

**SIMULATION OF IMPULSE ARC
DISCHARGE IN LINE LIGHTNING
PROTECTION DEVICES.**

Alexander Chusov

Lightning protection of overhead lines



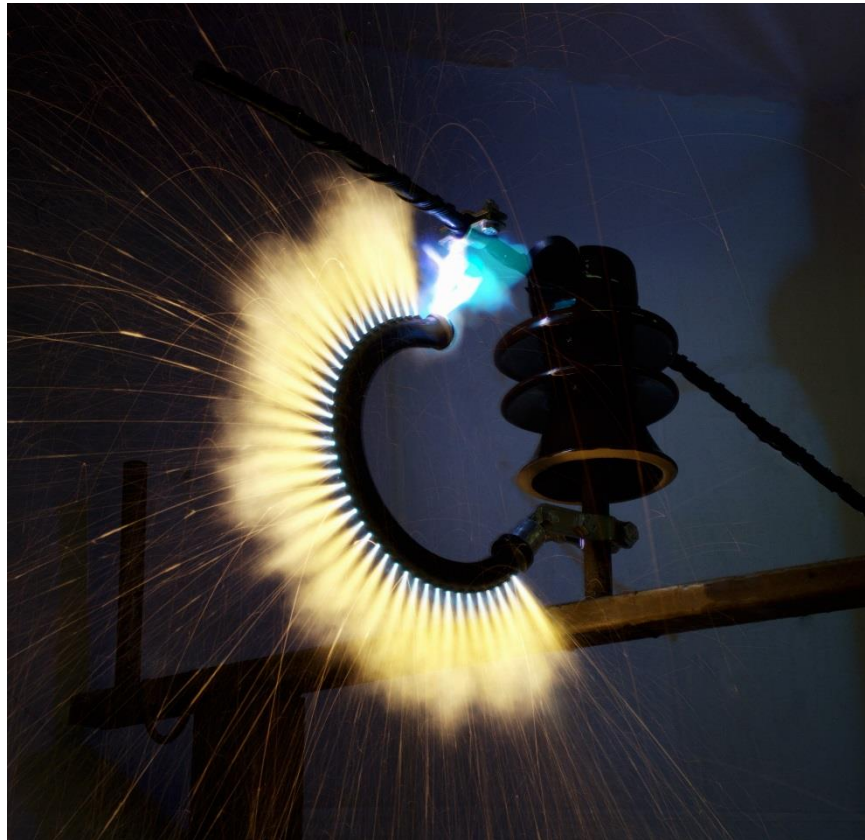
Lightning protection of overhead lines



MULTI-CHAMBER ARRESTERS

Lightning protection of overhead power lines up to 35 kV

20 kV

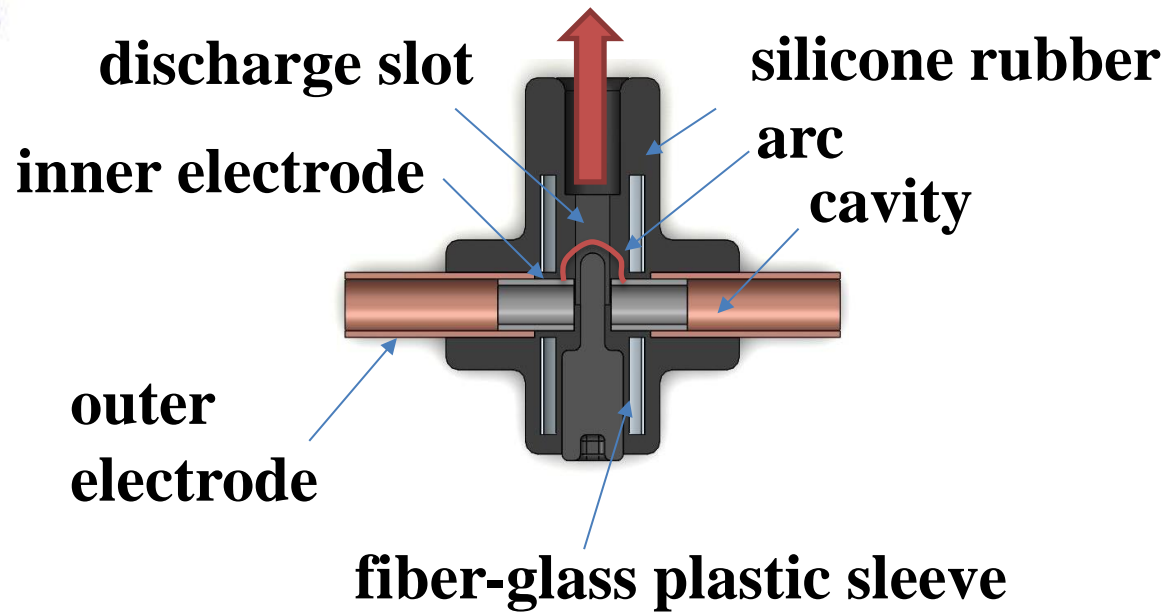
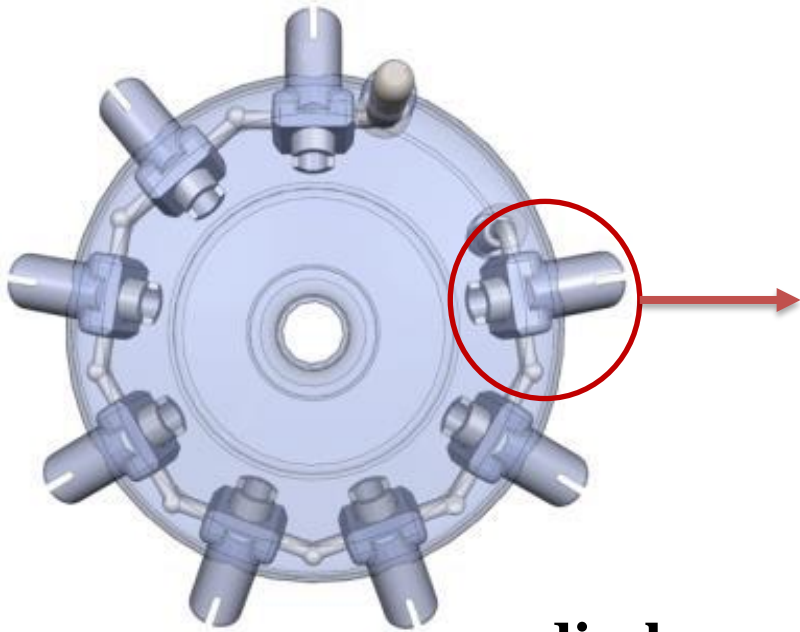


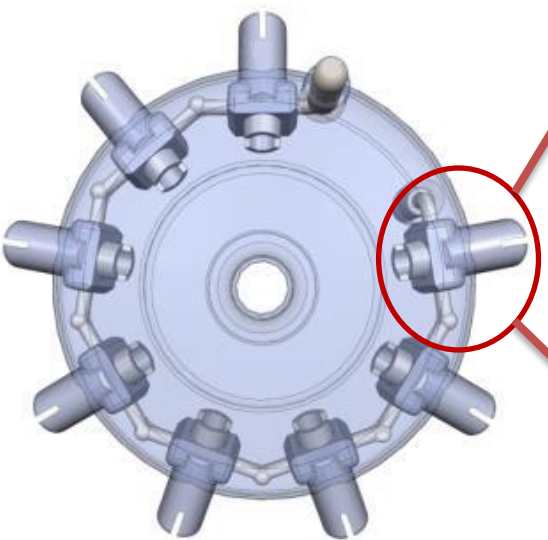
35 kV



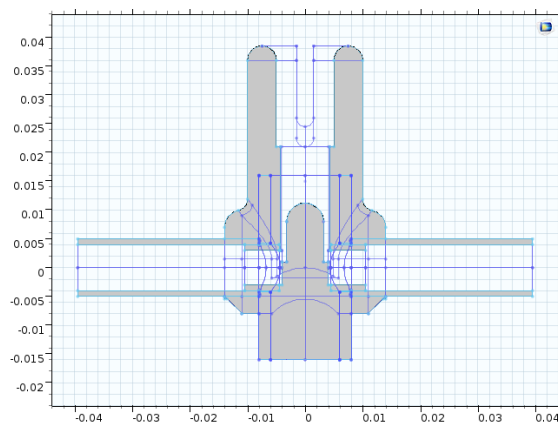
MULTI-CHAMBER ARRESTERS







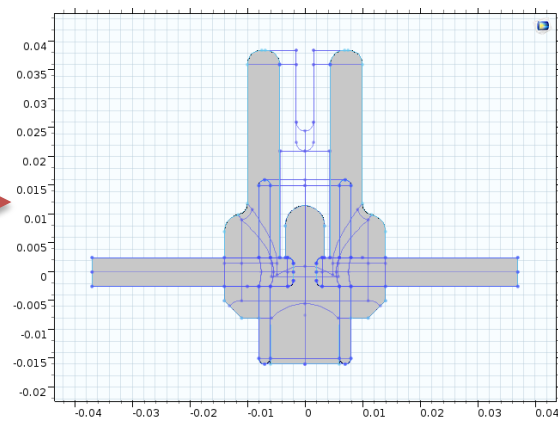
Type #1



Optimal geometry?



Type #2



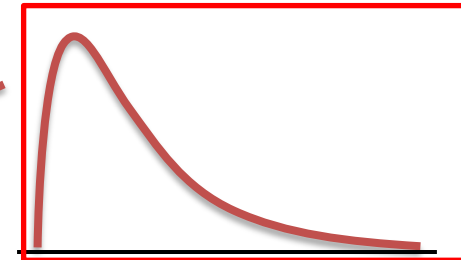
NUMERICAL EXPERIMENT SCHEME

Chamber 3D CAD model



Arc discharge model

Lightning current impulse



Arc resistance

ARC DISCHARGE MODEL

Magnetohydrodynamics equations (MHD)

$$\frac{\partial \rho}{\partial t} + \nabla \cdot \{\rho \mathbf{v}\} = 0$$

$$\frac{\partial (\rho \mathbf{v})}{\partial t} + \nabla \cdot \{\rho \mathbf{v} \otimes \mathbf{v}\} = -\nabla p + \nabla \cdot \mathbf{T} + \mathbf{j} \times \mathbf{B}$$

$$\frac{\partial (\rho H)}{\partial t} + \nabla \cdot \{\rho H \mathbf{v} - \lambda \nabla T\} = \frac{\partial p}{\partial t} + \nabla \cdot (\mathbf{T} \cdot \mathbf{v}) + \mathbf{j} \cdot \mathbf{E} - \nabla \cdot \mathbf{F}$$

$$\mathbf{j} = \sigma (\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

$$\nabla \times \mathbf{B} = \mu_0 \mathbf{j}$$

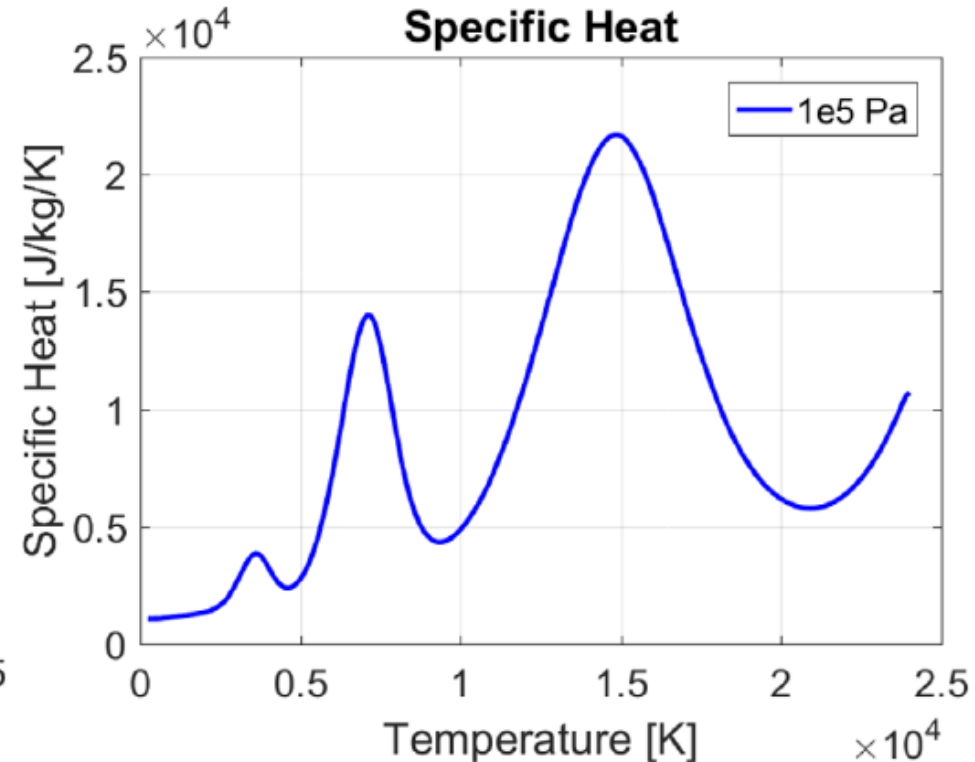
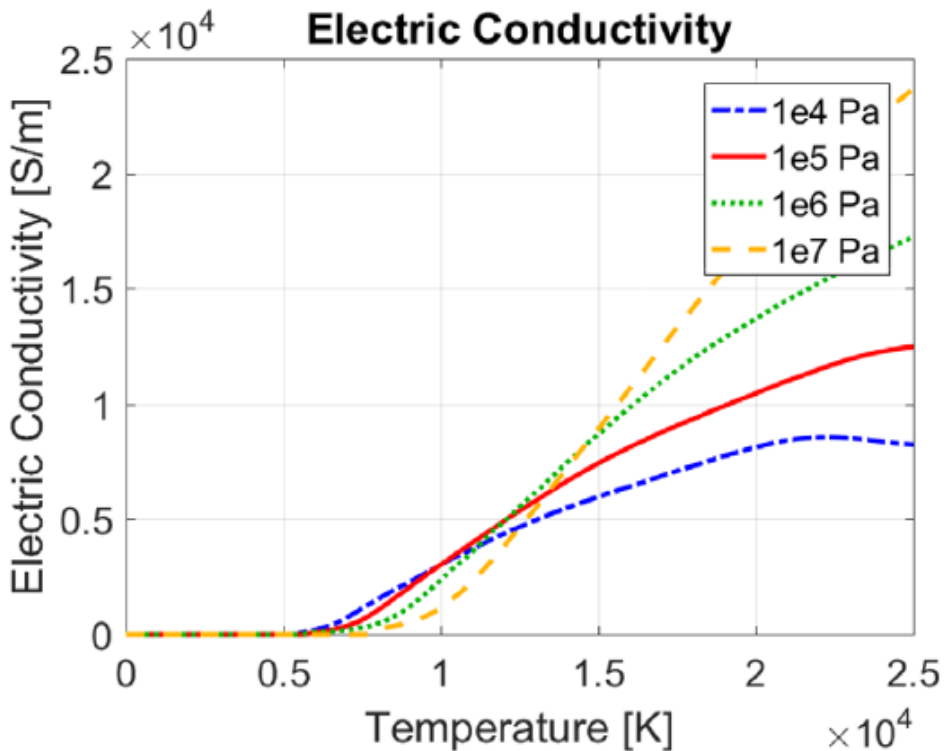
$$\partial_t \mathbf{B} + \nabla \times \mathbf{E} = 0$$

ARC DISCHARGE MODEL

Material properties

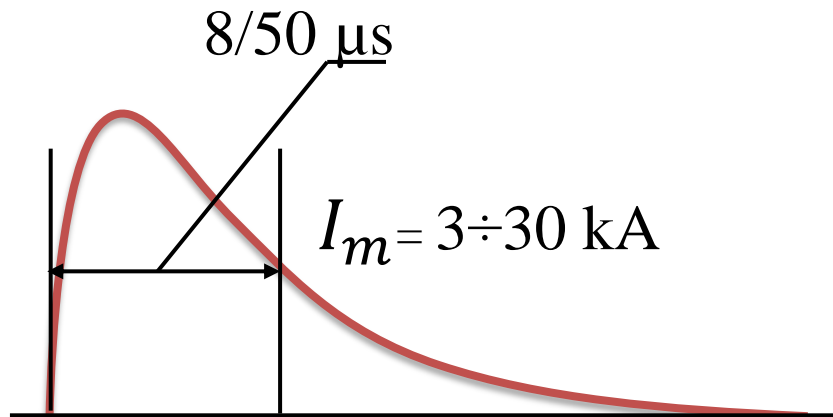
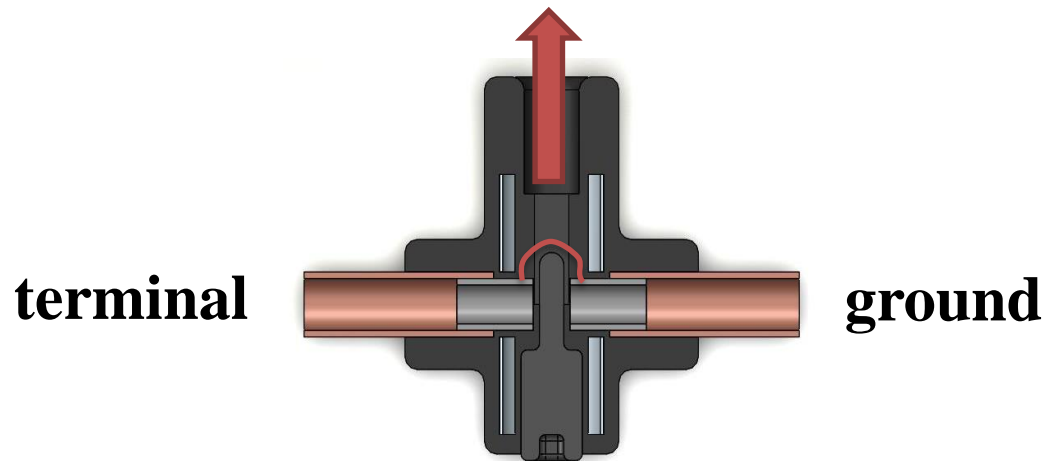
$$\sigma(p, T)$$

$$\rho(p, T)$$



ARC DISCHARGE MODEL

Electrodynamics



$$I(t) = \frac{I_{max}}{\eta} * (e^{-\frac{t}{\tau_1}} - e^{-\frac{t}{\tau_2}})$$

ARC DISCHARGE MODEL

Radiation transport

$$\mathbf{s} \cdot \nabla I_\nu(\mathbf{r}, \mathbf{s}) = \kappa_\nu [I_\nu^b(T) - I_\nu(\mathbf{r}, \mathbf{s})]$$

$$I_\nu^b(T) = \frac{2h}{c^2} \frac{\nu^3}{e^{h\nu/k_B T} - 1}$$

Two-band model

from zero up to $\lambda = 120$ nm

$$\alpha = 2000 \text{ m}^{-1}$$

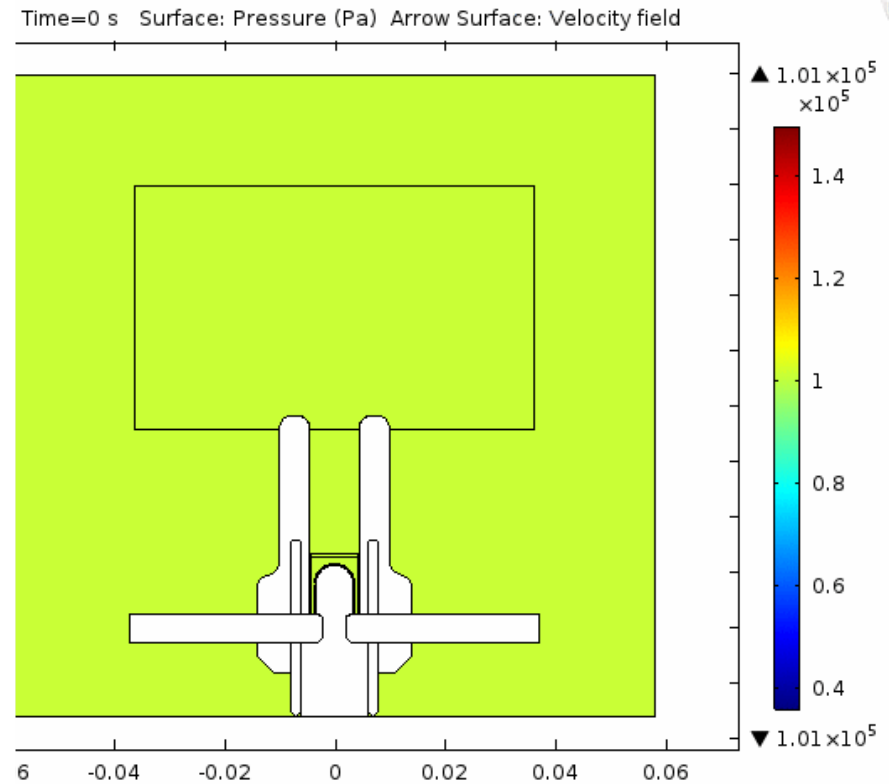
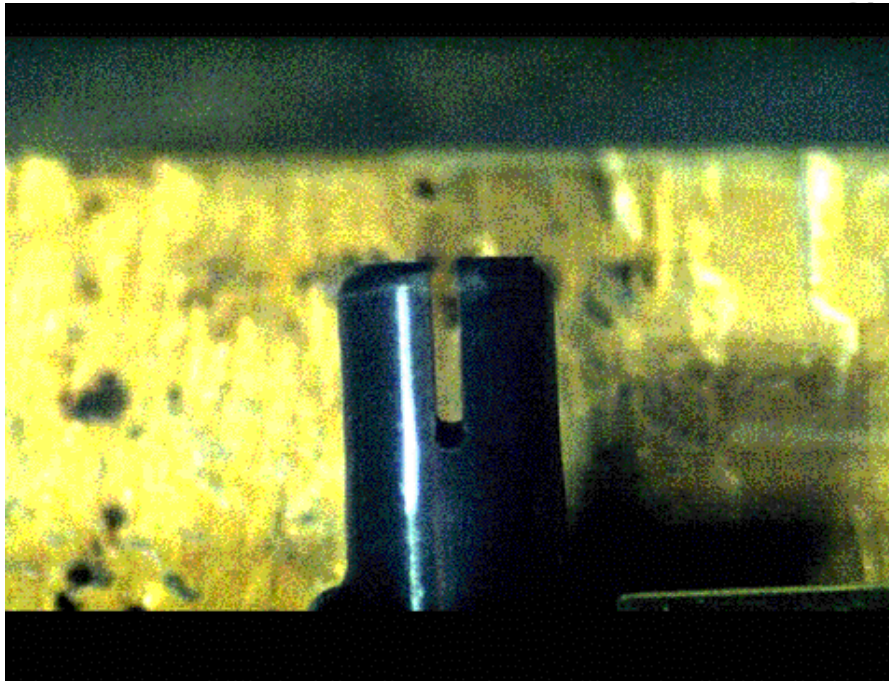
from $\lambda = 120$ nm up to $\lambda = 1$ mm

$$\alpha = 50 \text{ m}^{-1}$$

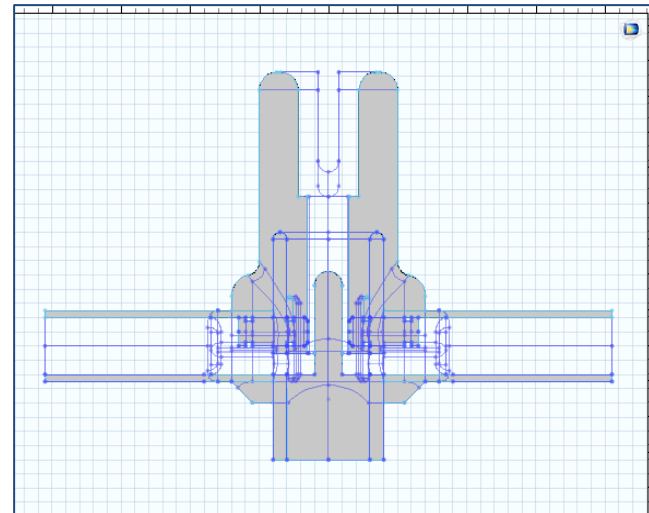
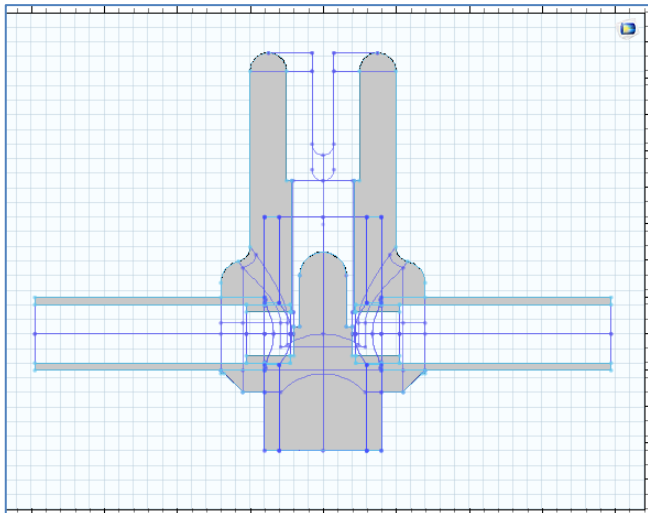
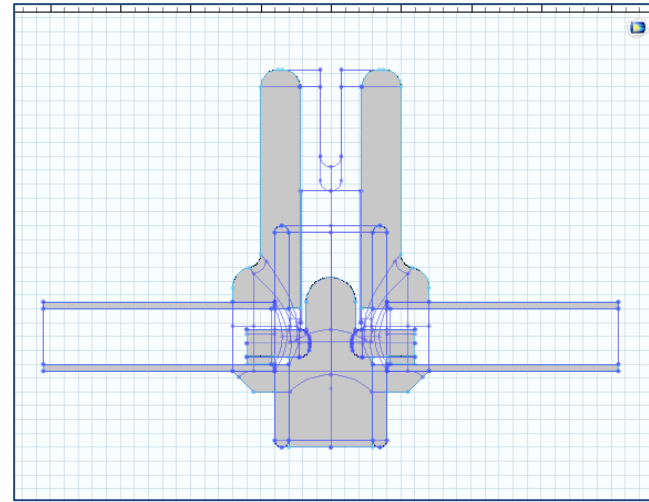
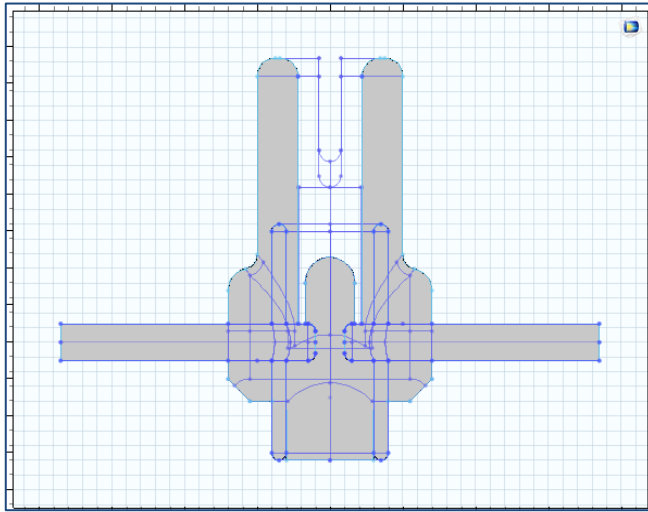
SIMULATION RESULTS



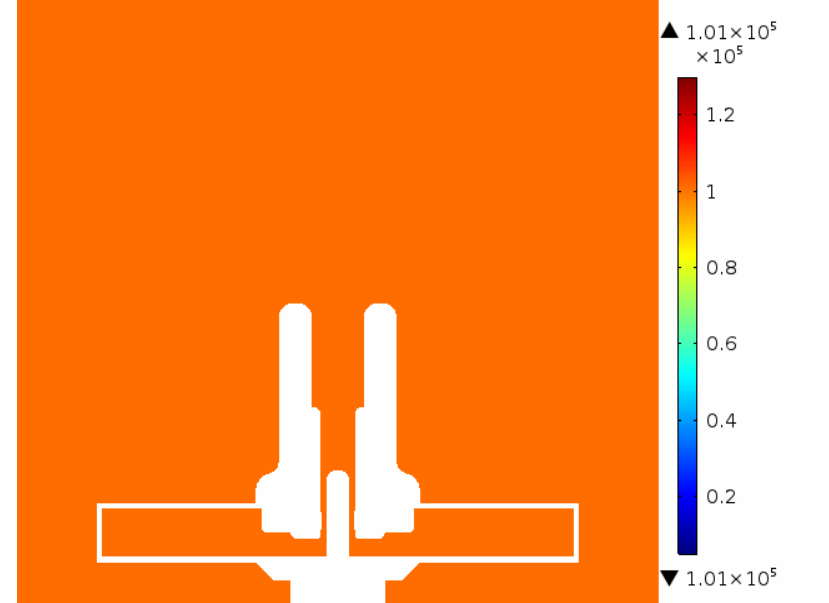
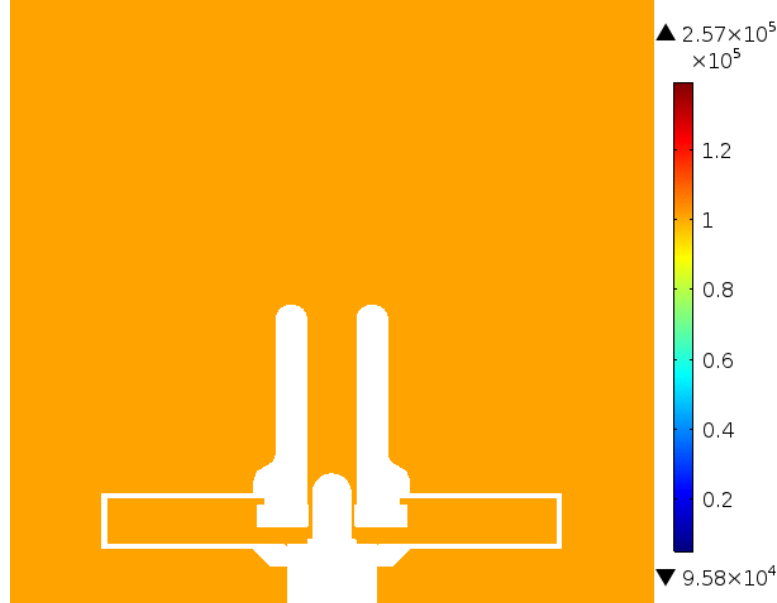
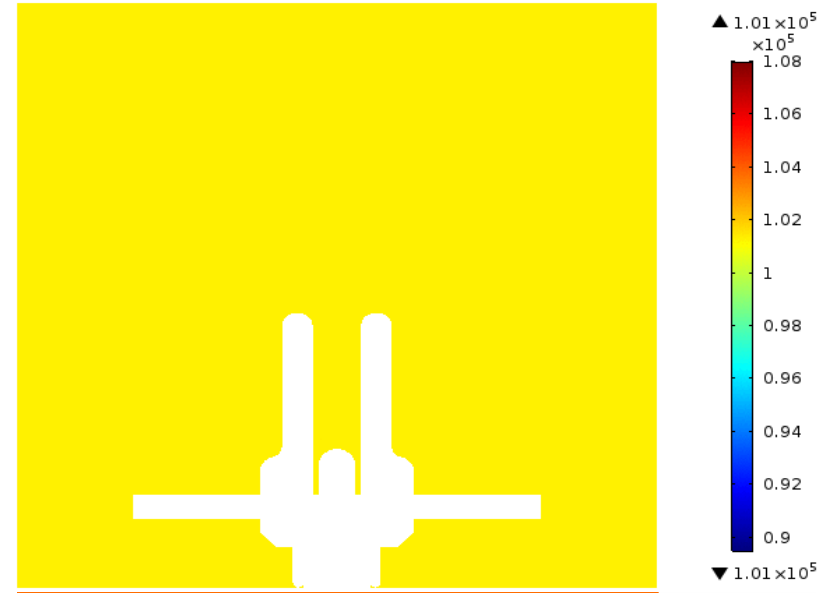
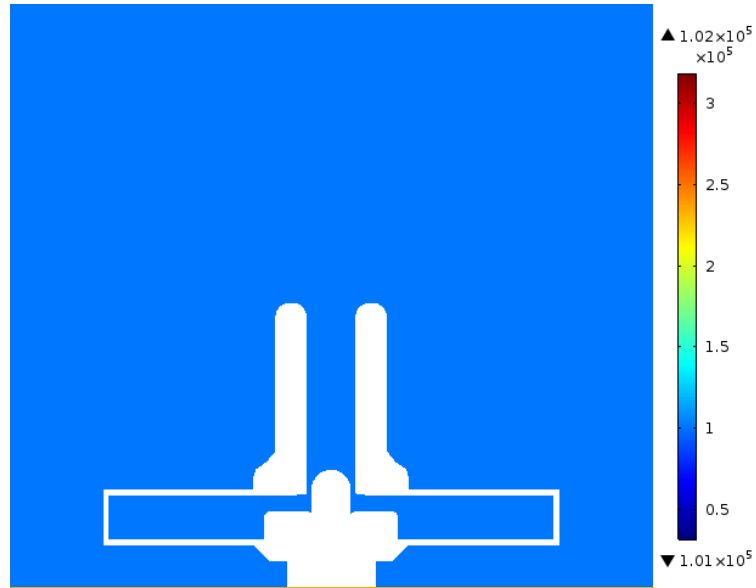
Fast-imaging record of plasma jet



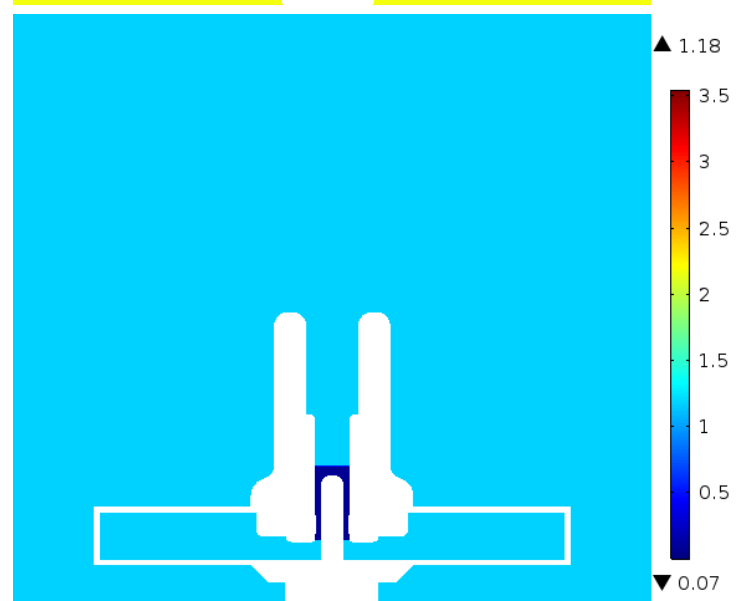
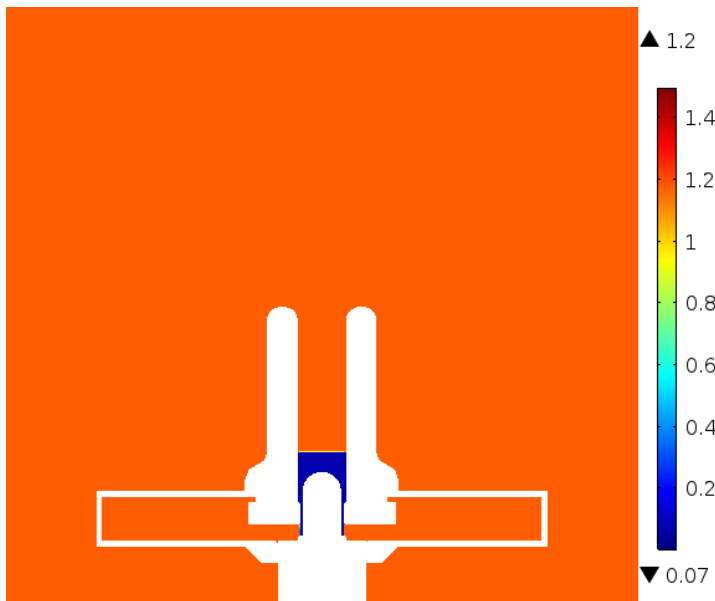
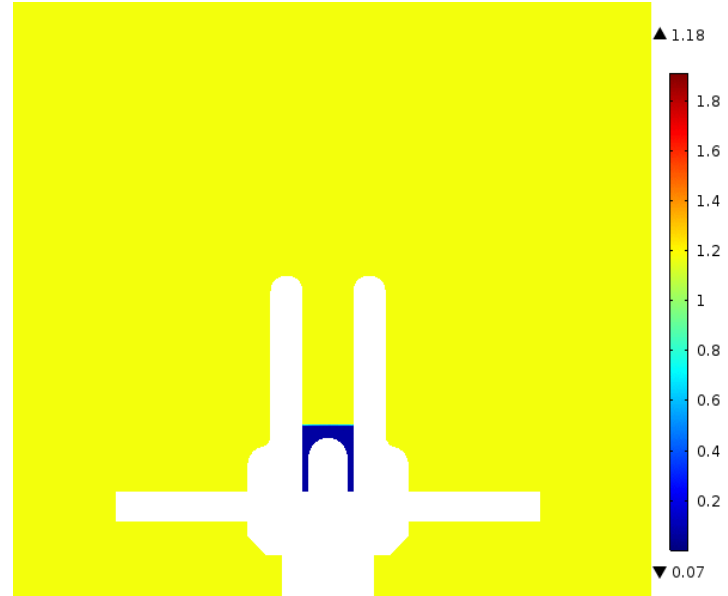
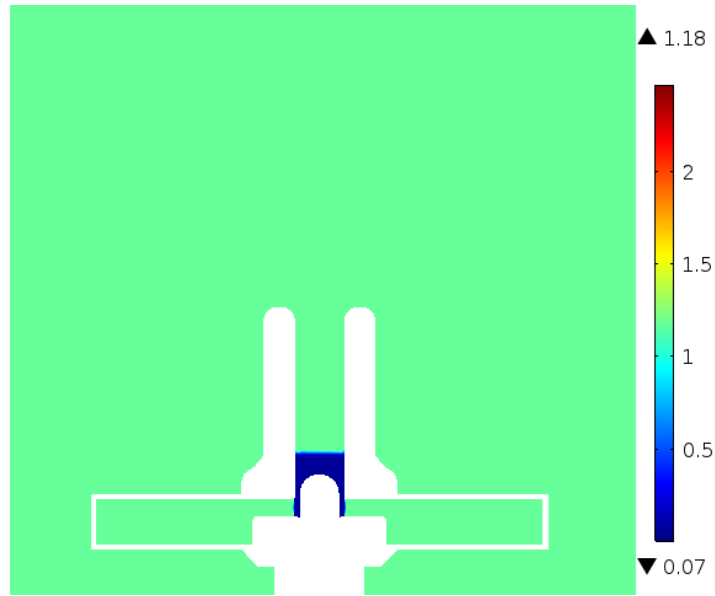
SIMULATION RESULTS



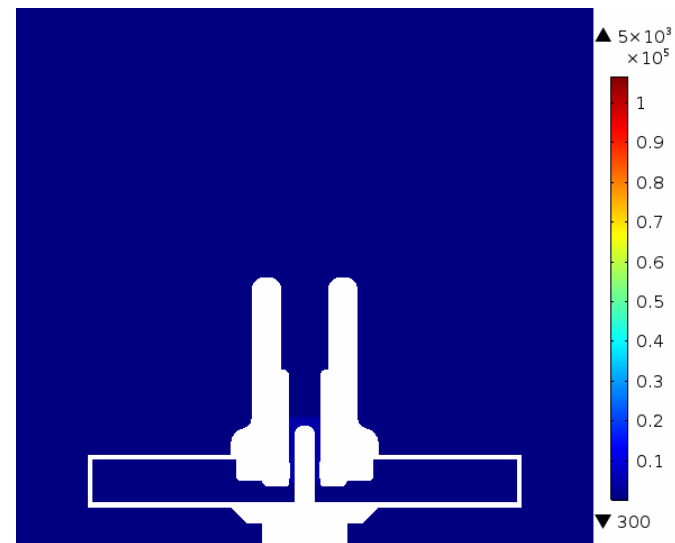
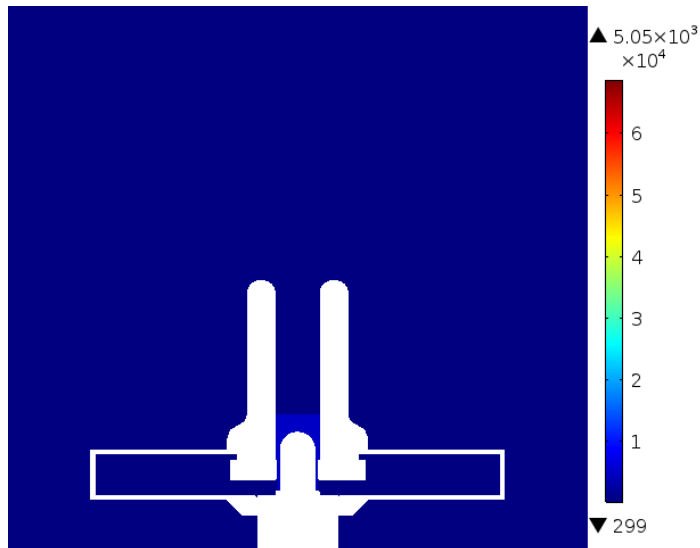
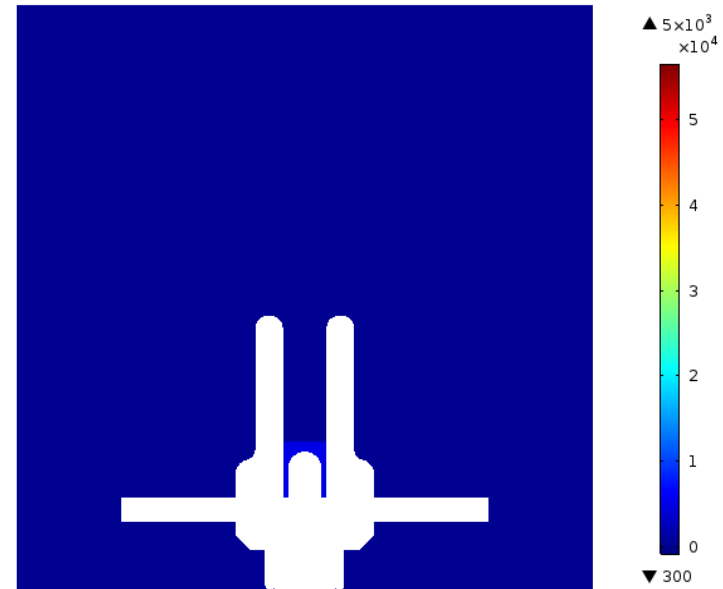
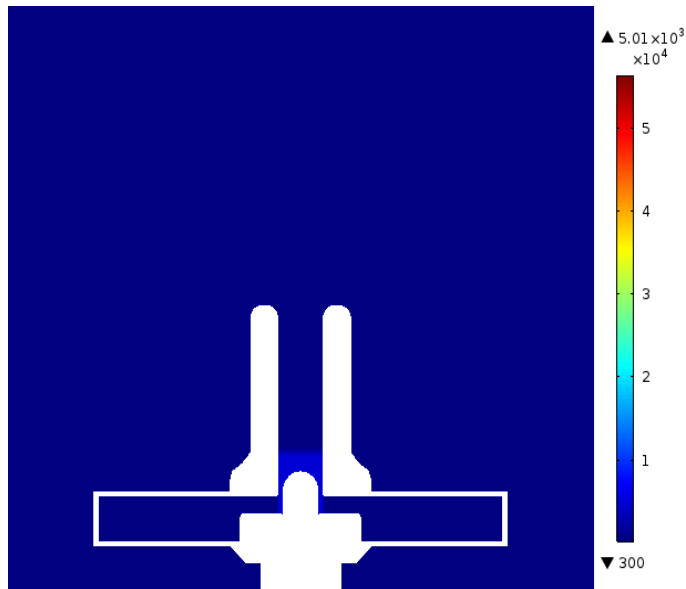
SIMULATION RESULTS: PRESSURE



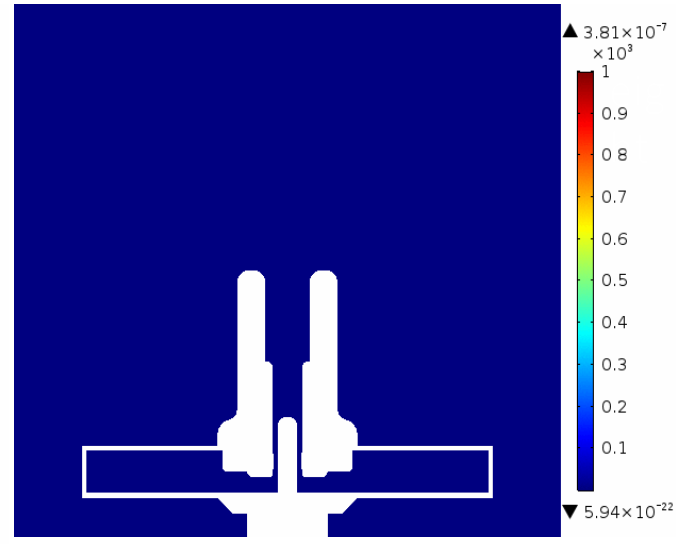
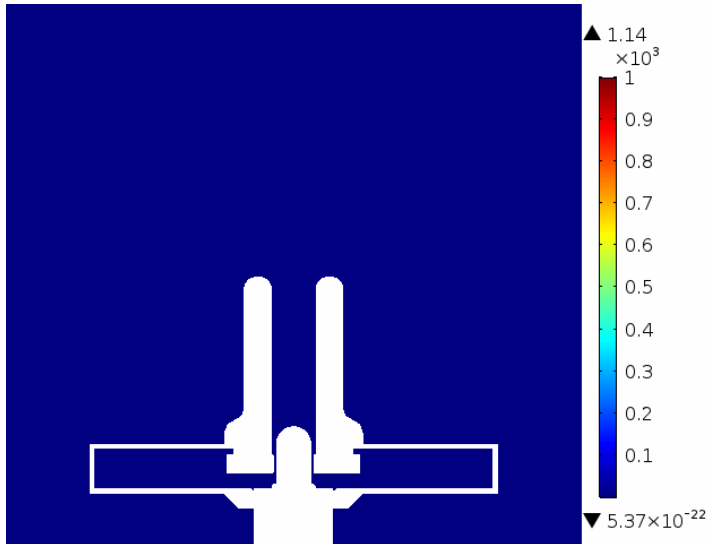
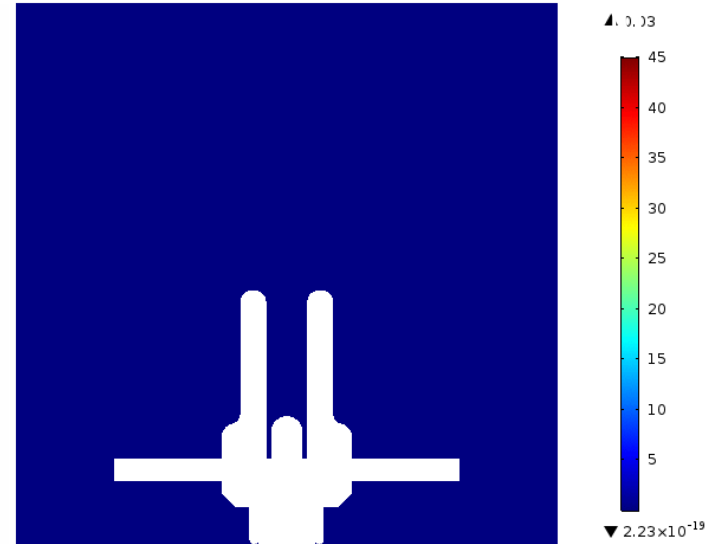
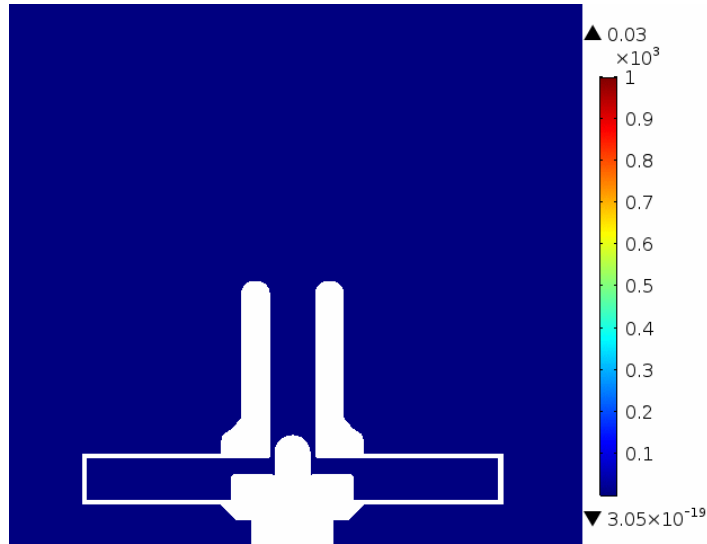
SIMULATION RESULTS:DENSITY



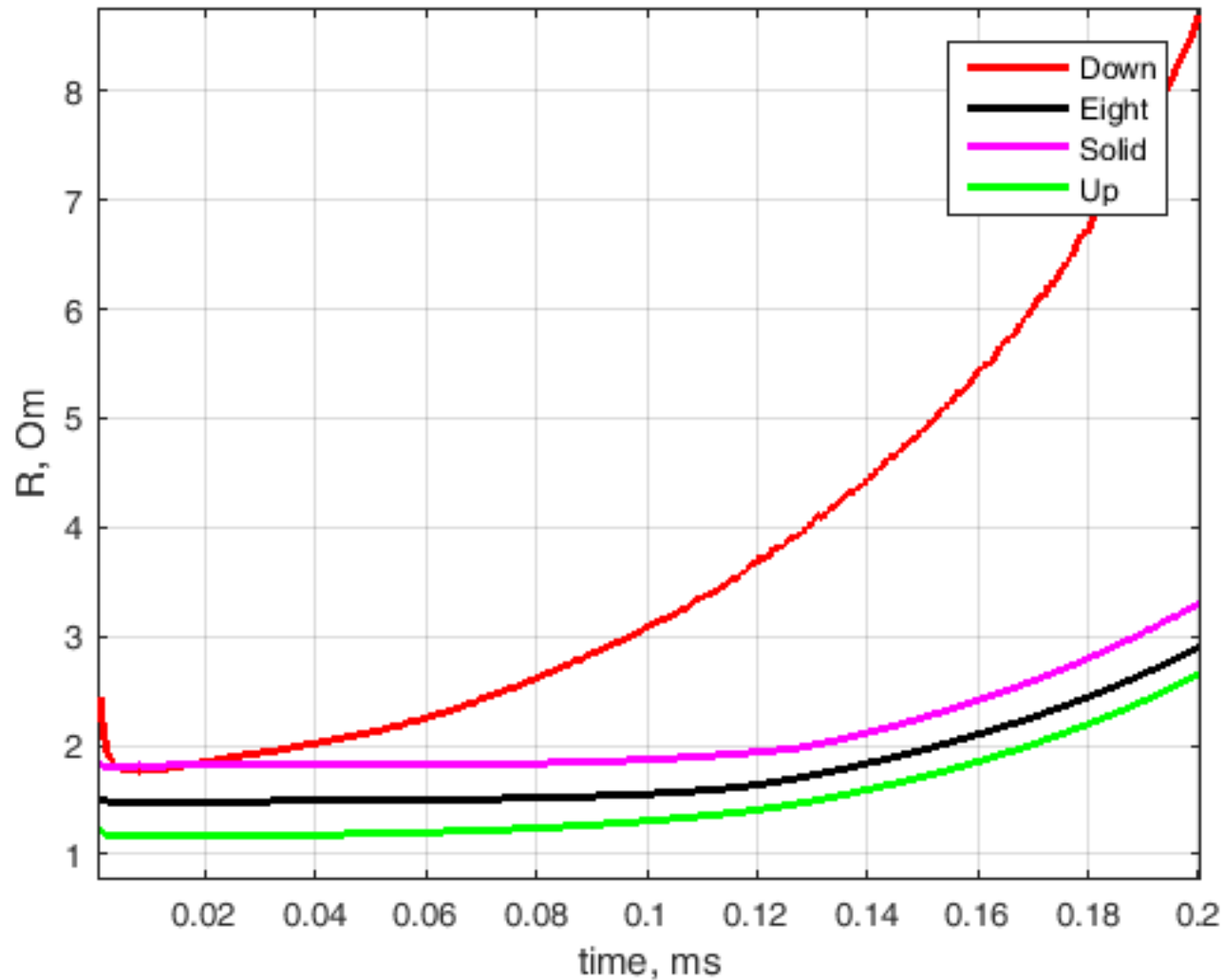
SIMULATION RESULTS: TEMPERATURE



SIMULATION RESULTS: VELOCITY



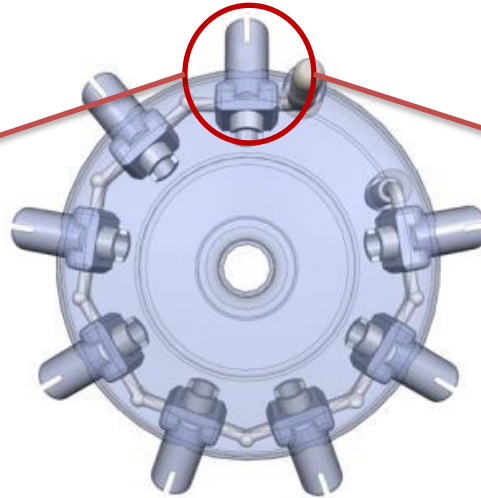
SIMULATION RESULTS



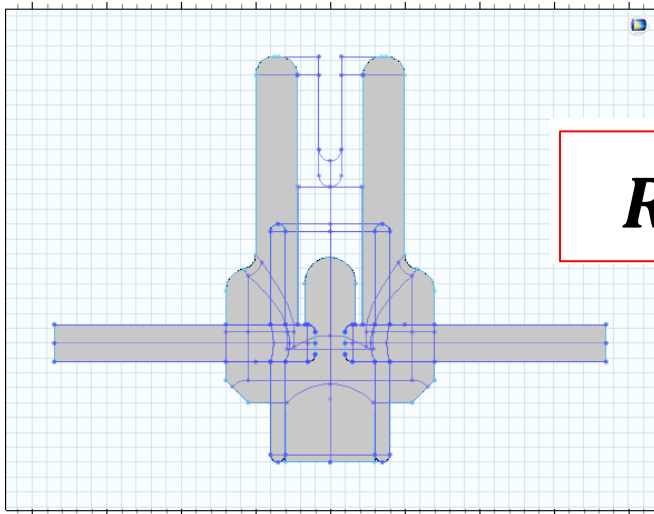
SIMULATION RESULTS



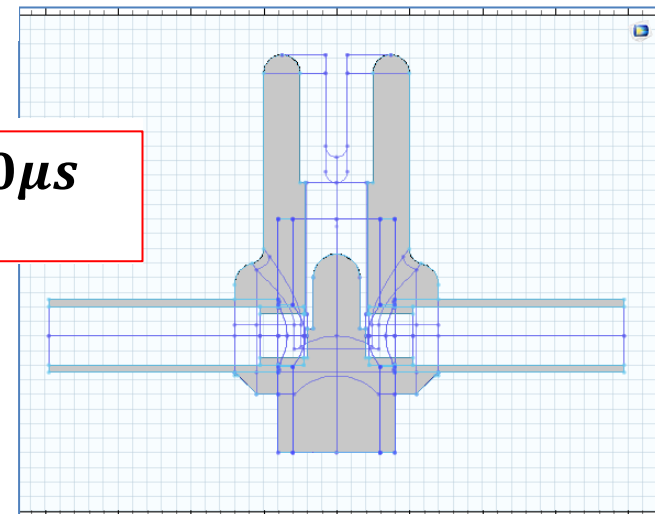
Type #1



Type #2



$$R_1^{t=200\mu s} < R_2^{t=200\mu s}$$



Type #1 is better than Type #2

CONCLUSIONS:

- **Predictions of certain type chamber performance are in qualitative agreement with experimental knowledge**
- **Numerical simulation is a promising design tool for future lightning protection devices**



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keeping the light

Thank you for your attention!