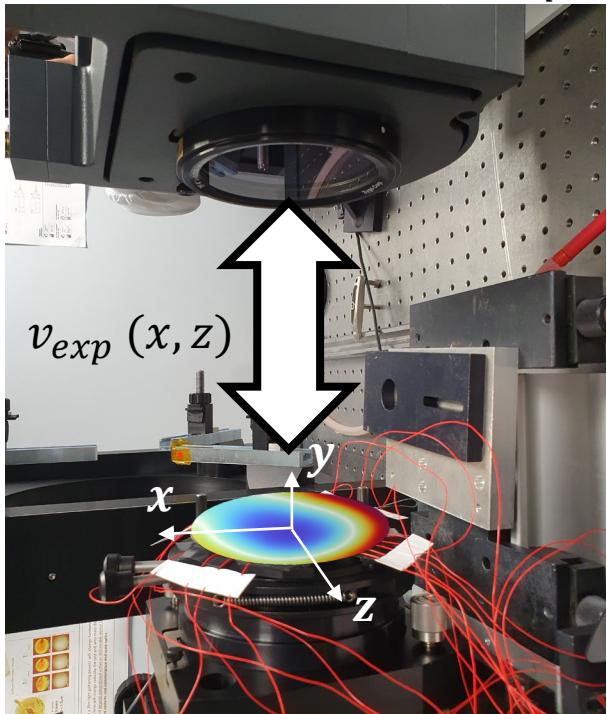
ZYGO measurements

Mirror surface deformed by
an active EAP actuator



I. Background – Objectives

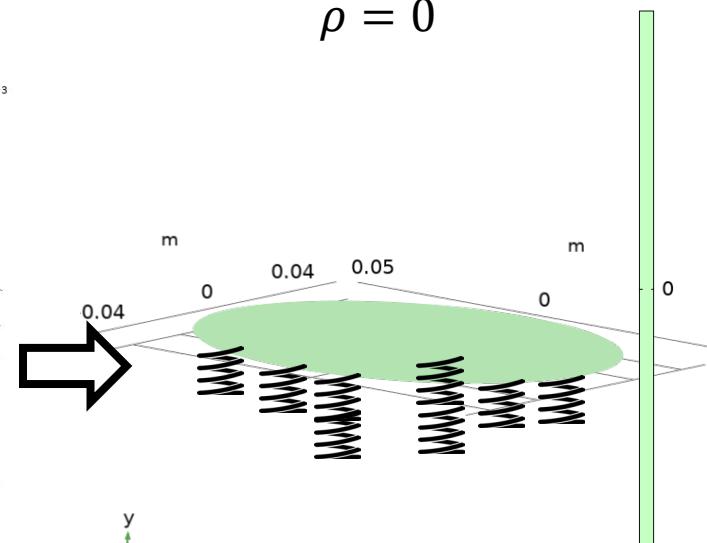
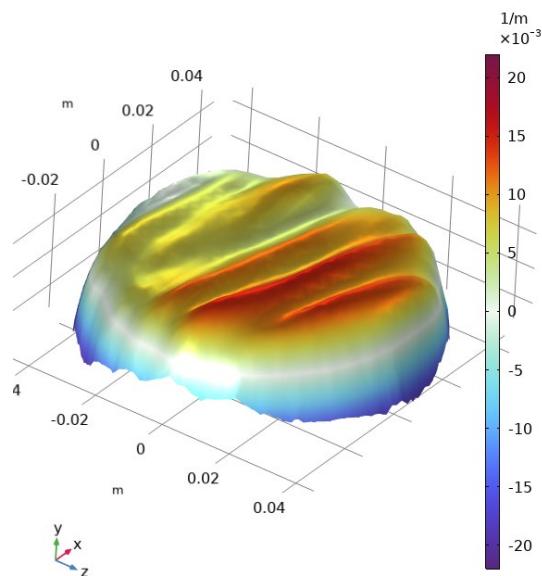
Imported data in Comsol : $v_{exp} (x, z)$



Real Local Curvature

$$\rho = \frac{\partial^2 v_{exp}}{\partial x^2} + \frac{\partial^2 v_{exp}}{\partial z^2}$$

$$\rho = 0$$

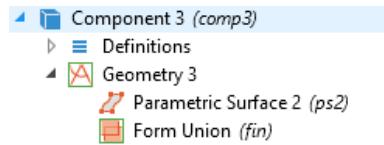


Objective :

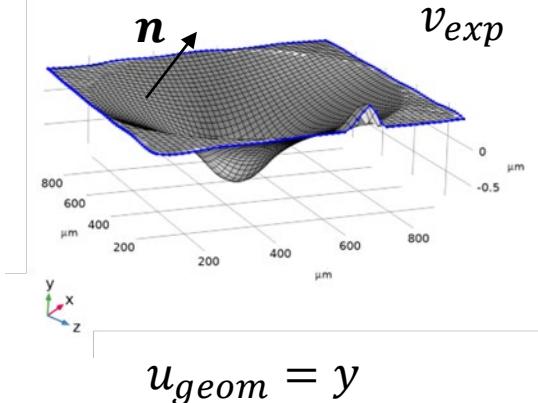
Find an optimized EAP layout that minimize the local curvature $\rho = \frac{\partial^2 v}{\partial x^2} + \frac{\partial^2 v}{\partial z^2}$

II. Modelling and Numerical Model

1st step: Curvature Computation



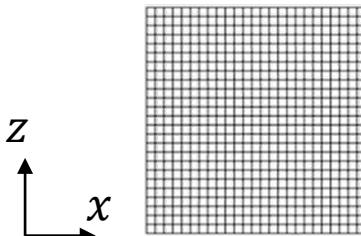
Parametric Curved Surface



$$\rho_{geom} = \Delta_T u = (I - \mathbf{n}\mathbf{n}^T)\Delta u_{geom}$$

2 methods tested in COMSOL

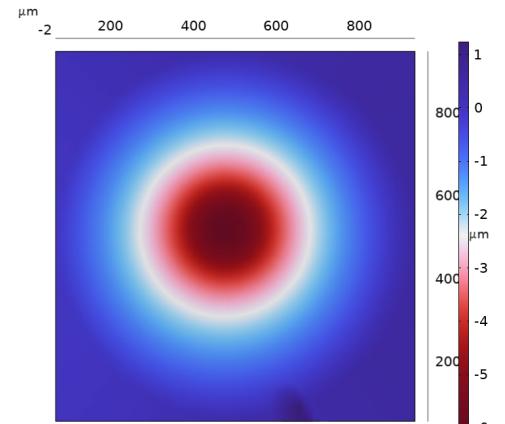
Mapped Geometry



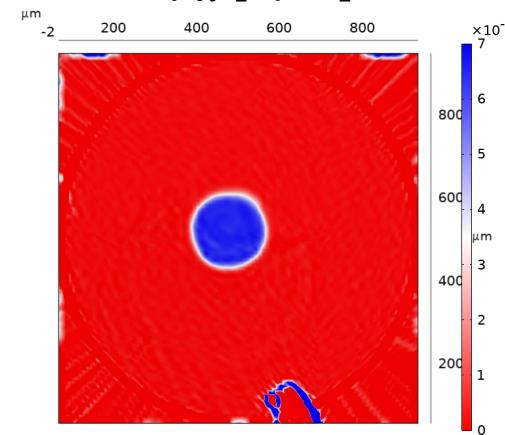
$$\lambda \Delta u + u = v_{exp}$$

$$\rho_\lambda = \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial z^2}$$

$$v_{exp}(x, z) [\mu m]$$



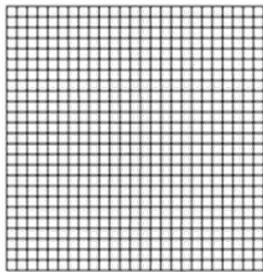
$$\rho_\lambda [1/m]$$



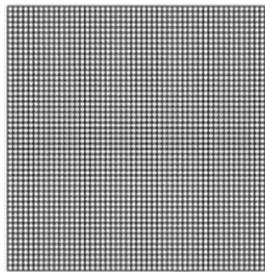
II. Modelling and Numerical Model

1st step: Curvature Computation – Mesh Validation

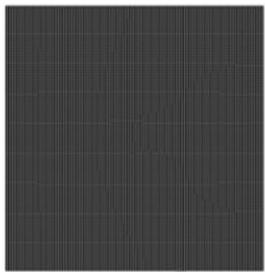
$n_{element} = 25$



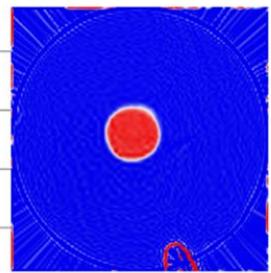
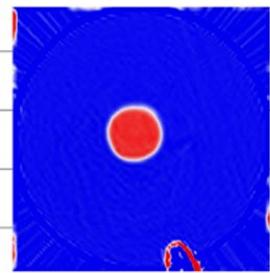
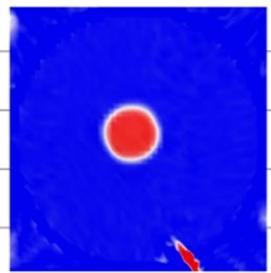
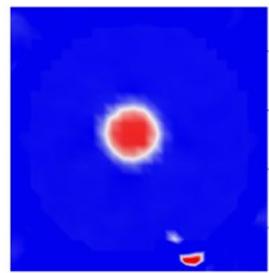
$n_{element} = 50$



$n_{element} = 100$

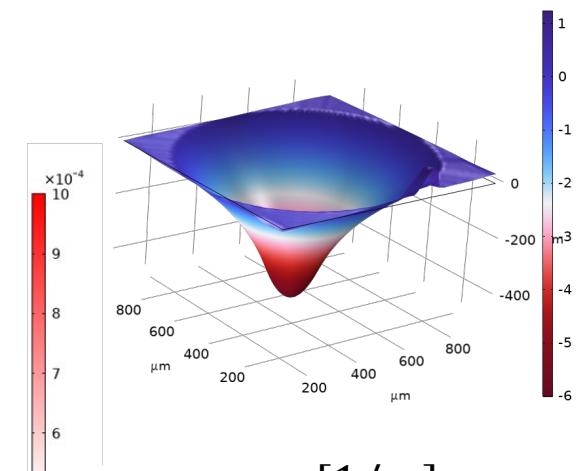


$n_{element} = 200$

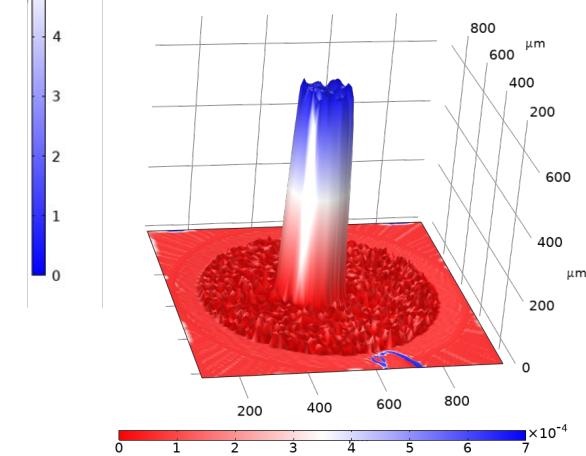


- Mesh convergence OK

$v_{exp}(x, z) [\mu\text{m}]$



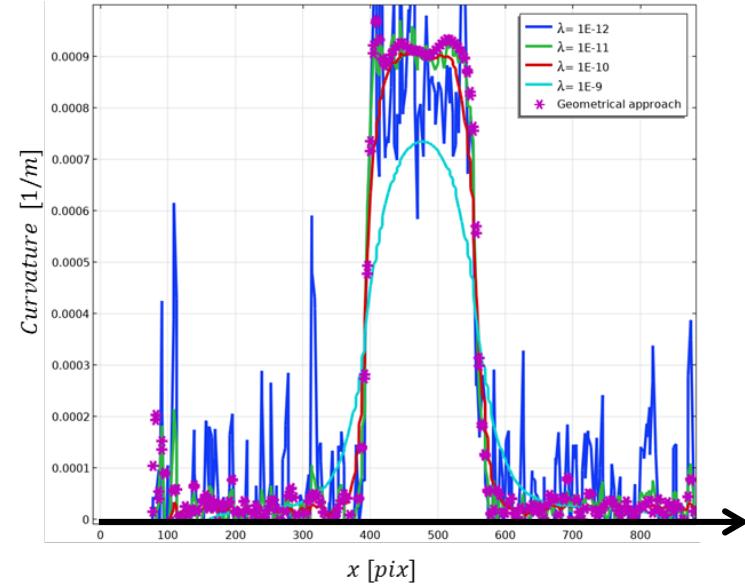
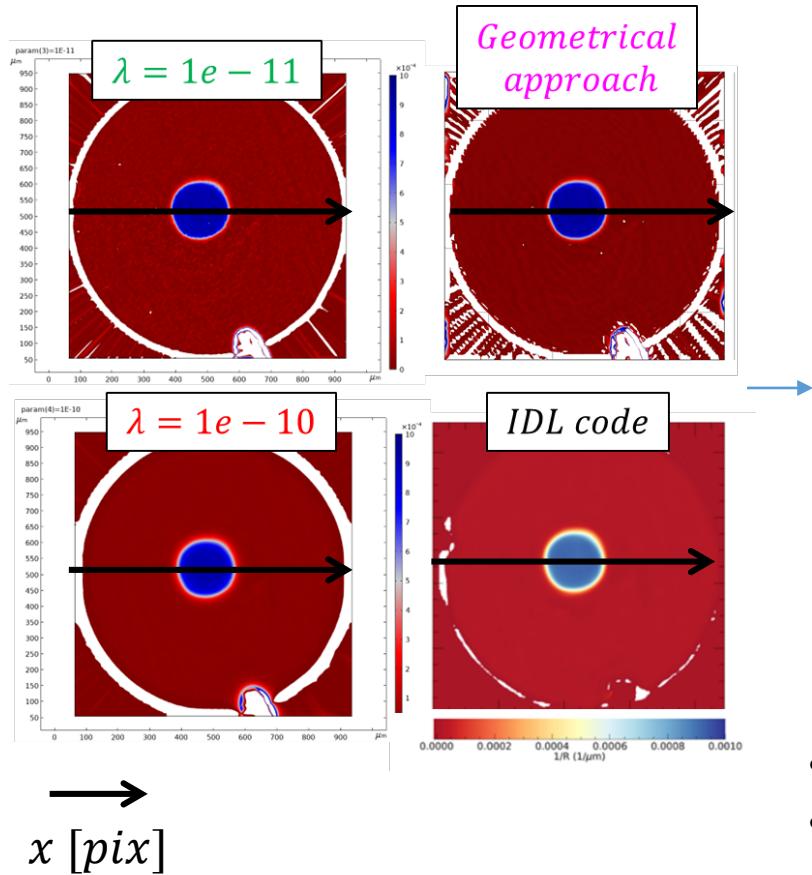
$\rho_\lambda [1/\text{m}]$



II. Modelling and Numerical Model

1st step: Curvature Computation – Numerical Validation

$$\lambda \Delta u + u = v_{exp}$$



- Validation of both approaches
- Choice of the parameter of tuning $\lambda = 1e - 11$

II. Modelling and Numerical Model

2nd step: Mechanical Problem – Equations & Boundary Conditions

Solid Mechanics

$$\nabla \cdot S = 0$$

$$\varepsilon_{el} = \frac{1}{2}(\nabla u + \nabla u^T)$$

ε_0 : Vacuum permittivity
 ε_r : Reference permittivity
 e : Coupling matrix
 C : Elasticity matrix

Electrostatics

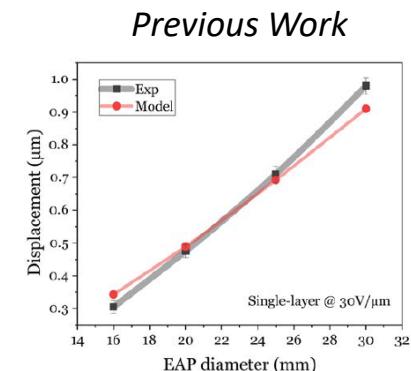
$$\nabla \cdot D = 0$$

$$E = -\nabla V$$

$$D = e : \varepsilon_{el} + \varepsilon_0 \varepsilon_r E$$

$$S = C : \varepsilon_{el} - e^T E$$

$$\Rightarrow S_{yy} \sim \varepsilon_0 \varepsilon_r E_y^2 \sim \varepsilon_0 \varepsilon_r \left(\frac{\Delta V}{Thickness} \right)^2$$



K. Thetraphphi, *Development of electroactive polymer actuators for next generation mirror : Live-Mirror*, PhD Thesis, 2021.

- ElectroMechanical Model validated with experimental results

II. Modelling and Numerical Model

2nd step: Mechanical Problem – Equations & Boundary Conditions

Solid Mechanics

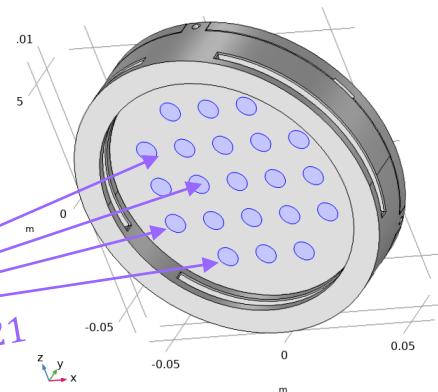
$$\nabla \cdot S = 0$$

$$\varepsilon_{el} = \frac{1}{2} (\nabla u + \nabla u^T)$$

- $u|_{R=R_{disk}} = 0$

- $S \cdot n = F_i$

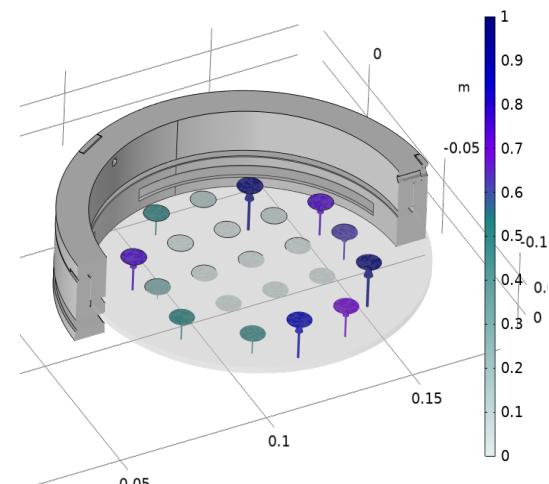
$i = 1 \dots 21$



- Mechanical problem solved

$$F_i = K_i * p_{piezo}$$

$$K_i$$



II. Modelling and Numerical Model

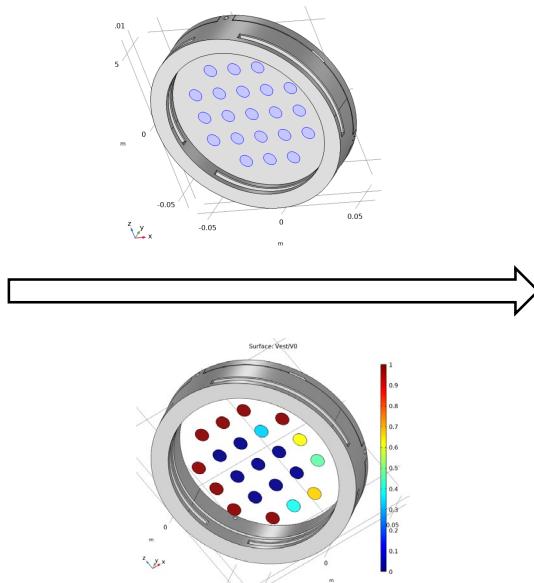
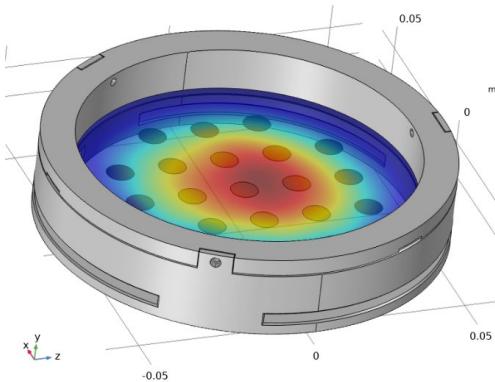
3rd step: Optimization Procedure

Optimization procedure to find K_{f_i} that minimizes :

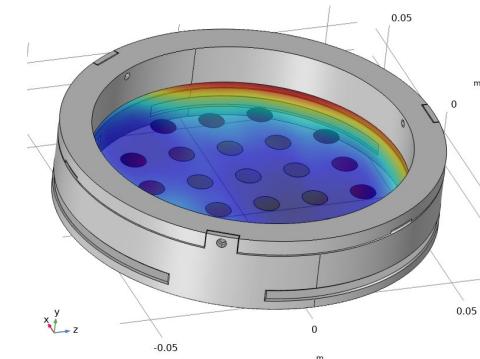
$$J = \iint (\rho_{exp} - \rho(K_{f_i}))^2$$

SNOPT Algorithm

Initial Curvature

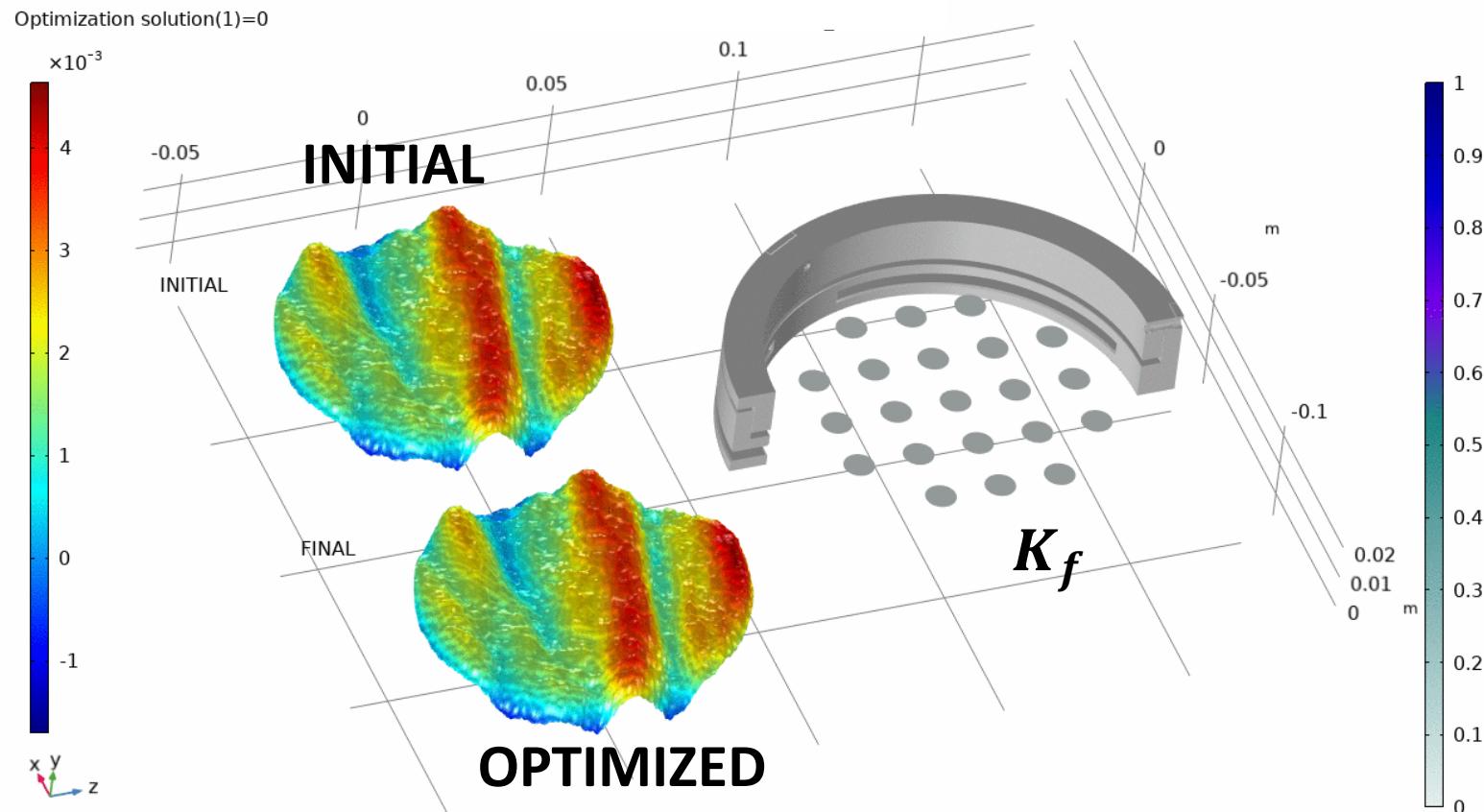


Final Curvature



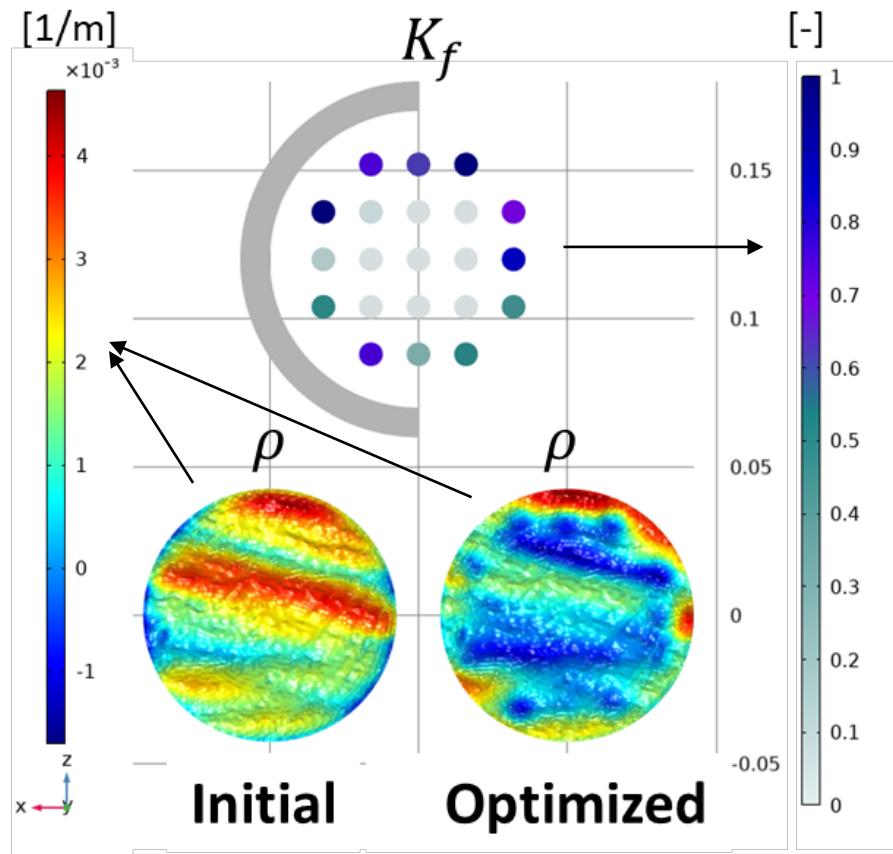
III. Main Results

Optimization Procedure



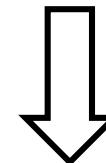
III. Main Results

Optimized Results



On this example:

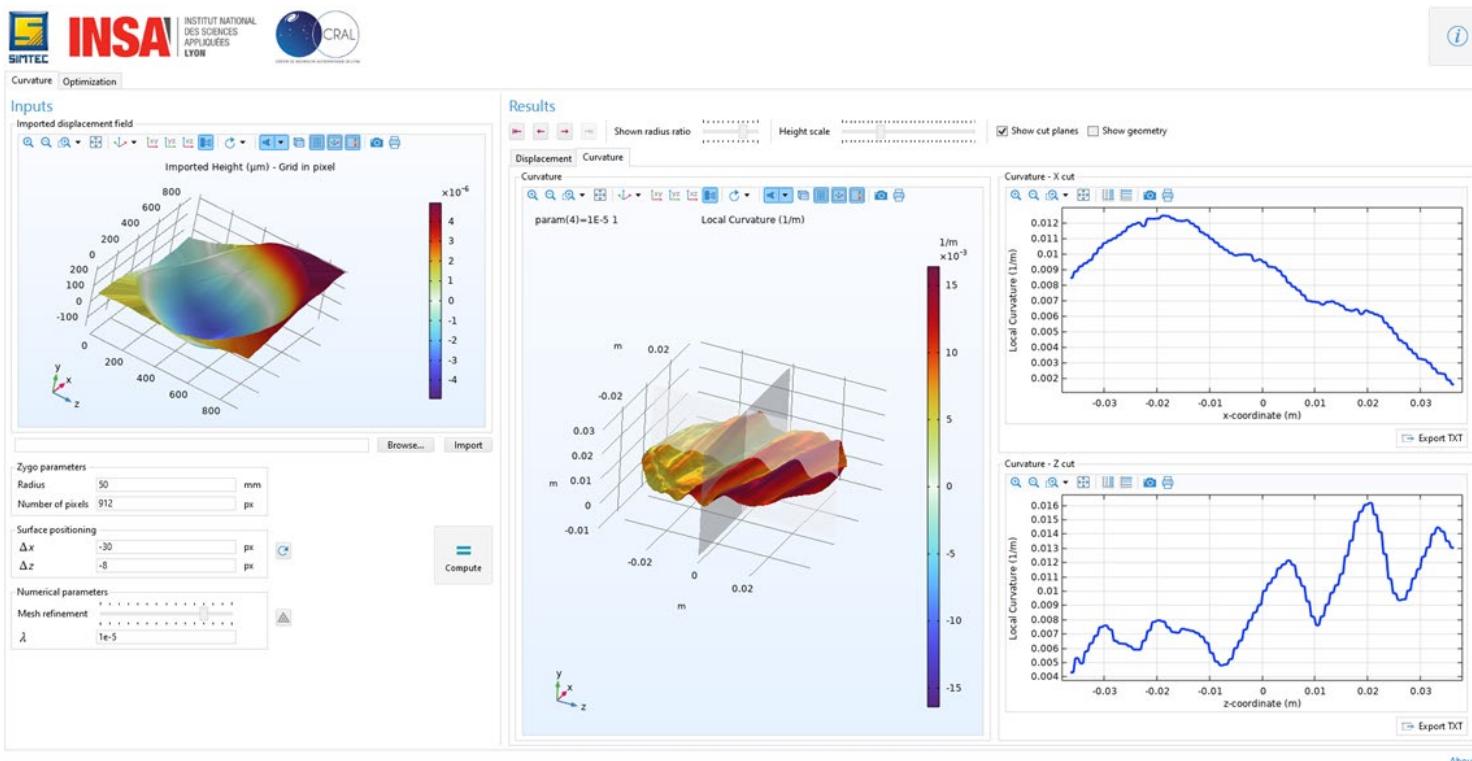
$$Gain = \frac{RMS(\rho_{initial})}{RMS(\rho_{optimized})} > 300\%$$



Validation of the numerical approach

III. Main Results

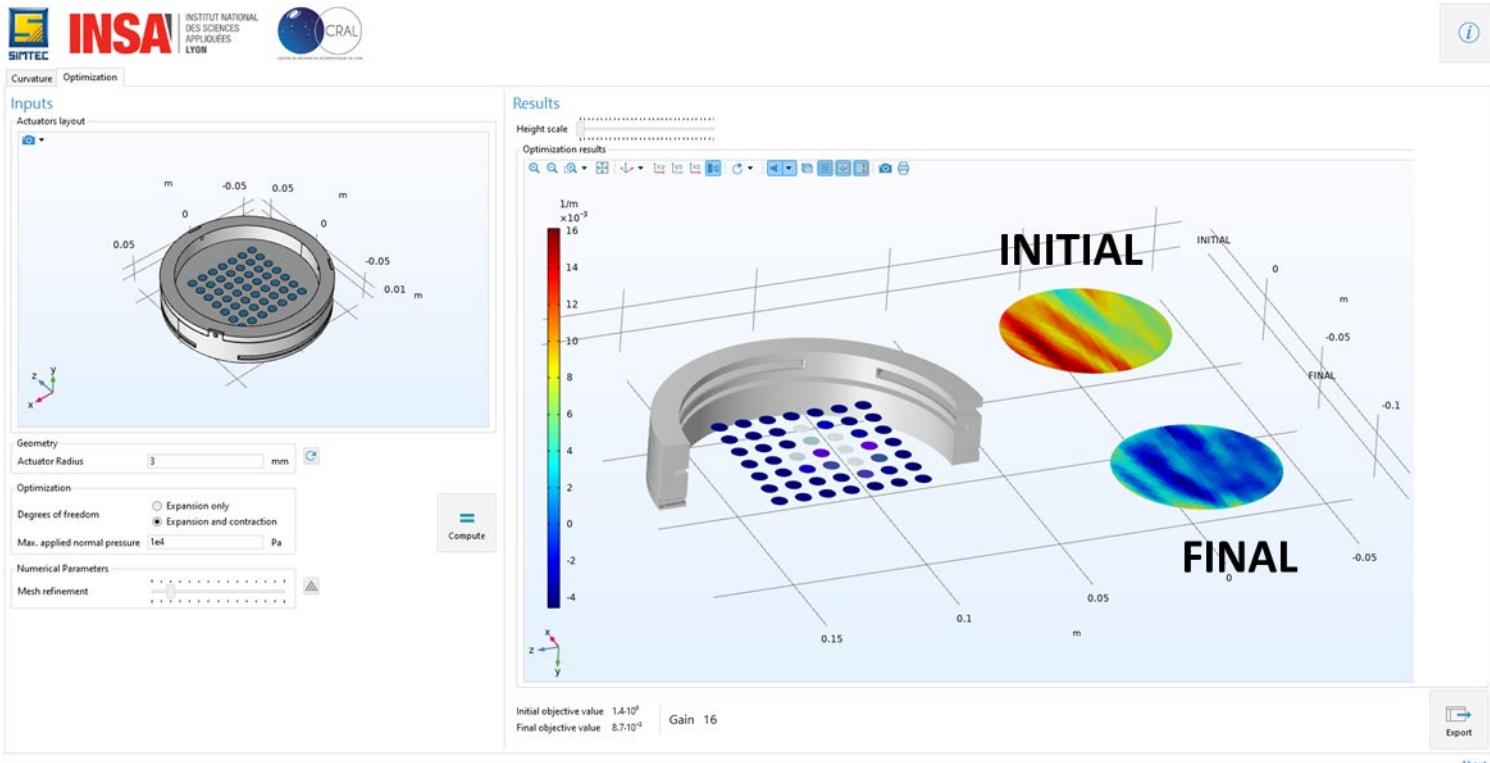
Application



- Import of experimental data & Pre-processing
- Local Curvature Computation and Post-processing

III. Main Results

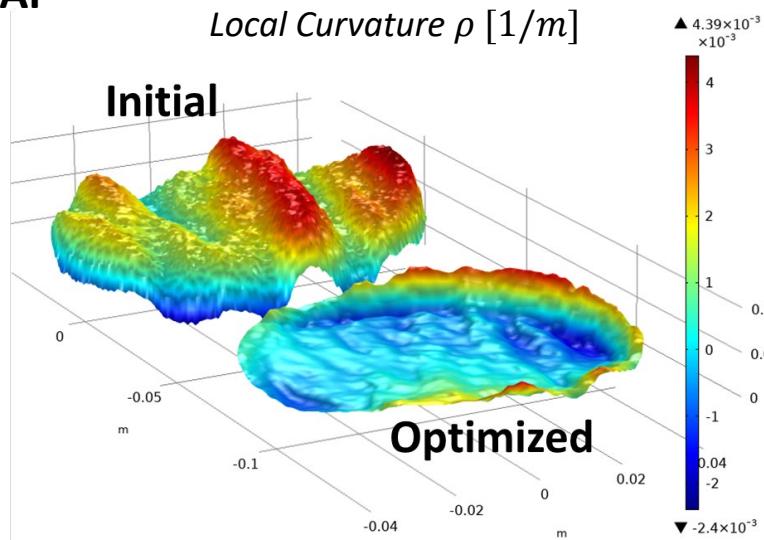
Application



- Parametrization of the EAP Geometry Pattern
- Full Parametrized Optimization Procedure
- Export of resulting K_{f_i} for each EAP

IV. Conclusions - Perspectives

- Development of an **optimization procedure** to predict the **optimum force** (\sim **electrical potential**) to be applied to each actuator,
- Parametrization of the optimization procedure to study **the influence of the geometry pattern**
- **Validation of the curvature computation and optimization loop with a specified pattern of EAP**



To finish...

Thank you!

Q&A?

Our question: What about a coffee
to discuss your topic? ☺



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0007-01 (Live-Mirror
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