

FEM ANALYSIS OF CONTAMINATE TRANSPORT IN LOAMY DESERT SOIL

Presented By,

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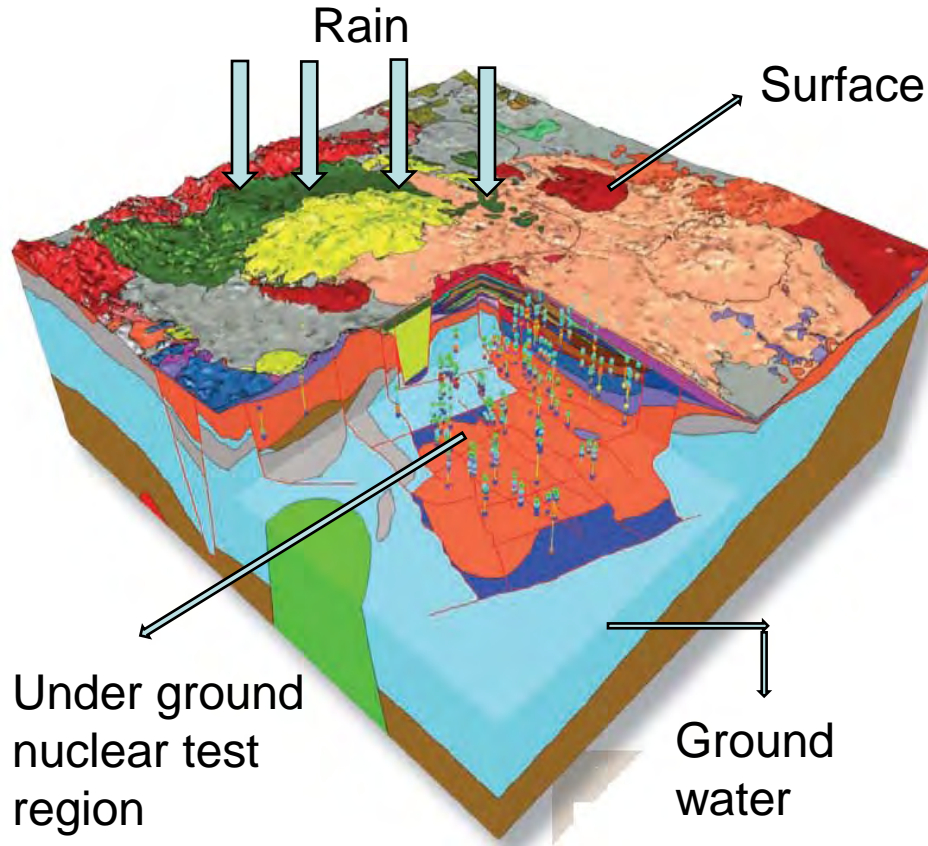
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INTRODUCTION



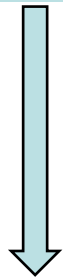
- From 1951 to 1992, 828 underground nuclear tests were conducted at the Nevada Test Site.
- Most of these tests were conducted hundreds of feet above the groundwater table
- One third of these were near the water table
- Rain water can mobilize the radionuclide ions present in the soil and can contaminate the ground water

Figure 1: Three Dimensional representation of how water and contaminates flow through soil in Nevada test site.
Ref: www.nv.doe.gov

MODEL DESCRIPTION

- Advective Dispersion Reaction Model:

$$\frac{\partial C}{\partial t} = -v \frac{\partial C}{\partial x} + D_L \frac{\partial^2 C}{\partial^2 x} - \frac{\rho(1-\varepsilon)}{\varepsilon} \frac{\partial q}{\partial t}$$



Rate of solute change in liquid phase



Convective flux term



Solute Transport by dispersion



Rate of solute adsorption on soil phase

Equilibrium between the solid and liquid phase

ρ Density of soil, kg/cm^3

ε Porosity of the bed

D_L Dispersion Coefficient, m^2/min

v Velocity, m/min

$$\frac{\partial q}{\partial t} = \frac{\partial q}{\partial C} \left[\frac{\partial C}{\partial t} \right]$$

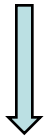
Ref: Applied contaminate transport modeling, Second edition , Chunmiao Zheng, Gordon D. Bennett

ADSORPTION ISOTHERM

- Langmuir Adsorption Isotherm

$$q = \frac{q_0 CK}{1 + CK}$$

q_0 Monolayer capacity, mol/kg
 K Adsorption Coefficient, m³/mol



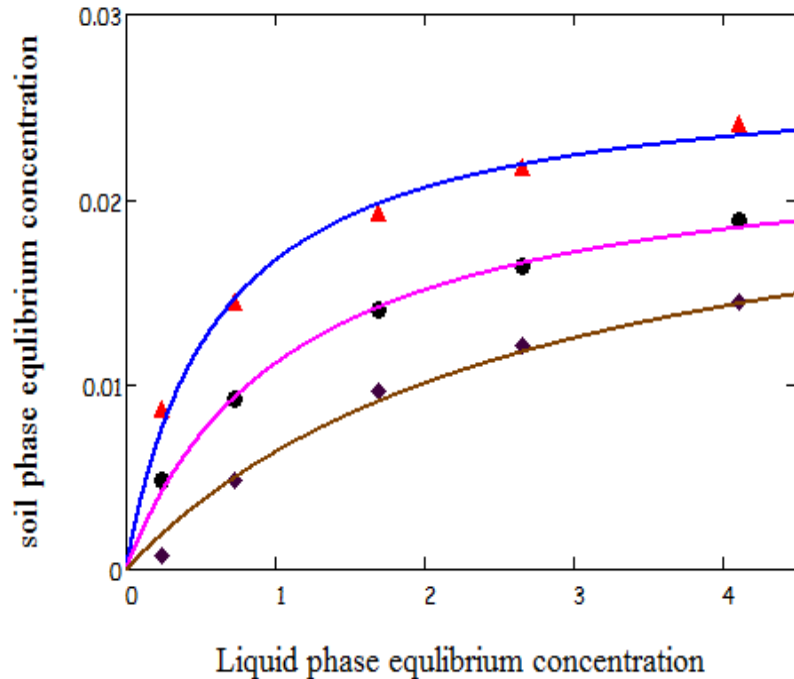
$$\frac{\partial q}{\partial C} = \frac{q_0 K}{(1 + KC)^2}$$

First derivative of the Langmuir equation

$$\frac{\partial C}{\partial t} \left[1 + \frac{\rho(1 - \varepsilon)}{\varepsilon} \frac{q_0 K}{(1 + KC)^2} \right] = -v \frac{\partial C}{\partial x} + D_L \frac{\partial^2 C}{\partial x^2}$$

Final PDE by combining equilibrium and Langmuir expression

Batch Adsorption Results



- ▲▲▲ Experimental data At 25 C
- Langmuir fit at 25 C
- Experimental data At 35 C
- Langmuir fit at 35 C
- ◆◆◆ Experimental data At 45 C
- Langmuir fit at 45 C

T	q_0 , mol/kg	K , m ³ /mol	RMSE
25°C	0.027	1.633	0.00060
35°C	0.023	0.906	0.00069
45°C	0.022	0.357	0.00069

T *Temperature, °C*

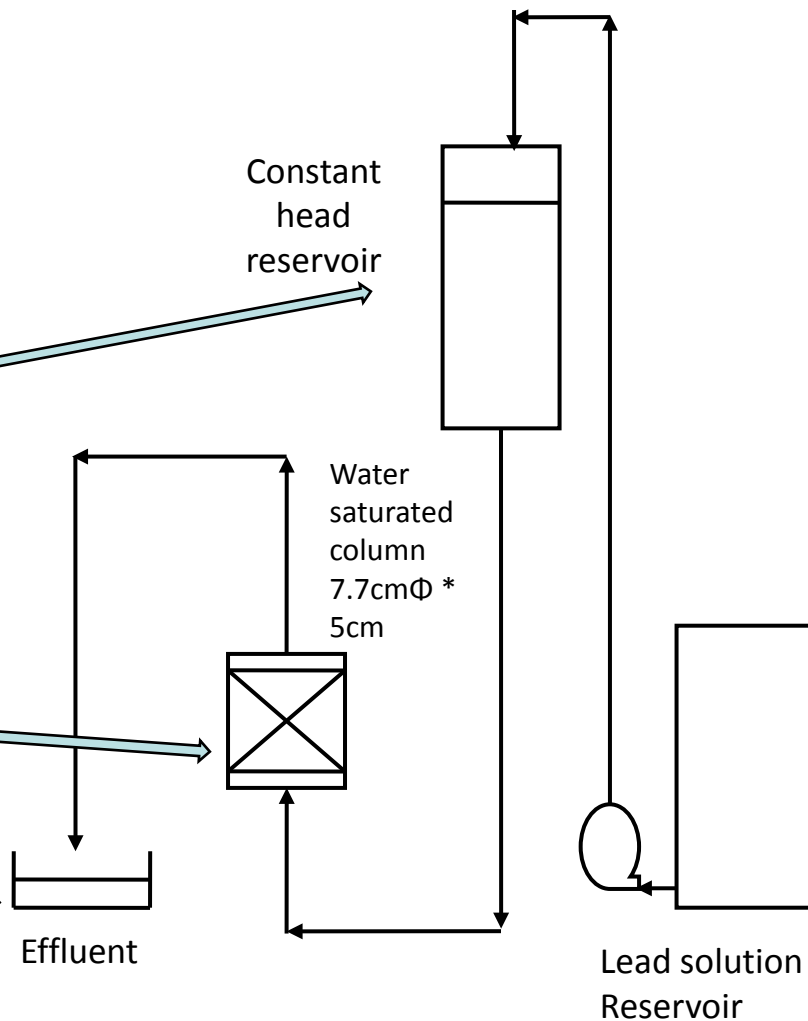
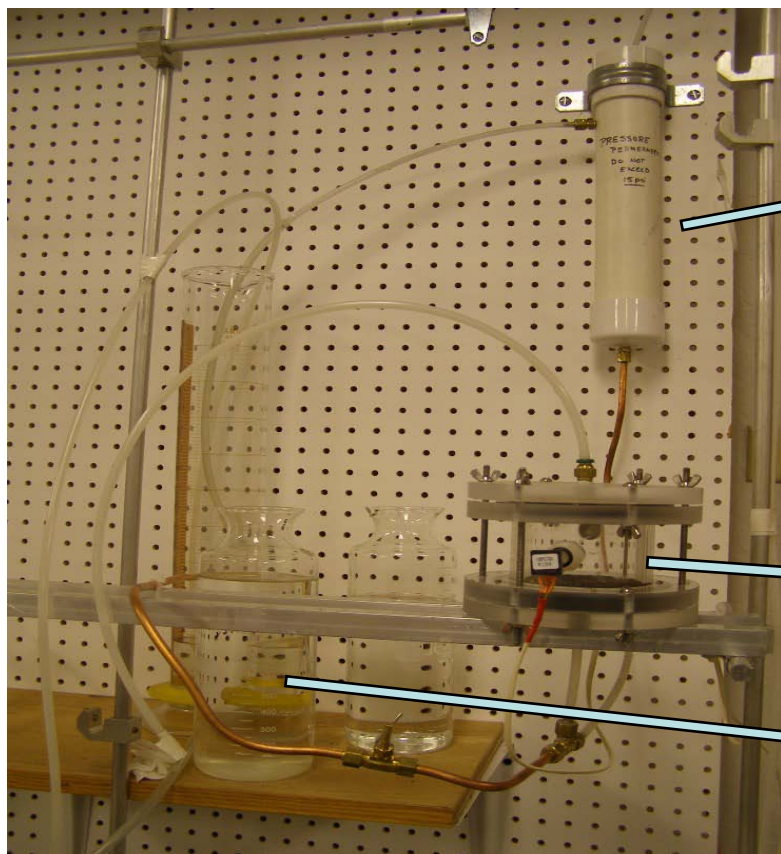
q_0 *Monolayer capacity, mol/kg*

K *Adsorption Coefficient, m³/mol*

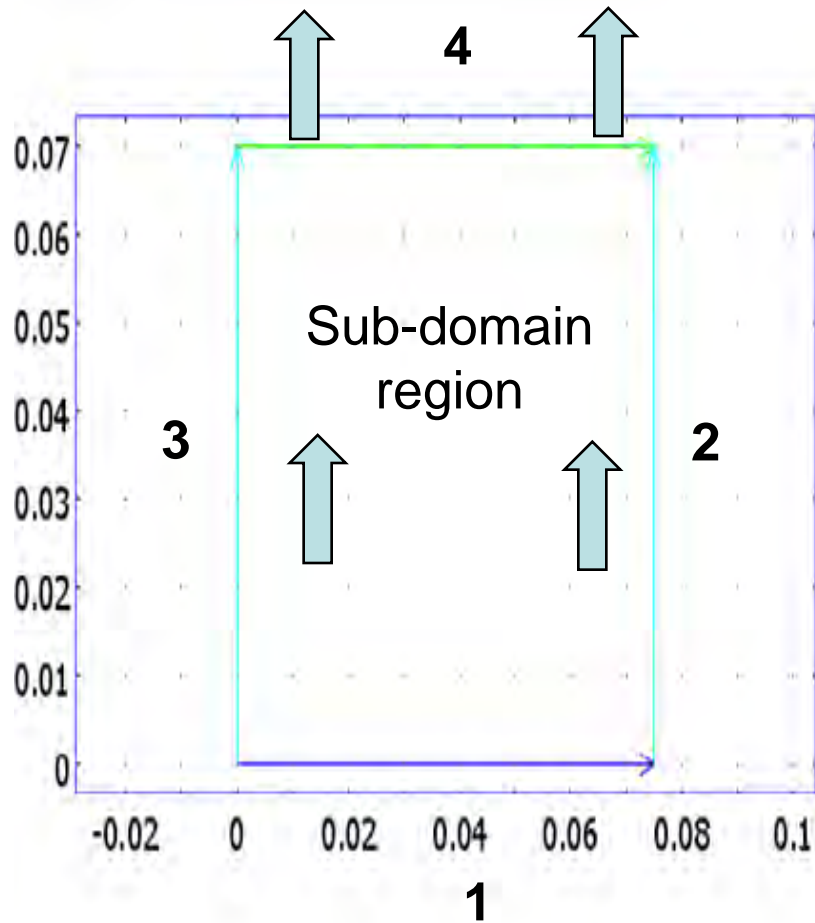
RMSE *Root mean square error*

Experiments and Model Validation

Column Experiments:



Boundary and Initial Conditions



Boundaries	Boundary conditions ($t \geq 0$)
1	$C = C_0$
2	Insulation (Flux = 0) $\frac{\partial C}{\partial t} = 0$
3	Insulation (Flux = 0) $\frac{\partial C}{\partial t} = 0$
4	Convective Flux
Sub-domain region	($t=0$) $C=0$

MODEL PARAMETERS

C_0	0.314 mol/m^3
K	$1.633, 0.906, 0.357 \text{ m}^3/\text{mol}$
ε	0.45
ρ	1500 kg/m^3
q_0	$0.027, 0.023, 0.022 \text{ mol/kg}$
v	$1.5 \cdot 10^{-5} \text{ m/s}$
D_L	$8.7 \cdot 10^{-7} \text{ m}^2/\text{s}$
δt	$1 + \frac{(1 - \varepsilon)}{\varepsilon} \frac{q_0 K}{(1 + KC)^2}$

Darcy's Law to determine velocity of adsorbate solution

$$Q = \frac{KA(h_2 - h_1)}{L}$$

$$Q = Av$$

K Hydrodynamic conductivity, m/s

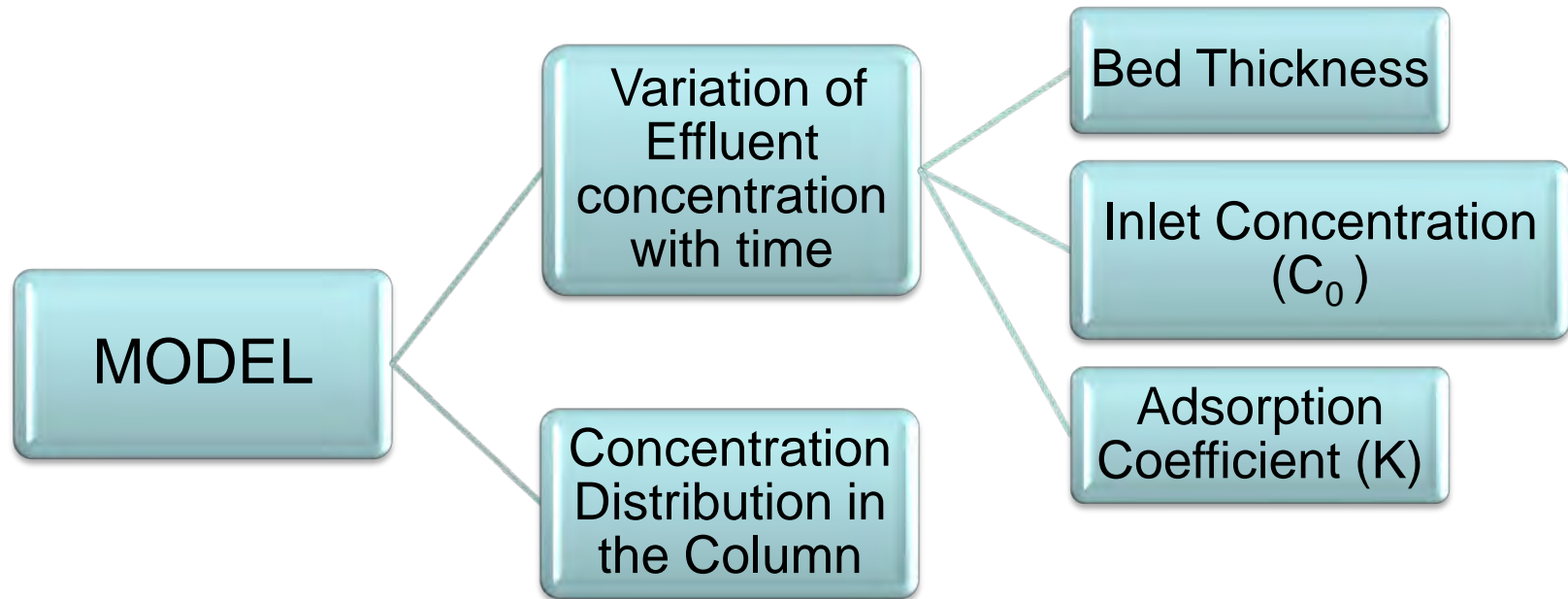
A Cross sectional area, m²

L Length of the soil packing in the column, m

Q Volumetric flow rate, m³/min

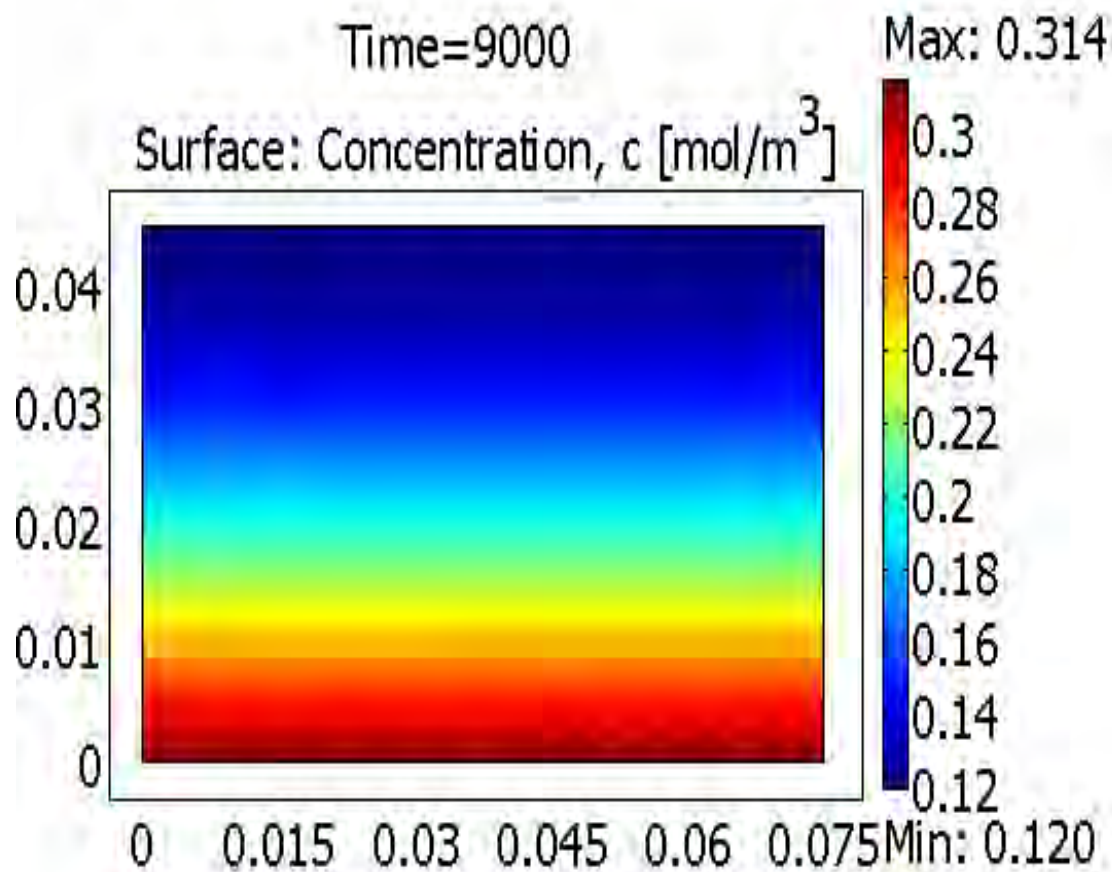
v Velocity, m/s

Quantitative evaluation of Model



“Convection Diffusion module” in “Comsol Multiphysics 3.2” provide the best features to couple any nonlinear adsorption isotherm with the “Advective Dispersion Reaction Equation”

MODEL EVALUATION

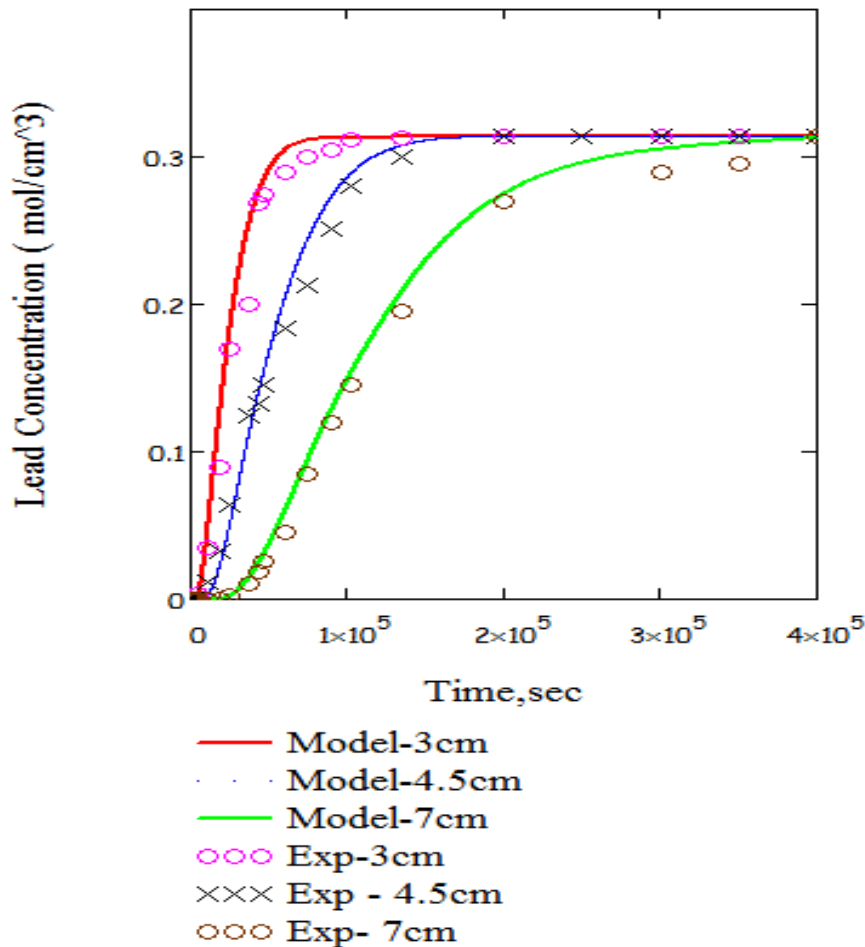


Conditions:

- $C_0 = 0.314 \text{ mol}/\text{m}^3$
- $Q = 6 \text{ ml}/\text{min}$
- *Bed thickness = 4.5 cm*
- $K = 1.66 \text{ m}^3/\text{mol}$
- $q_0 = 0.027 \text{ mol}/\text{m}^3$

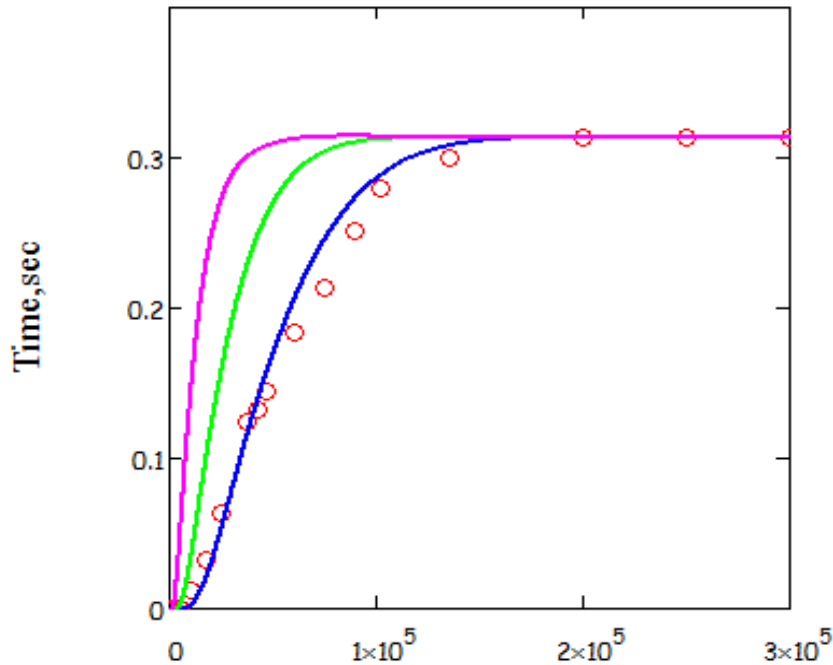
Contaminant concentration distribution in the column

Break through curves for different bed thickness and Experimental Validation



Bed Thickness	Saturation Time
3.0 cm	$1.5 \cdot 10^5$ sec (1day 17 hr)
4.5 cm	$2.0 \cdot 10^5$ sec (2days 8hr)
7.0 cm	$5 \cdot 10^5$ sec (5days 18hr)

Break through curves for different values of K



Liquid phase concentration, mol/m³

○○○ Exp at 25 C

— k=1.66 m³/mol(25 C)

— k= 0.903 m³/mol(35 C)

— k=0.357 m³/mol(45 C)

Conditions:

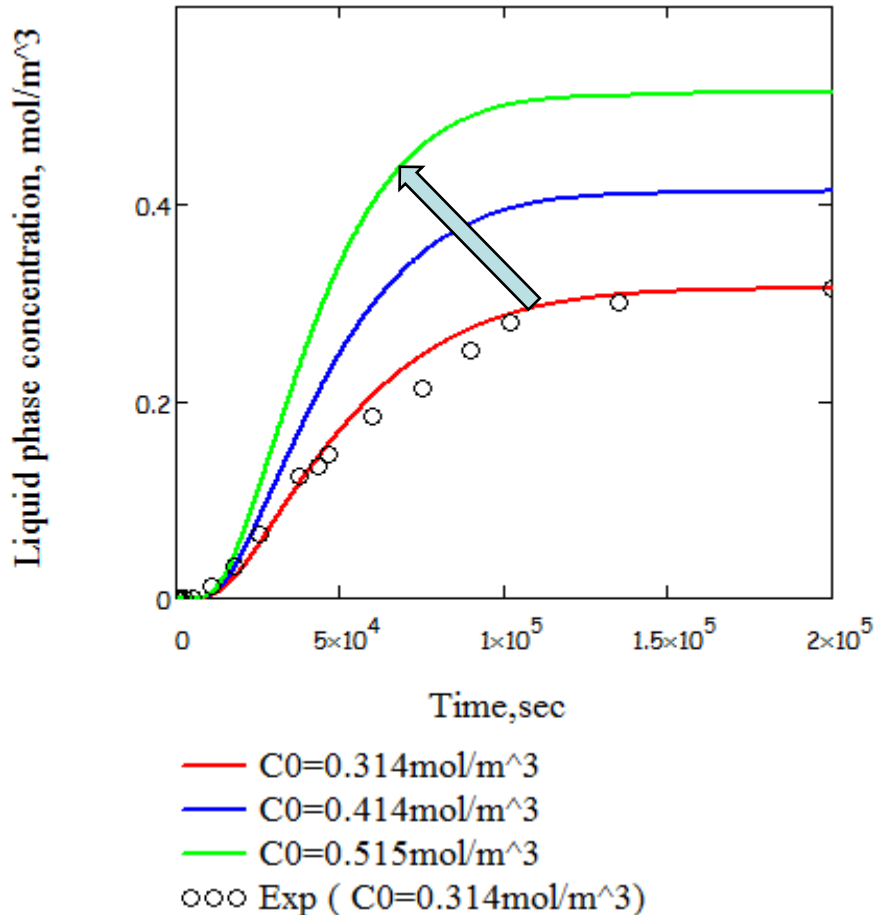
- $C_0 = 0.314 \text{ mol/m}^3$
- $Q = 6 \text{ ml/min}$

Bed thickness = 4.5 cm

- K values obtained from batch experiments are used to simulate the system. Model is validated for $1.66 \text{ m}^3/\text{mol}$.
- Saturation time decreases with decrease in k value.

$K \text{ m}^3 / \text{mol}$	Saturation Time
1.66	$2 \cdot 10^5 \text{ sec}$
0.37	$0.7 \cdot 10^5 \text{ sec}$

Break through curves for different Initial Concentrations



Conditions:

- $K = 1.633 \text{ m}^3 / \text{mol}$
- $q_0 = 0.027 \text{ mol/kg}$
- $Q = 6 \text{ ml/min}$
- *Bed thickness = 4.5 cm*

The break through curves are steeper for higher values of feed concentration

Mass transfer rate



Bed Saturation Time



Equilibrium attains faster

Conclusions and future Developments

- Advective Dispersion Reaction Equation (ADRE) coupled with Langmuir adsorption isotherm was solved using COMSOL MULTIPHYSICS -3.2
- Any Nonlinear adsorption isotherms can be readily coupled with ADRE using this model and solved by COMSOL MULTIPHYSICS - 3.2
- This model can be used to predict the behavior of the system under various conditions without conducting the experiments by knowing the adsorption parameters
- Velocity variation along the length of the column was not considered, momentum equation will be coupled with ADRE to overcome this limitation

ACKNOWLEDGEMENT

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THANK YOU



QUESTIONS ?

