

**COMSOL
CONFERENCE**
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On Modeling and Simulation of Electroosmotic Micropump for Biomedical Applications

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Outline

- Micro-Total Analysis Systems
- Electroosmotic Micropump
- Non-Newtonian Fluids
- Governing Equations
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- Simulated Model
- Verification
- Results
- Conclusion



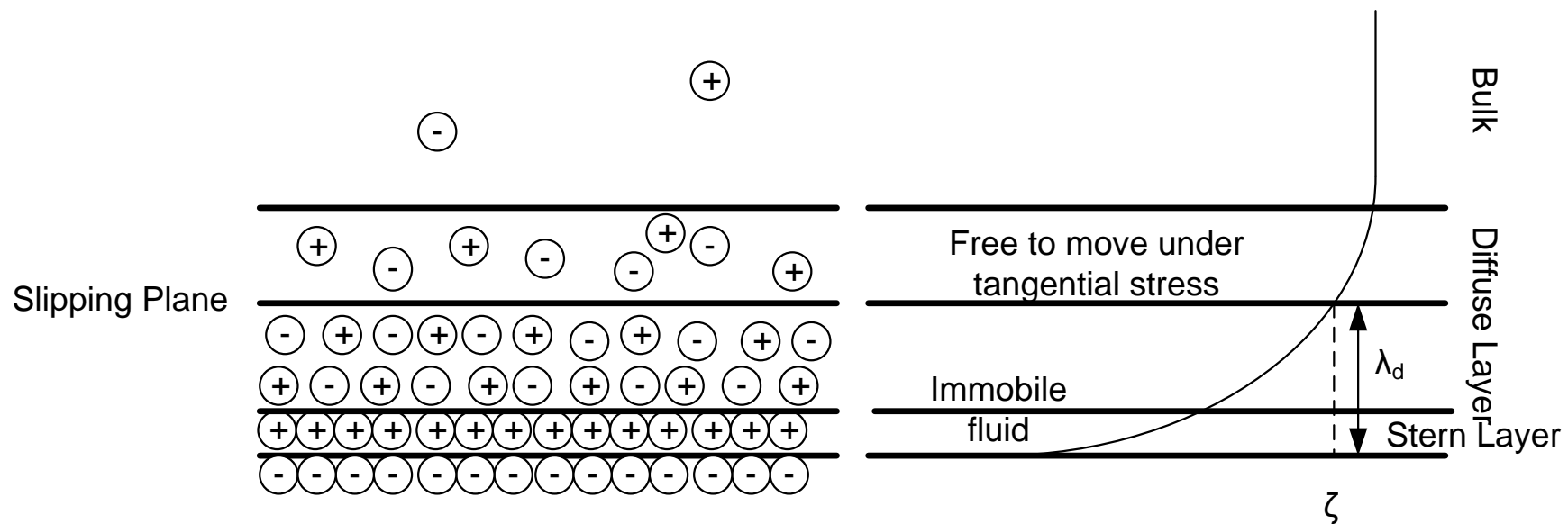
Micro Total Analysis Systems (μ TAS)

- Usage : Medical Diagnostics, Drug Delivery, DNA Analysis, Toxicity Monitoring
- Lab on a Chip and usage of microfluidics
- Require
 - Small volume of fluids
 - Parallel processing (multiple of samples at once)
 - Low Power consumption
- Micropumps for control fluid flow inside the channels
- Fluid channels height or depth of $1\mu\text{m}$ - $500\mu\text{m}$



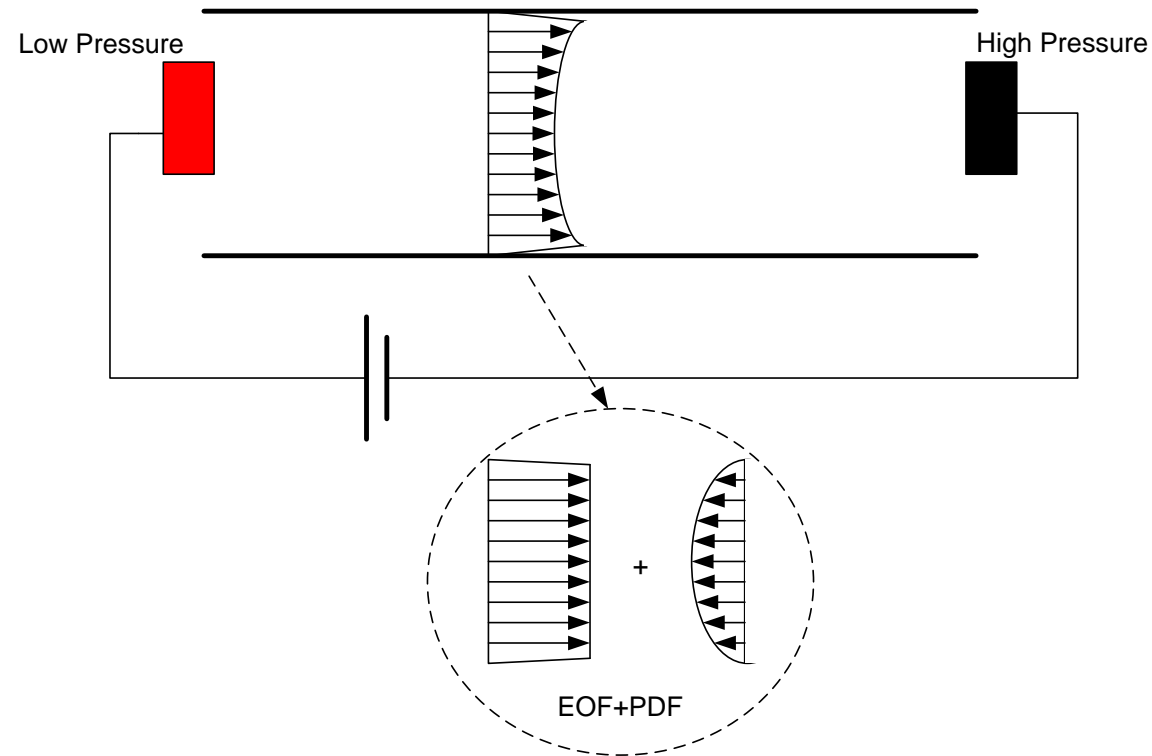
Electroosmotic Micropump

- A non-mechanical micropump (no moving parts)
- The Fluid motion is induced by an applied electric potential across the channel.
- Electric Double Layer (EDL)



Electroosmotic Micropump

- Electroosmotic Flow and Pressure Driven Flow



Non-Newtonian Fluid

- It is a fluid where its viscosity is not constant with applied sheer stress.
- Shear thinning
 - Viscosity decreases with high shear strain
- Newtonian
 - Viscosity is constant with shear strain
- Shear Thickening
 - Viscosity increases with high shear strain

Blood is considered a shear thinning non-Newtonian fluid.



Governing Equations

Navier-Stokes Equations

$$\rho(\mathbf{u} \cdot \nabla)\mathbf{u} = -\nabla P + \mu \nabla^2 \mathbf{u} + \mathbf{F}$$

Reynolds number $< 1 \Rightarrow$ creeping flow and inertial terms could be neglected.

$\rho_e = 0$ at the bulk $\Rightarrow F=0$

$$0 = -\nabla P + \mu \nabla^2 \mathbf{u}$$

Electroosmotic Slip Velocity

$$\mathbf{u} = \mu_{eo} E = \frac{\varepsilon_0 \varepsilon_r \zeta}{\mu}$$

Continuity Equation

$$\nabla \cdot \mathbf{u} = 0$$

Carreau model for non-Newtonian fluid

$$\mu = \mu_\infty + (\mu_0 - \mu_\infty) [1 - (\lambda \dot{\gamma})^2]^{\frac{n-1}{2}}$$

Gauss Law

$$\mathbf{E} = -\nabla V$$

$$\nabla \cdot \mathbf{D} = \rho_e$$

$$\mathbf{D} = \varepsilon_0 \varepsilon_r \mathbf{E}$$



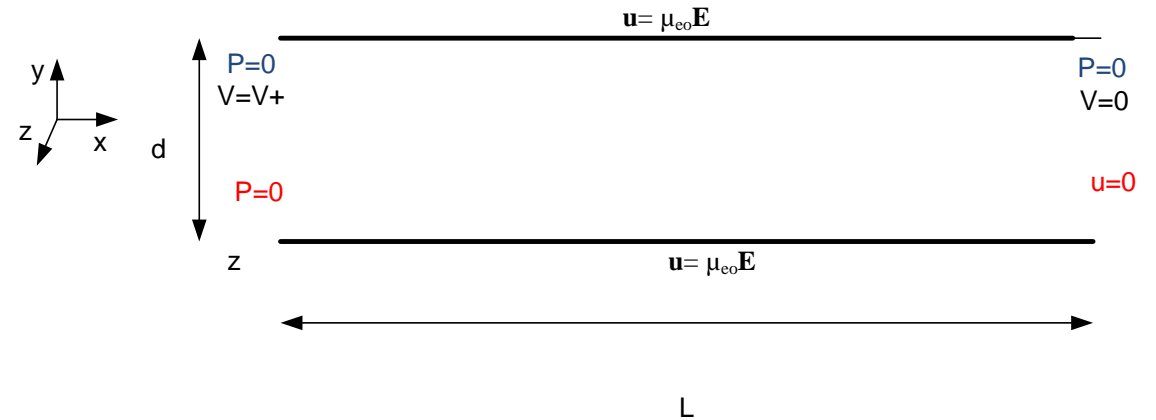
COMSOL Modeling

- Coupled Physics used are:

- Creeping Flow
- Electrostatics

- Boundary Conditions:

- Creeping Fluid Flow
 - Maximum Velocity (free flow boundary condition)
 - Maximum Pressure
 - Electroosmotic wall velocity
- Electrostatics



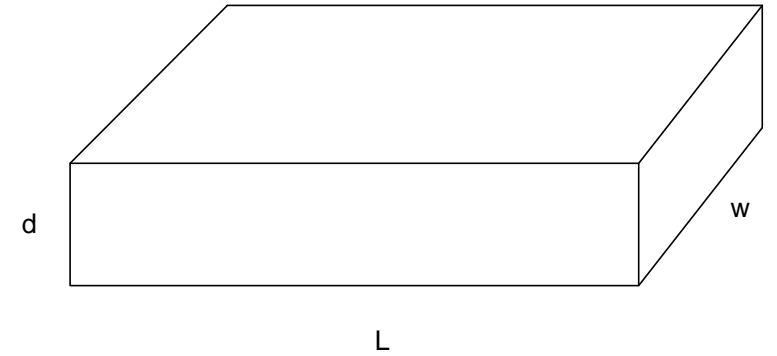
Simulated Model

- For a Planar Electroosmotic Micropump
 - High voltage is required for an applicable pressure and volume flow rate.

$$\Delta P = \frac{-12\varepsilon_0 \varepsilon_r \zeta \Delta V}{d^2}$$

$$\Delta Q = u_{wall} A = \frac{-\varepsilon_0 \varepsilon_r \zeta \Delta V}{\mu L} wd$$

- To maximize the pressure with the same voltage (minimize d)
However to maintain the same Q (L has to be reduced)
- The velocity of different combination of the d and L will be examined

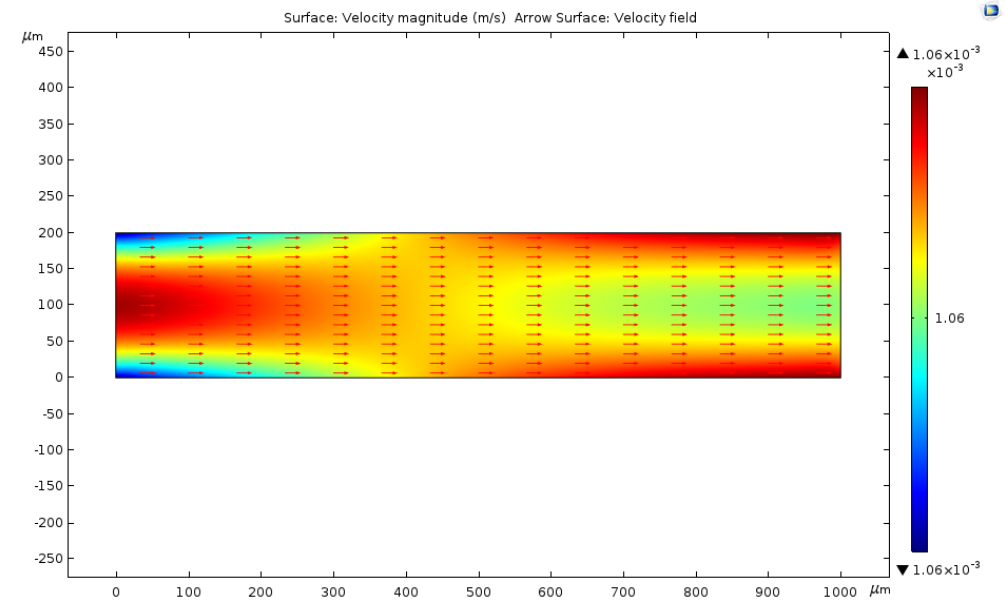
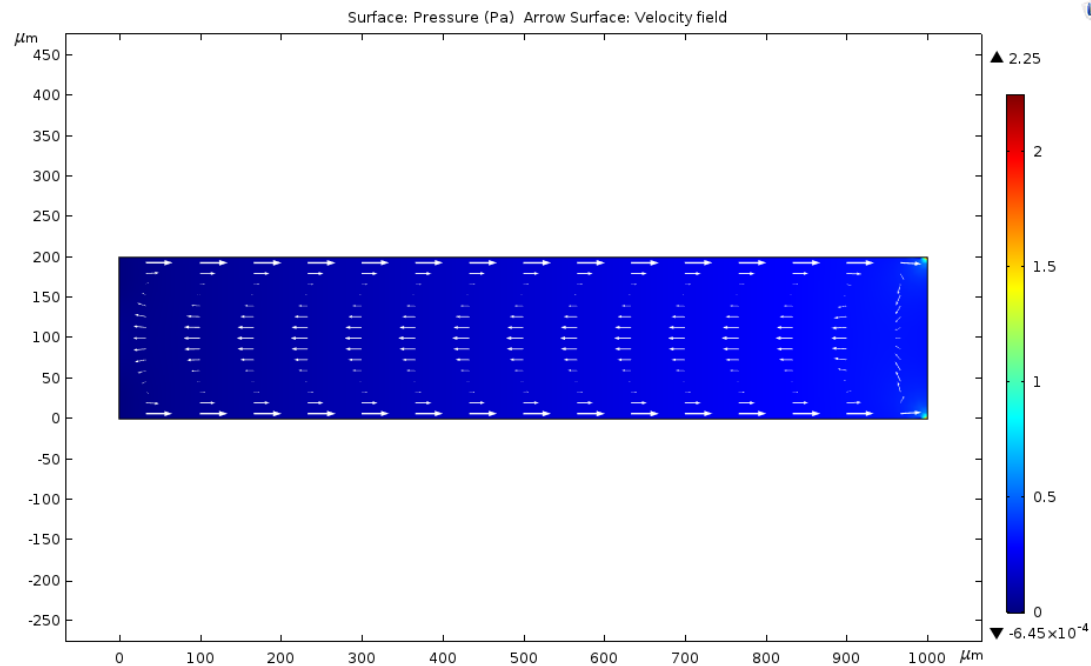


Verification

- Analytical Verification:

A Planar Electroosmotic Micropump using water as the working fluid.

$L=1000\ \mu\text{m}$ $d = 200\ \mu\text{m}$ with an applied 30 V



Data

- Variations in d and L were as follows:

$d(\mu\text{m})$	160	80	40	20	10	5
$L(\mu\text{m})$	3200	1600	800	400	200	100

- A constant applied voltage of 20 V
- Blood Carreau Law values are:

Parameter	Value
μ_{∞}	0.056 Pa.s
μ_0	0.00345 Pa.s
λ	3.313 s
n	0.3568

Parameter	Value
ρ	998 Kg/m ³
ϵ_r	78.5
ζ	-50 mV



Results

- Variations in d and L were as follows:

$d(\mu\text{m})$	160	80	40	20	10	5
$L(\mu\text{m})$	3200	1600	800	400	200	100
Velocity ($\mu\text{m}/\text{s}$)	3.88E-6	7.76E-6	15.5E-6	31E-6	62.1E-6	124E-6



Conclusions

- The Assumption of using the electroosmotic velocity as a boundary condition was appropriate.
- For the same voltage, the velocity can be increased by decreasing the length of the channel
- Pressure can also be increased with the same voltage by decreasing the depth of the channel

