

## Introduction

- MHD instabilities in liquid metal(LM) flows in a fusion reactor blanket associated with the mixed-convection phenomena have recently been recognized to be dominant, critically important to any LM blanket concept.
- Understanding and quantifying these effects is absolutely necessary to design a feasible LM blanket.
- The existing MHD codes lack the ability to capture such phenomena at high Ha, Re and Gr numbers or this ability has not been demonstrated.
- Therefore, we initiated an effort to build and test a new computational methodology (physical/mathematical model, boundary conditions, numerical methods) to particularly address a class of time-dependent MHD flows with volumetric and surface heating.
- We selected COMSOL as the starting code for building 3-D MHD capability because it is a commercial 3-D multi-physics solver with many advanced capabilities.

## Governing equations and Dimensionless parameters

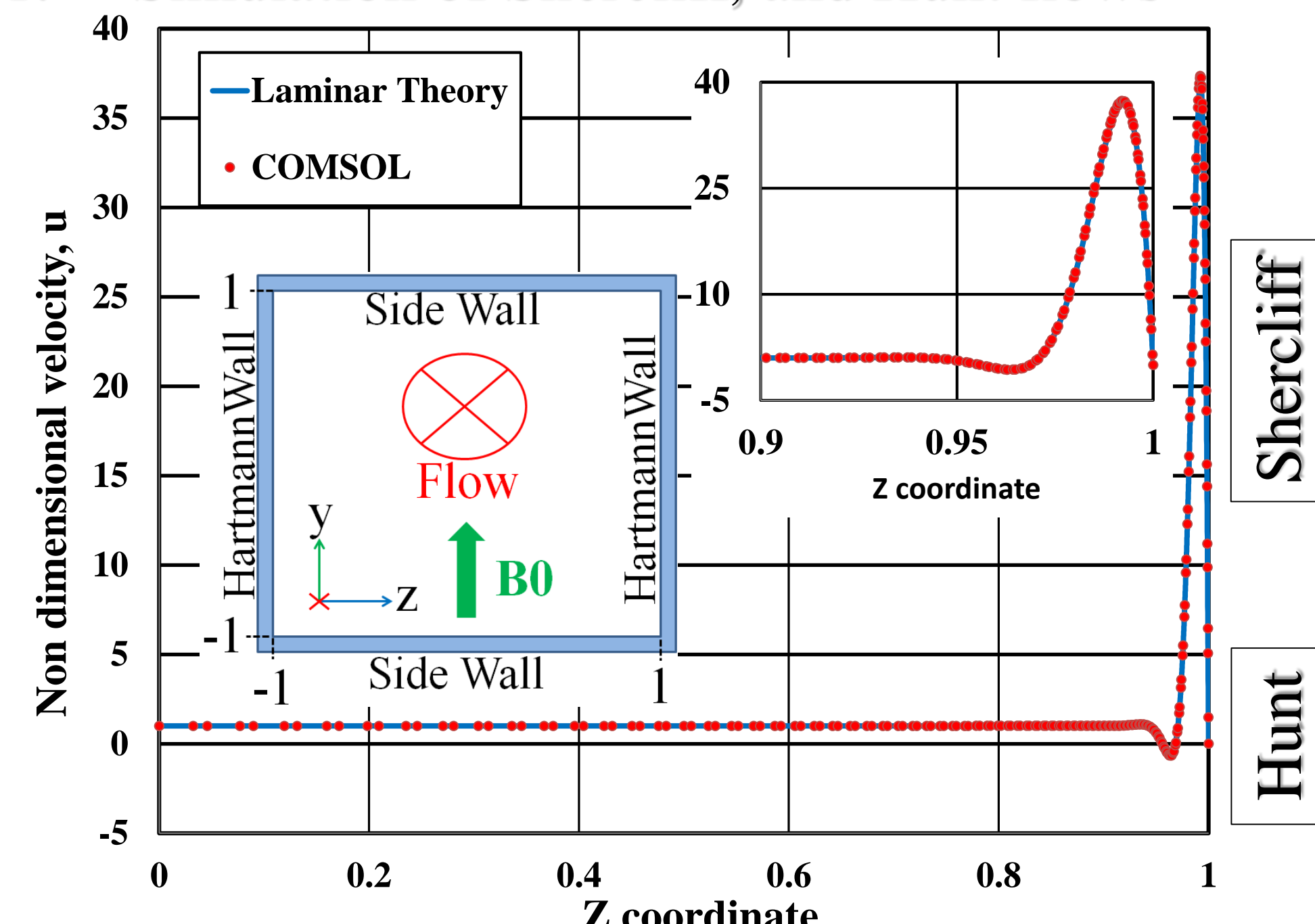
- Flow equations:  $\nabla \cdot (\mathbf{u}) = 0; \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla p + \nu \nabla^2 \mathbf{u} + \mathbf{f}$   
where  $\mathbf{f} = \frac{1}{\rho} \mathbf{J} \times \mathbf{B} + \mathbf{g}(1 - \beta(T - T_0))$
- Electric potential equation:  $\nabla^2 \phi = \nabla \cdot (\mathbf{u} \times \mathbf{B});$
- Ohm's law:  $\mathbf{J} = \sigma(-\nabla \phi + \mathbf{u} \times \mathbf{B});$
- Heat transfer equation:  $\rho C_p \frac{\partial T}{\partial t} + \rho C_p \mathbf{u} \cdot \nabla T + \nabla \cdot (-\kappa \nabla T) = Q_e$

Reynolds number (Re)	Hartmann number (Ha)	Grashof number (Gr)/ Rayleigh number (Ra)
Re: Ratio of inertia to viscous force	Ha <sup>2</sup> : Ratio of Electromagnetic to viscous force	Gr or Ra: Ratio of buoyancy to viscous force

## Validation procedure and Results

- We follow the validation approach proposed in 2014 by Smolentsev et al [1].
- First, **fully developed laminar MHD flows** were computed and the results compared with the analytical Shercliff [2] and Hunt [3] solutions at high Ha up to 15,000 for electrically conducting and insulating ducts.
- Second, the COMSOL capability to **address developing MHD flows** was tested against available experimental data for 3D laminar steady MHD flows in a non-uniform transverse magnetic field [4].
- As a final test, **two unsteady MHD flows** were computed and the results compared against available 3D numerical data: (1) MHD flow in a horizontal cavity with volumetric heating [5] and (2) periodic MHD flow in conducting duct with thin electrically conducting walls [6].

### 1. Simulation of Shercliff, and Hunt flows



Ha	Non-dimensional flow rate		Relative Error
	Analytical	COMSOL	
500	7.6790e-3	7.6655e-3	0.1761%
5000	7.9018e-4	7.8715e-4	0.3839%
10000	3.9654e-4	3.9521e-4	0.3372%
15000	2.6479e-4	2.6384e-4	0.3596%
500	1.4050e-3	1.4057e-3	0.0501%
5000	1.9070e-5	1.9014e-5	0.2948%
10000	5.1690e-6	5.1445e-6	0.4675%
15000	2.4250e-6	2.4133e-6	0.4859%

Fig.1 Velocity distribution for Hunt flow at Ha = 15000 with electrically insulating on side wall and 0.01 of conducting ratio on Hartmann wall

Table 1 Numerical comparison between analytical and COMSOL solutions with same set up parameters in Fig. 1

- Good agreement between COMSOL results and analytical solutions with less than 0.5% difference for flow rate at Hartmann number up to 15000.

### 2. 3D laminar pipe MHD flow with fringing magnetic field

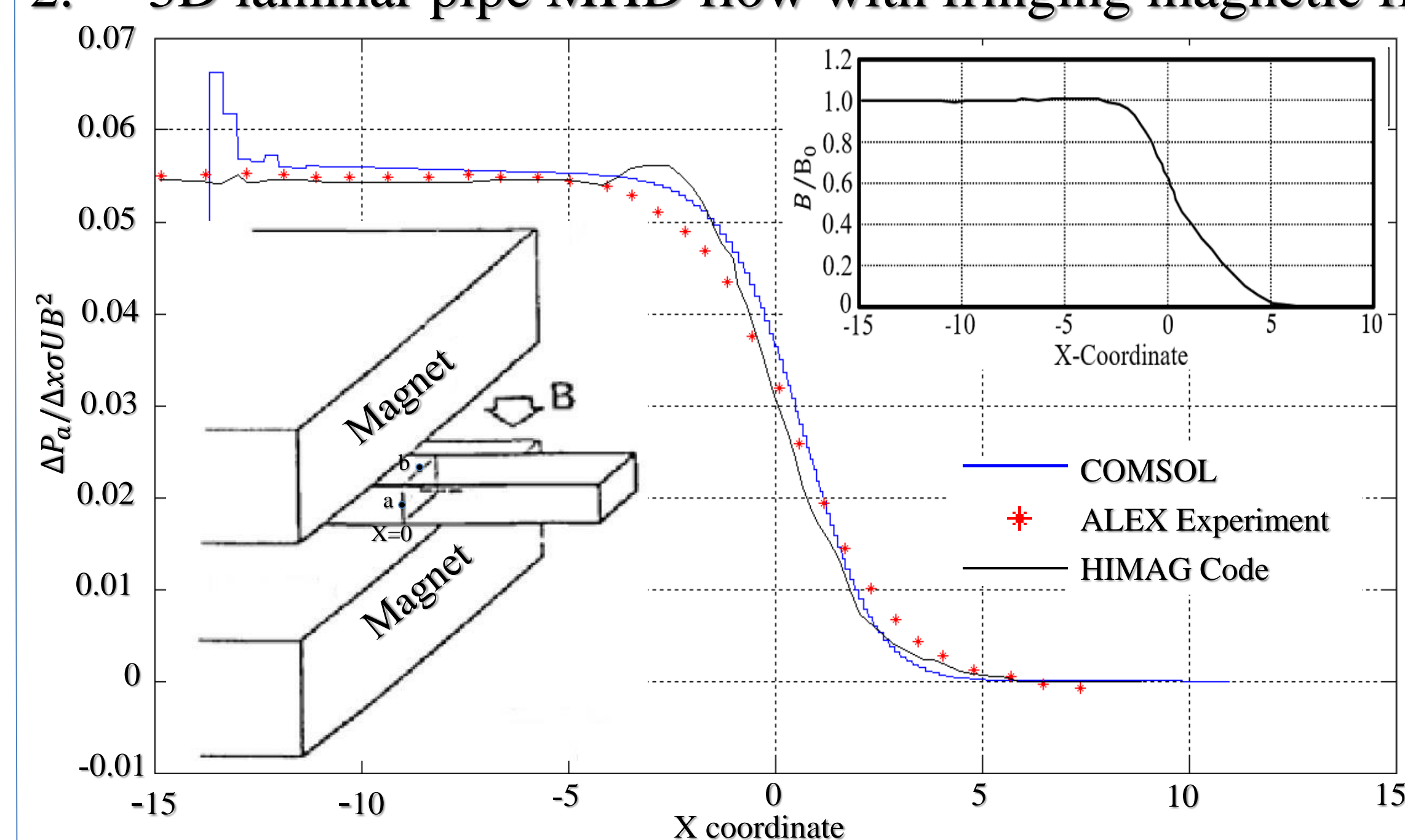


Fig.2 Comparisons of non-dimensional pressure gradient distribution at point a, along flow direction with Ha = 2900 and Re = 15574

- Qualitative and quantitative agreement with experimental data and HIMAG simulation.

### 3. Unsteady natural convection MHD flow in a cubic enclosure with volumetric heating. All walls are adiabatic except for top isothermal wall.

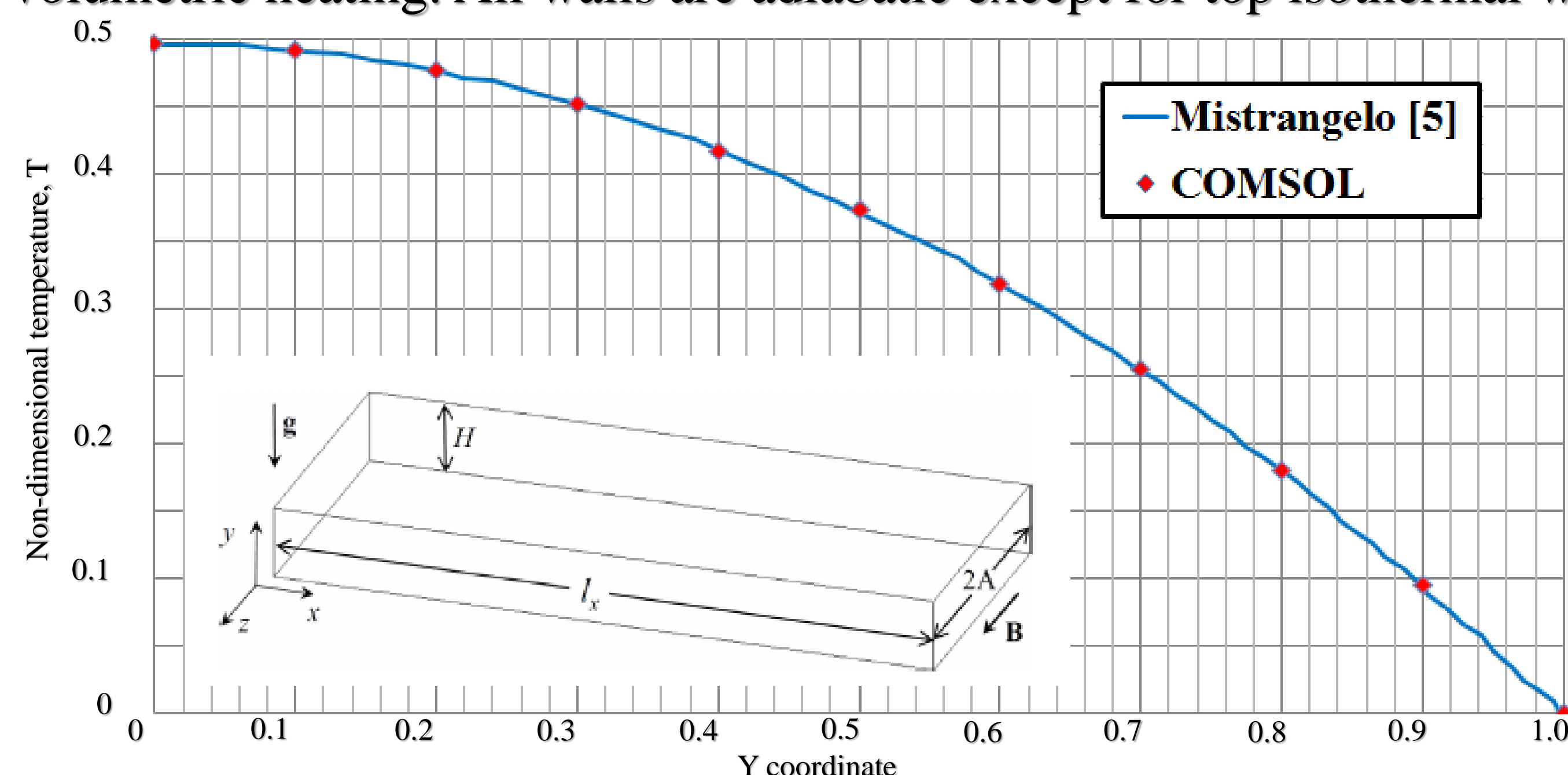


Fig.3 Axially averaged temperature distribution along vertical axis with Ha = 200 and Ra = 1e4 (steady)

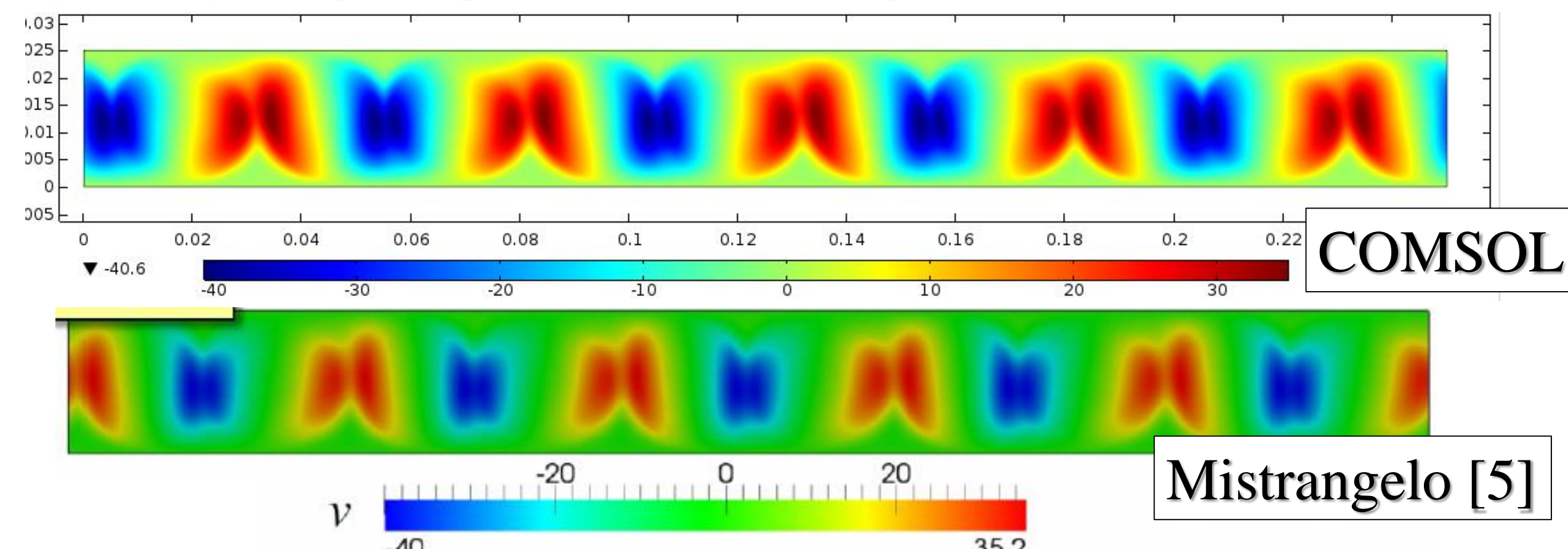


Fig.4 Instantaneous contours of vertical velocity at y-z plane with Ha = 200, Ra = 3e5 (unsteady).

- Qualitative and quantitative match on steady solution, and qualitative agreement on unsteady solution (No quantitative data in reference [5]).

### 4. Simulation of Kelvin-Helmholtz instability on isothermal MHD flow generated naturally by high flow jet in an electrically conducting duct.

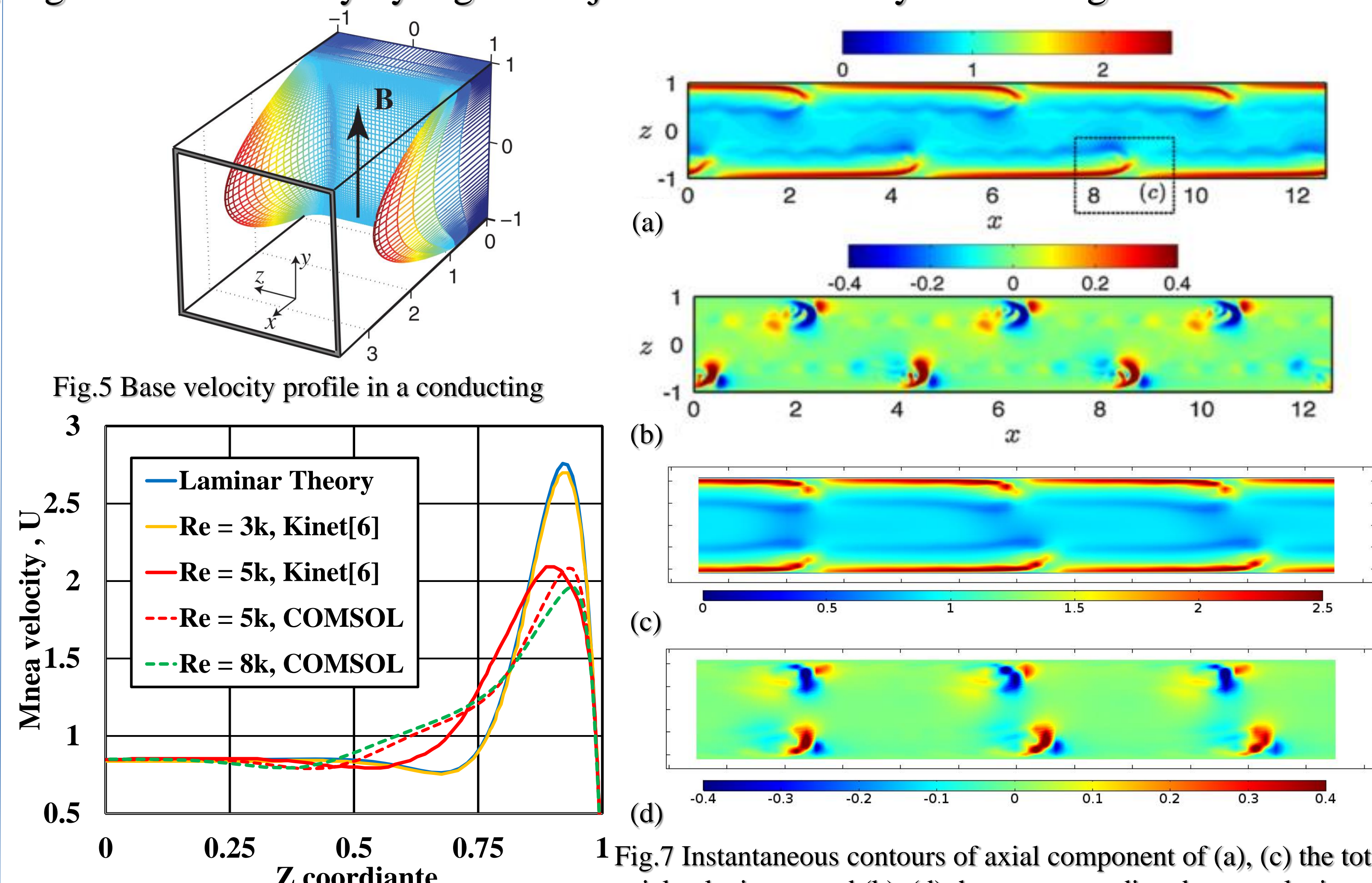


Fig.5 Base velocity profile in a conducting

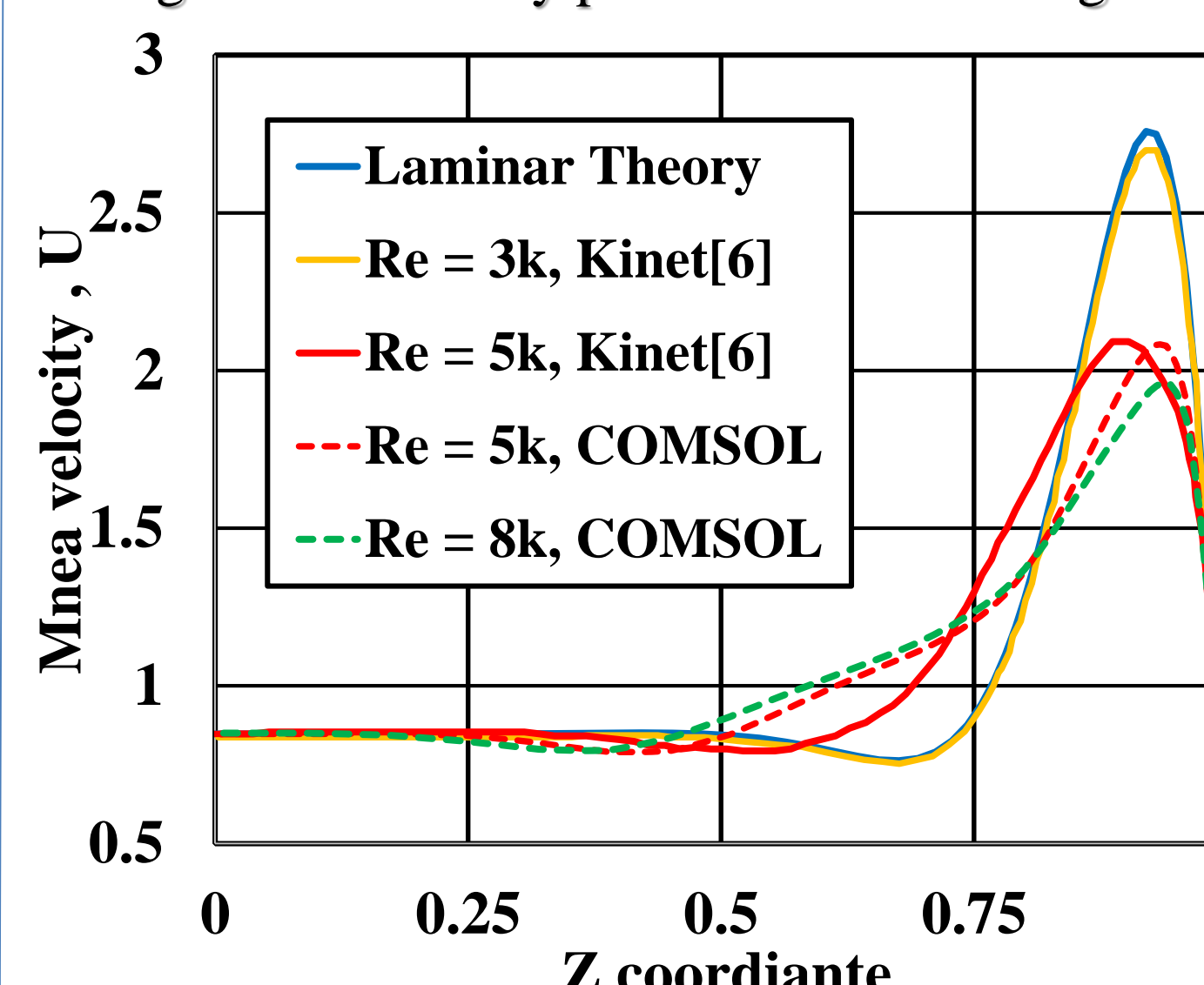


Fig.6 Mean velocity distribution along z axis

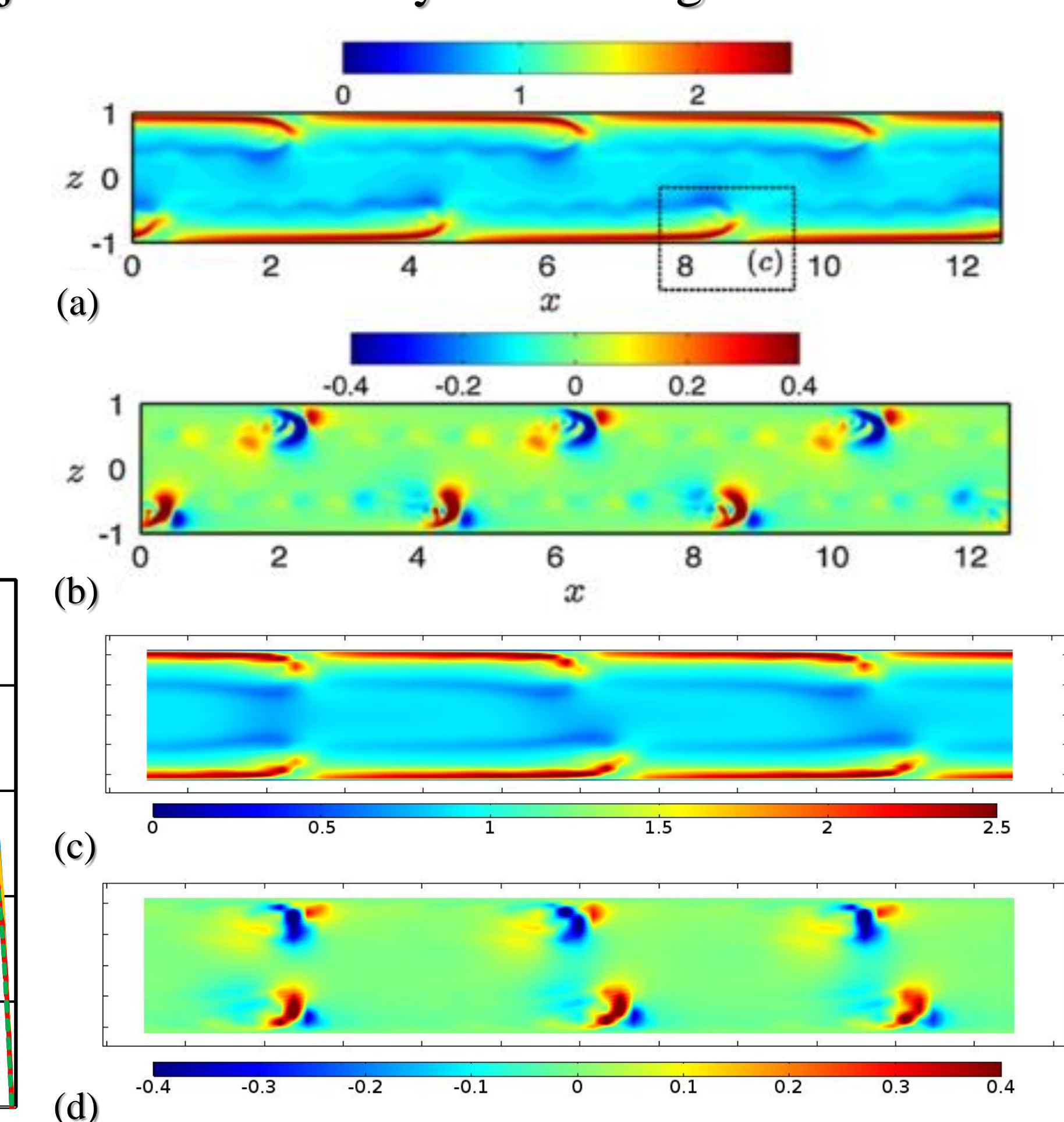


Fig.7 Instantaneous contours of axial component of (a), (c) the total axial velocity  $u_1$  and (b), (d) the transverse disturbance velocity  $u_3'$  for Re = 5000 from Kinet [6] and COMSOL respectively

- Qualitative and quantitative match on mean velocity distribution and flow development patterns comparing with DNS code results in reference [6].
- Higher numerical dissipation on the bulk side of flow jet can be observed in COMSOL, and future tune up will be proceeded.

## Concluding Remark and Future Work

- All computations have demonstrated good qualitative and in most of the cases fair quantitative match with the available experiment, analytical and numerical data.
- It suggests that COMSOL can serve as a good CMHD tool along to analyze multi-physics effects in MHD flows for fusion applications.
- As a next step, we will apply our numerical methodology to analyze critical MHD instabilities under experimental and real blanket conditions.

## References

- [1] S. Smolentsev, S. Badia, R. Bhattacharyay, et al., Fusion Eng. Des. 100 (2015) 65–72
- [2] Shercliff, Mathematical proceeding of the Cambridge Philosophical Society, 1953, pp 136-144.
- [3] Hunt, J.Fluid Mech. (1965), vol. 21, pp. 577-590
- [4] B.F. Picologlou, C.B. Reed, in: JUTAM Symposium on LM MHD, Riga, USSR, 1988
- [5] Chiara Mistrangelo and Leo Buhler, Physics of Fluids. 28, 024104 (2016)
- [6] Kinet, Knaepen, Molokov, Phys Rev Lett. 2009 Oct 9; 103(15):154501.