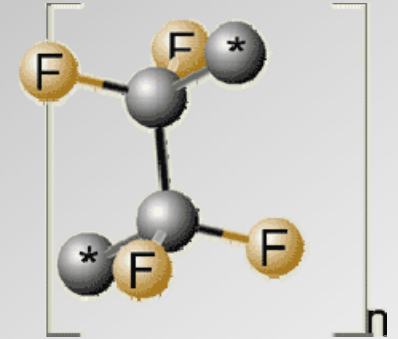


Study of a Self Heating Process of Tetrafluoroethylene by the Exothermic Dimerization Reaction to Octafluorocyclobutane

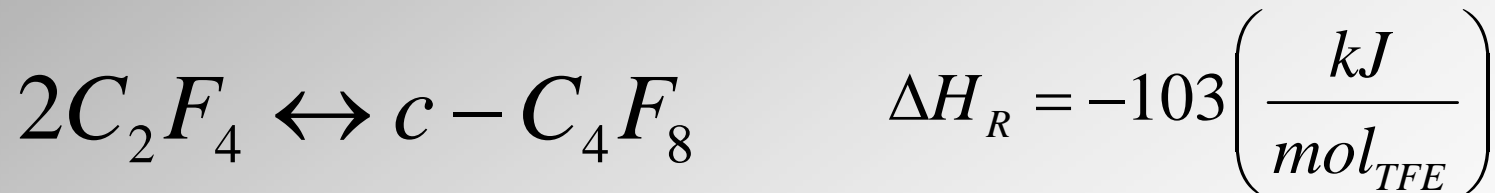
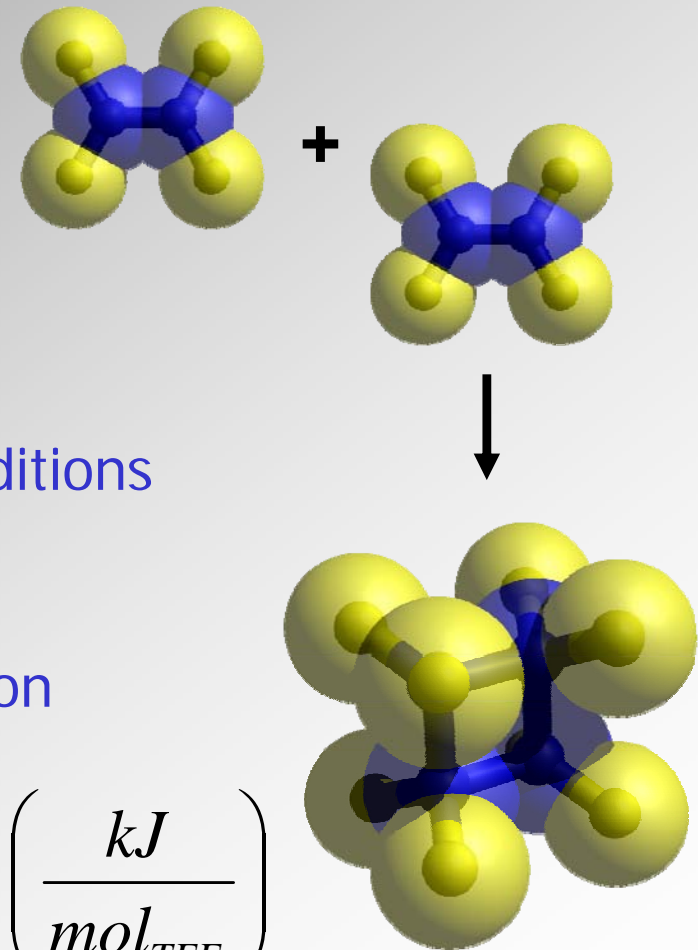
M. Beckmann-Kluge, H. Krause, V. Schröder, A. Acikalin and J. Steinbach
Federal Institute for Materials Research and Testing (BAM),
Technical University Berlin

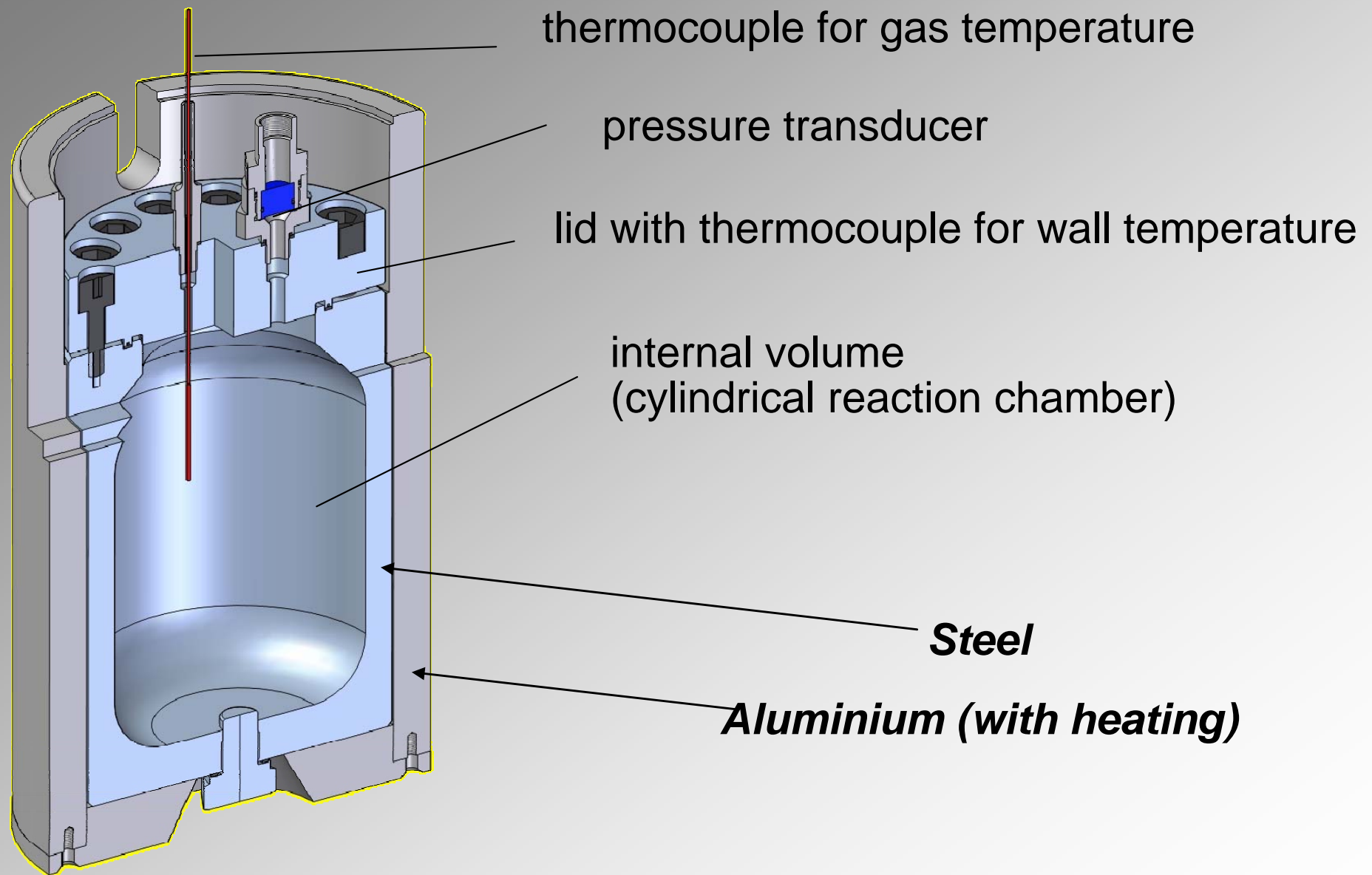
- Motivation
- Hazardous properties of Tetrafluoroethylene
- Experiments
- Geometric and numerical model
- Numerical simulation of self heating process
 - Feedback between model and experiments
 - New Kinetics for dimerization reaction
 - Measurement of more detailed temperature field
- Outlook

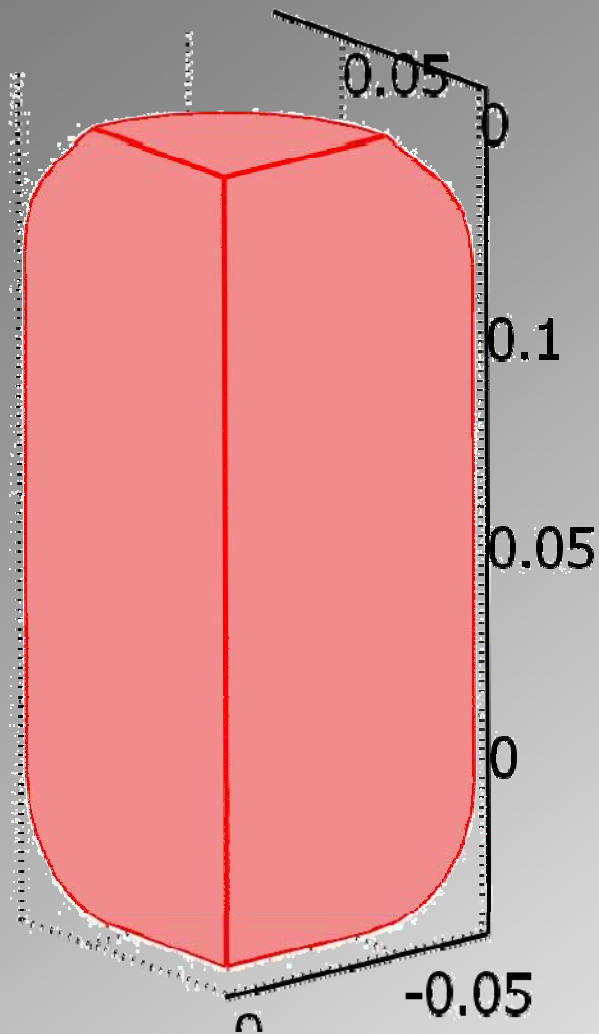
- Tetrafluoroethylene (TFE, C_2F_4) is monomer of Polytetrafluoroethylene (PTFE) and other copolymers (100.000 t/year)
- PTFE is resistant to most reactive and corrosive chemicals and has non-sticky properties



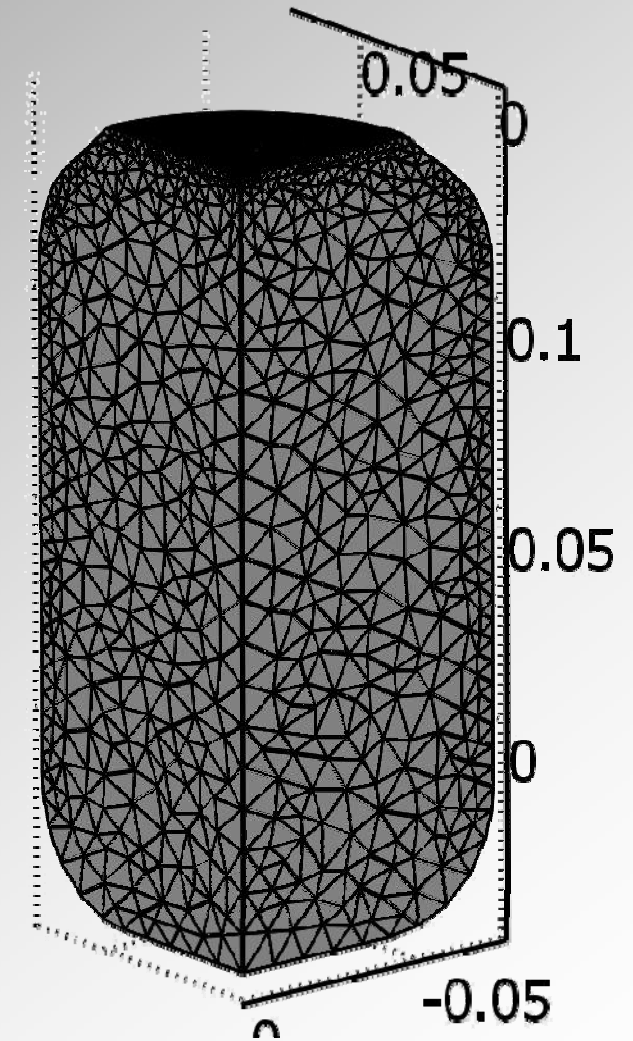
- TFE is a decomposable gas → possibility of explosive decomposition
- Several accidents in the last decades
- Sources for ignition:
 - Spark ignition, electrostatic
 - Hot surfaces → content of this work
- Research project to determine hazardous conditions
- Exothermic Dimerization reaction of TFE to Octacyclofluorobutane can cause ignition

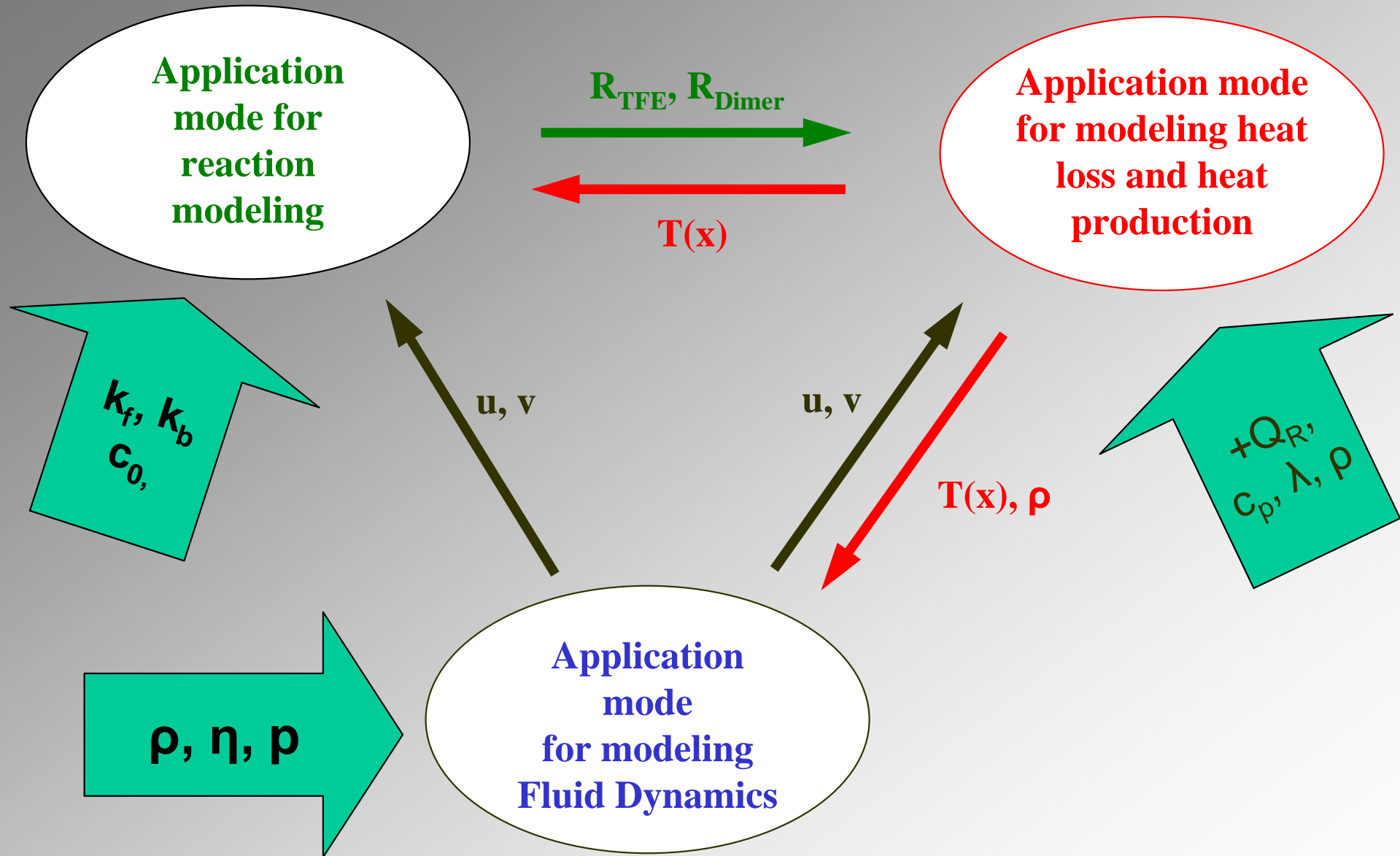






- 3D-geometry of 3-dm³ autoclave was transferred from a CAD software
- First calculations were carried out
- Very long solving times
- Transfer to 2D-model





- Heat transfer by conduction and convection

$$\rho \cdot c_p \cdot \frac{\partial T}{\partial t} = \nabla(k \cdot \nabla T) + Q_{production} \cdot \rho \cdot c_p \cdot \mathbf{u} \cdot \nabla T$$

- Species transfer by diffusion and convection

$$\frac{\partial c_1}{\partial t} = \nabla(D \cdot \nabla c_1) + R - \mathbf{u} \cdot \nabla c_1$$

with $R = \text{reaction rate } c_1$

- Impulse transport by Navier-Stokes approach

$$\rho \cdot \frac{\partial \mathbf{u}}{\partial t} + \rho \cdot \mathbf{u} \cdot \nabla \mathbf{u} = \nabla \left[-\rho \mathbf{I} + \eta (\nabla \mathbf{u} + (\nabla \mathbf{u})^T) - \left(\frac{2\eta}{3} - \kappa_{dv} \right) \cdot (\nabla \cdot \mathbf{u}) \cdot \mathbf{I} \right] + \mathbf{F}$$

with : \mathbf{u} is the velocity field

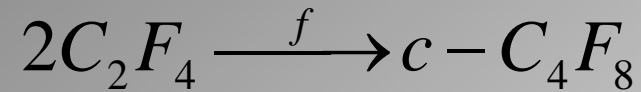
\mathbf{F} is the volume force field

\mathbf{I} is the identity matrix for the viscous stress tensor

Computational results for a 3-dm³- autoclave (300°C; 5,0 bara)
In 3D for 14 s, solving time about 28 hours

- **First calculations were carried out**
- **Very long solving times**
→
- **Transfer to 2D-model**

forward reaction



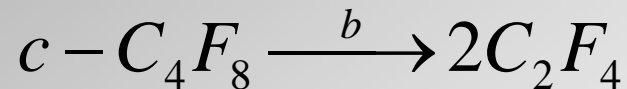
2. order reaction

$$k_f = 82800 \left[\frac{\text{m}^3}{\text{mol} \cdot \text{s}} \right] \cdot \exp\left(\frac{-105200[\text{J/mol}]}{RT}\right)$$

$$r_f = \left(c_{C_2F_4} \right)^2 \cdot k_f$$

New 2-stage kinetics
was determined

backward reaction

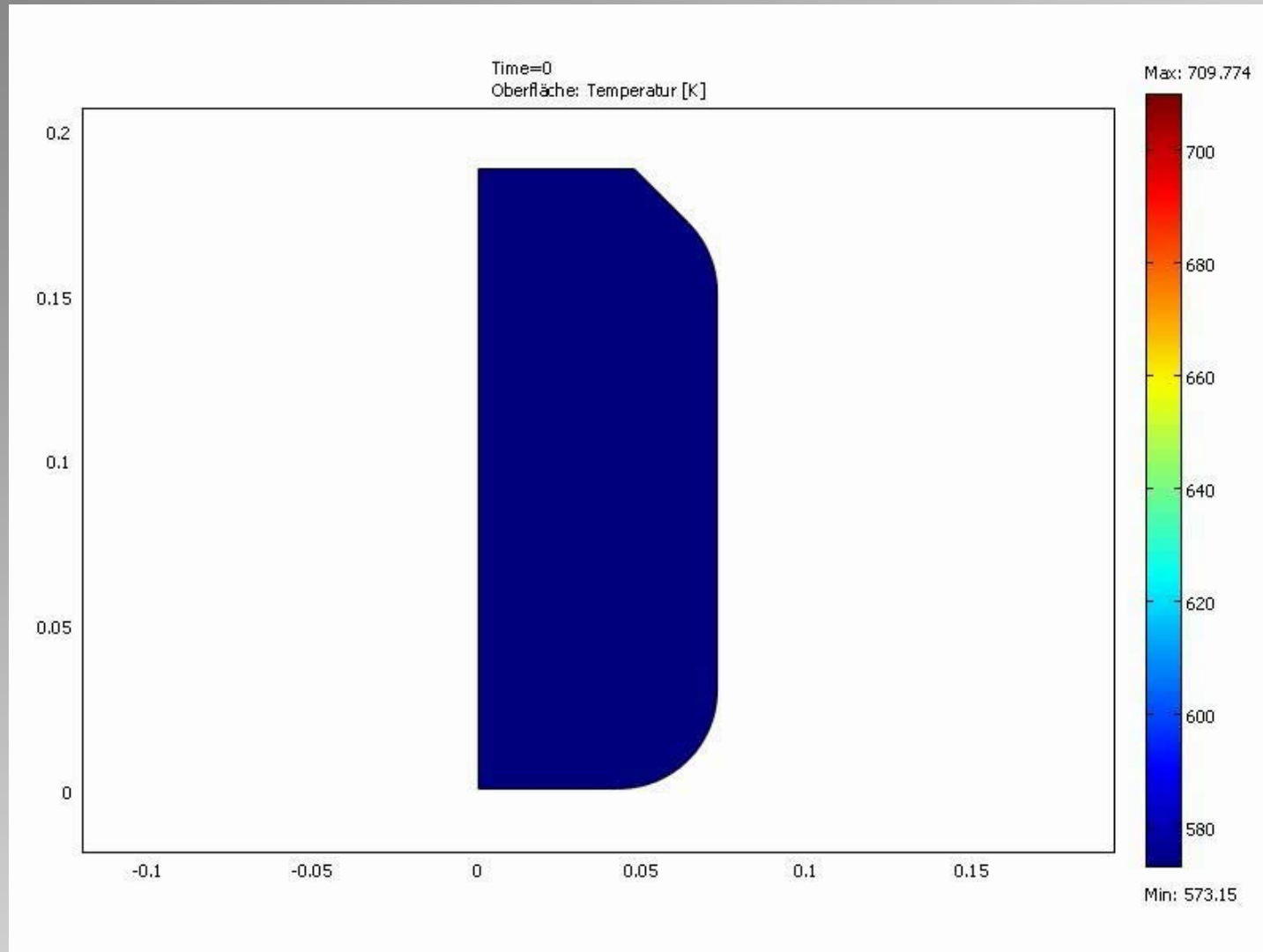


1. order reaction

$$k_b = 2,1 \cdot 10^{16} \left[\frac{\text{m}^3}{\text{mol} \cdot \text{s}} \right] \cdot \exp\left(\frac{-310961[\text{J/mol}]}{RT}\right)$$

$$r_b = c_{c-C_4F_8} \cdot k_b$$

Computational results for a 3-dm³- autoclave (300°C; 5,0 bara)



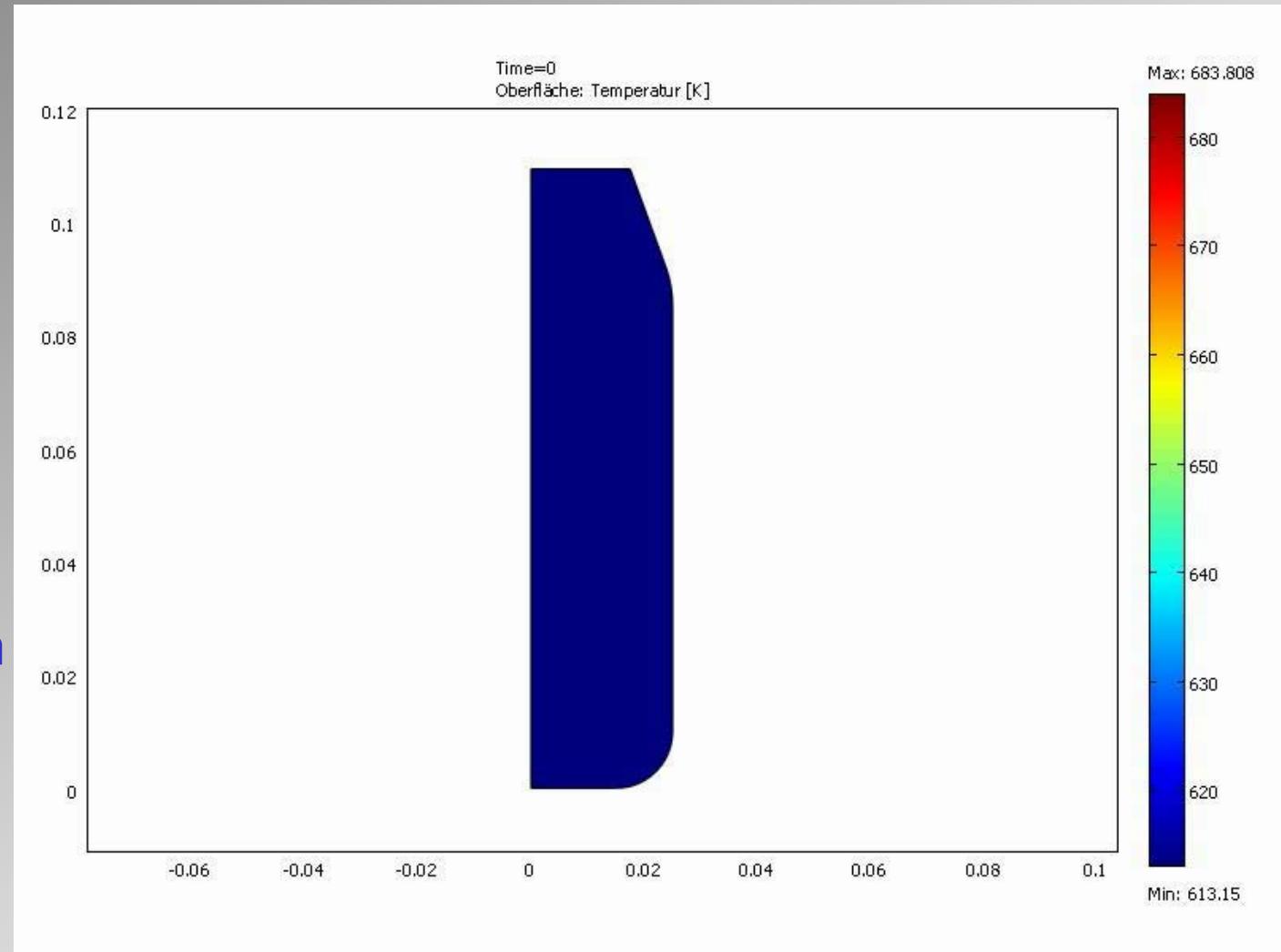
= 436°C

= 300°C

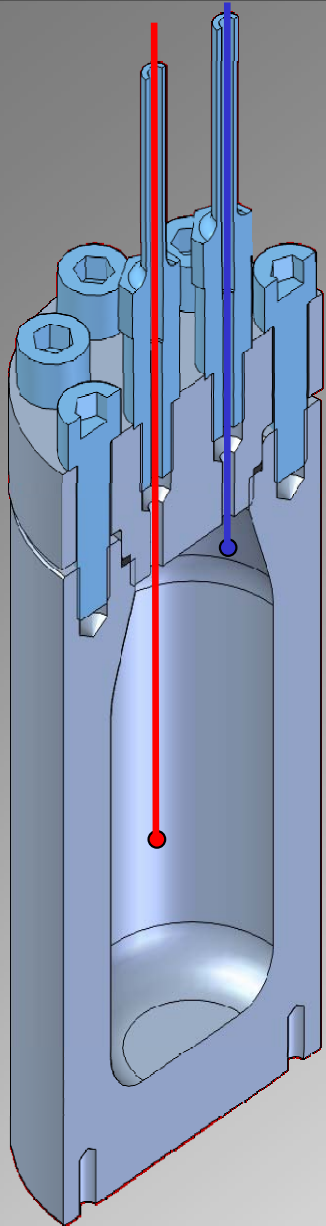
Feedback Effekte: Modellierung \leftrightarrow Experiment???

- FEM – modeling showed thermal layering \rightarrow even in a 0.2-dm^3 autoclave, inner height of 120 mm

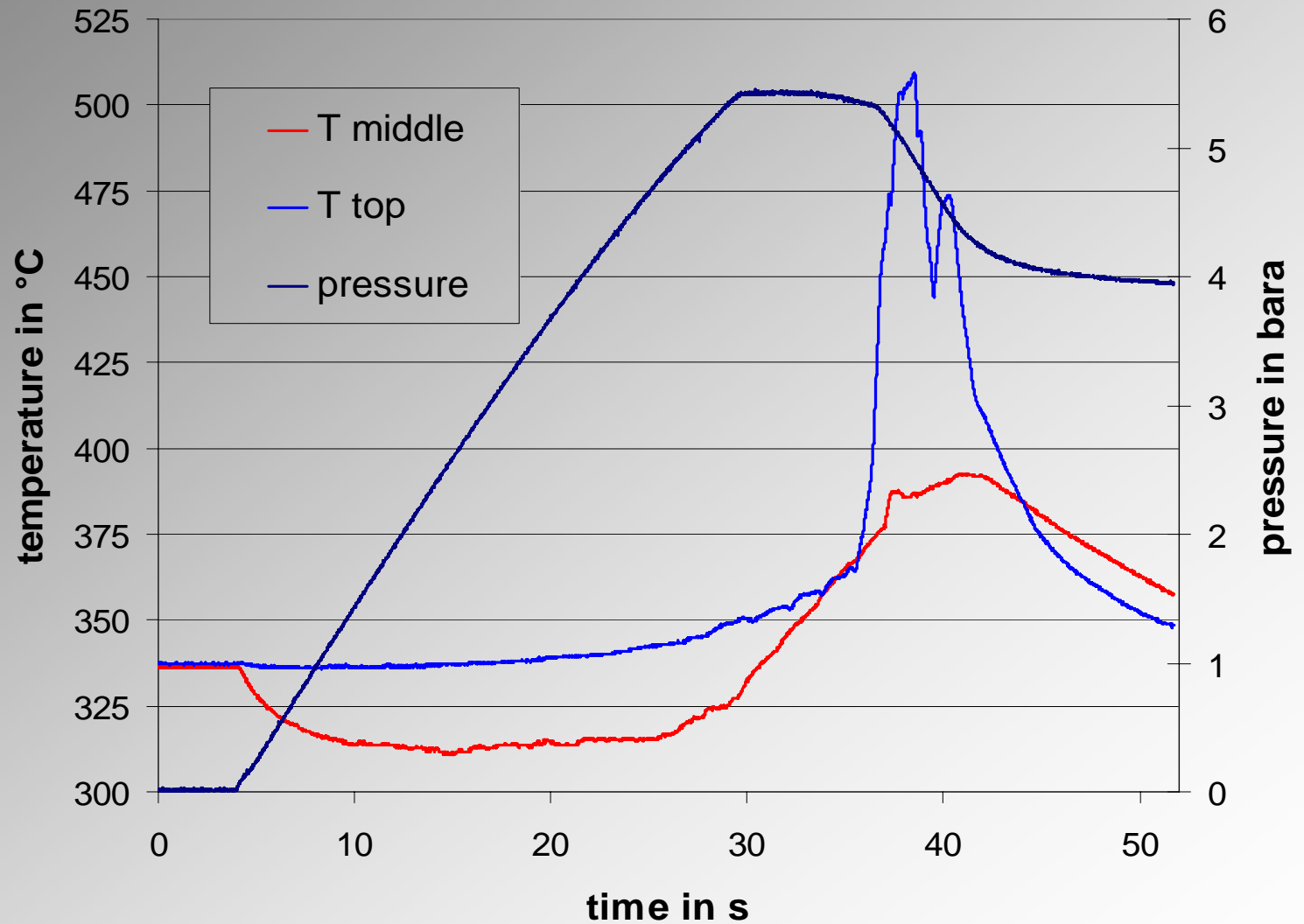
- Experiments with thin thermocouples were carried out



Feedback effects: additional tests for temperature layering



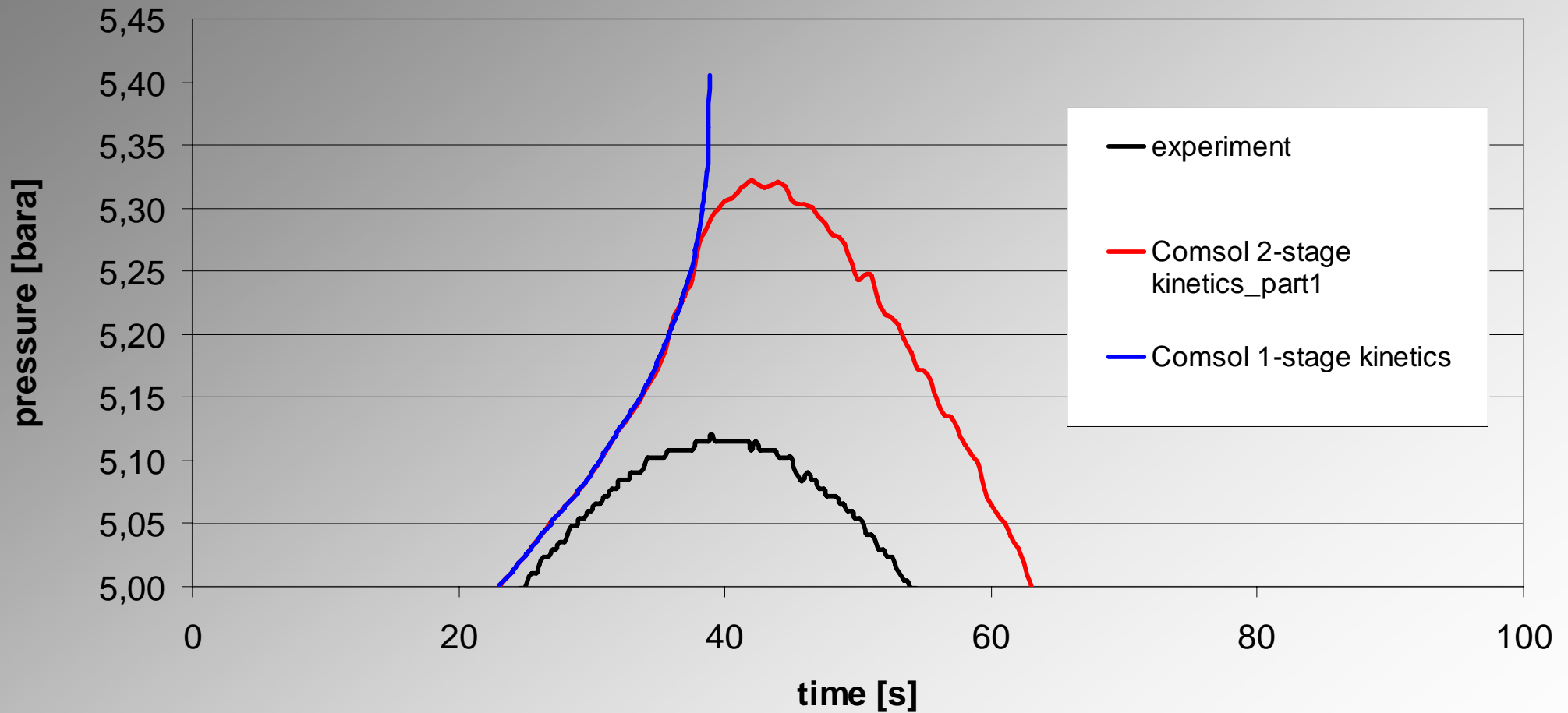
test 5bara, 340°C, 0.2-dm³ autoclave



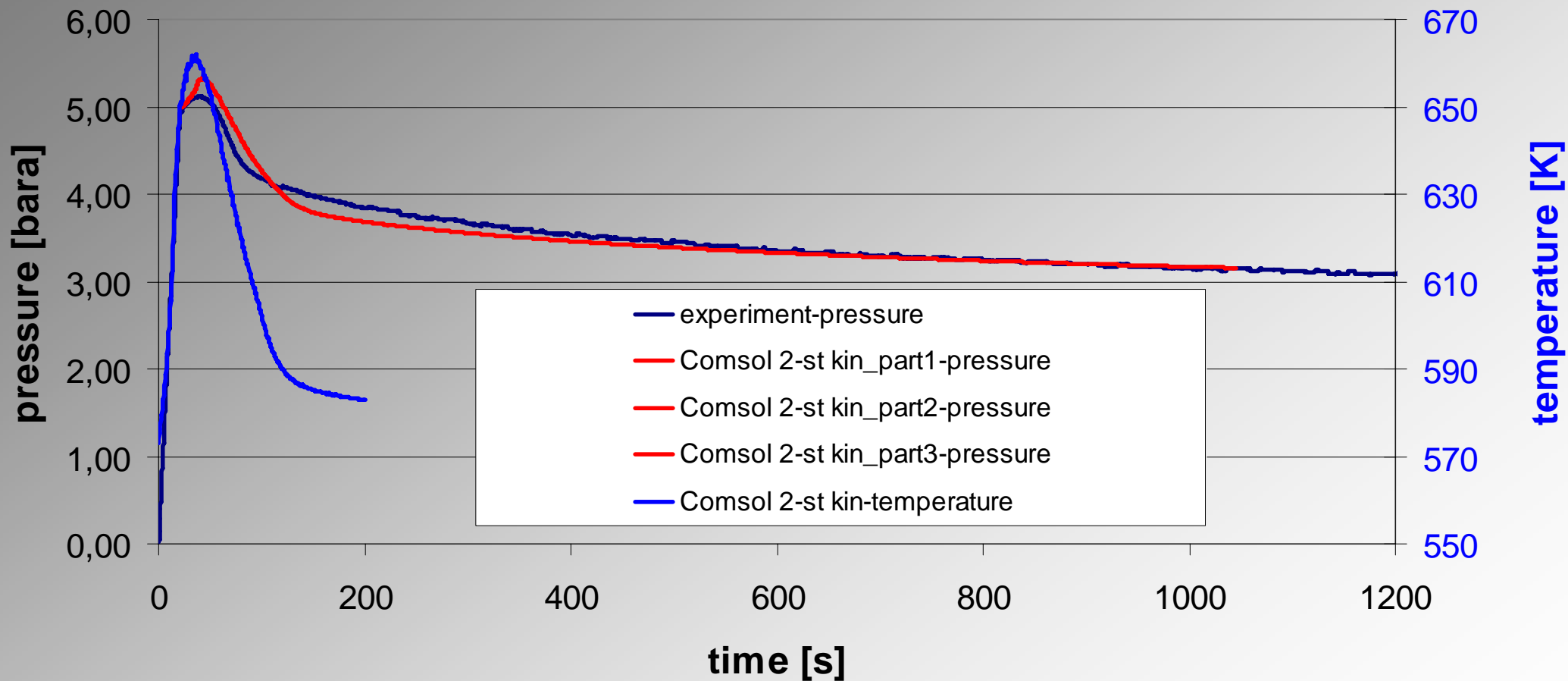
Advantage of 2-stage-kinetics



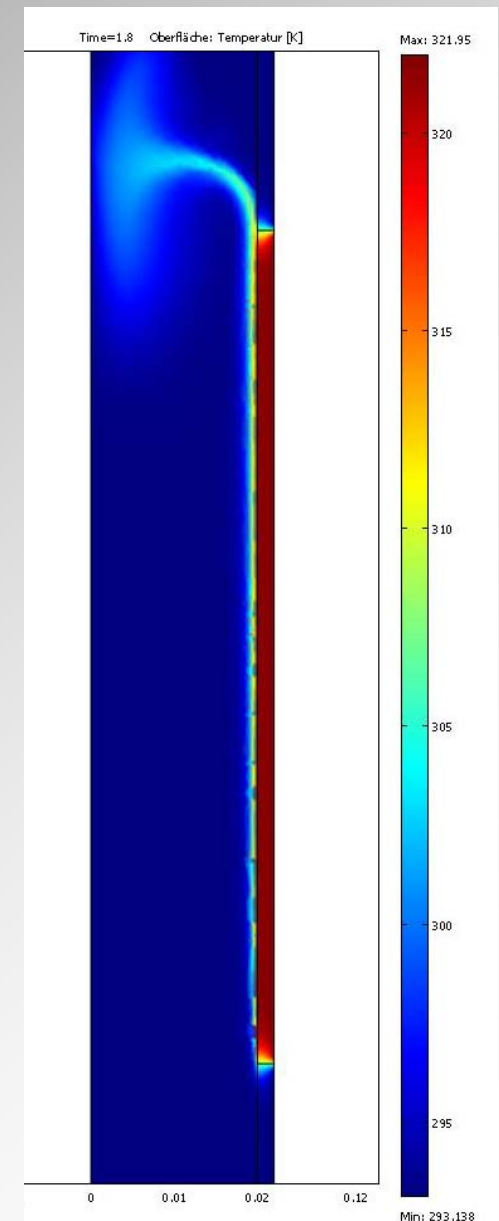
100% TFE, 3-dm³, $t_{\text{wall}}=300^{\circ}\text{C}$, test TFEait70



100% TFE, 3-dm³, $t_{\text{wall}}=300^{\circ}\text{C}$, test TFEait70



- appliance of the numerical approach on other geometries
 - Vertical and horizontal pipes with different diameters
 - Big vessels
 - Influence of forced flow in pipes on self heating process
- Improvement of the used Kinetics approach



Thanks for your attention!