

Level set based Topology Optimisation of Convectively Cooled Heat Sinks

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 - ▣ 2D Low conductivity solid
 - ▣ 2D Flow with minimum Viscous dissipation
 - ▣ Combined Thermal Compliance & Viscous Dissipation
 - ▣ 3D High conductivity solid
- Conclusions

Introduction to Topology Optimisation

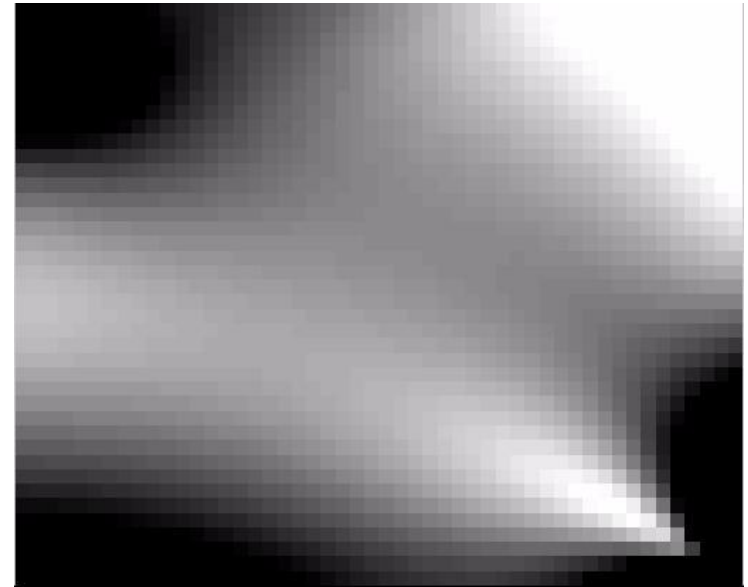
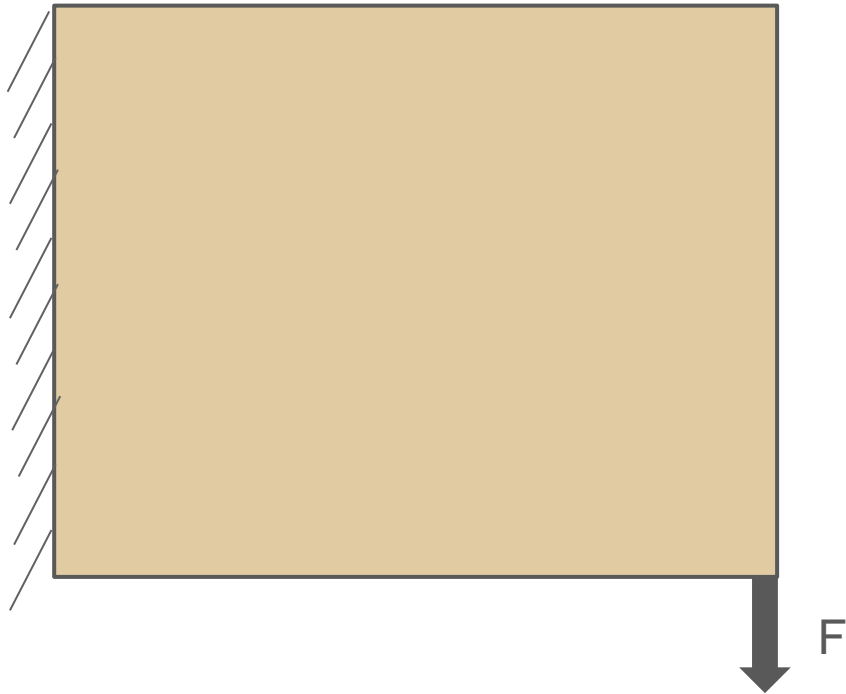
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- Topology optimisation is a mathematical approach that **optimises material layout** for a given **set of constraints** meeting prescribed set of performance **objectives**.
- Concept is started for structural mechanics problems (by Bendsoe & Kikuchi) but now it finds application in Fluids, Acoustics, Electromagnetics, Optics etc.
- There are different methods for Topology optimisation they are,
 - ▣ Density Method
 - ▣ Level set methods
 - ▣ Topological derivative
 - ▣ Phase field method and
 - ▣ Evolutionary approaches.

Introduction to Topology Optimisation

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Cantilever Subjected to Tip Load



Ref: O Sigmund, A 99 line Topology optimisation code written in Matlab, Struc & Multidisc Optim 2001

Objective: Maximum stiffness or minimum compliance [$F^T U$]

Constraints: 30% of material volume
 $KU = F$ (Governing equation)

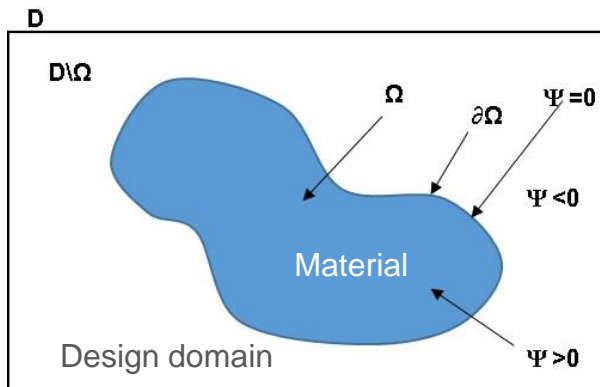
■ Solid

□ No material/ Void

TO with the Level-set method

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- Level set method is a concept developed for studying moving boundaries
- Major steps in Level-set TO
 - LSF parametrization (Polynomial shape function or Radial Basis function)
 - Mapping of geometry into mechanical model, Ersatz material, XFEM, Conforming mesh
 - Optimization strategy (Hamilton Jacobi solver or Mathematical programming)



$$\psi = \begin{cases} = 0 \forall x \in \partial\Omega \text{ (boundary)} \\ > 0 \forall x \in \Omega^+ \text{ (solid region)} \\ < 0 \forall x \in \Omega^- \text{ (void region)} \end{cases}$$

Hamilton-Jacobi equation

$$\frac{\partial\psi}{\partial t} = -v|\nabla\psi| - \omega g$$

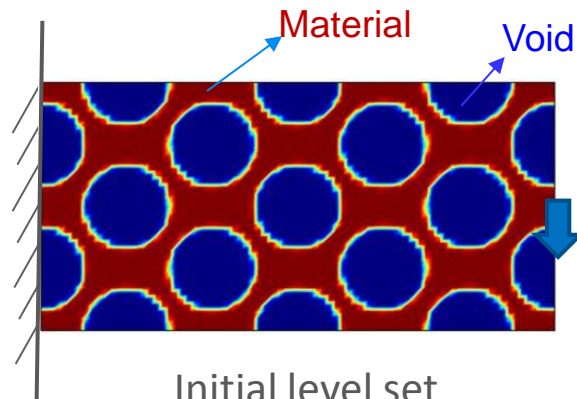
Velocity of propagation

Nucleation of new holes

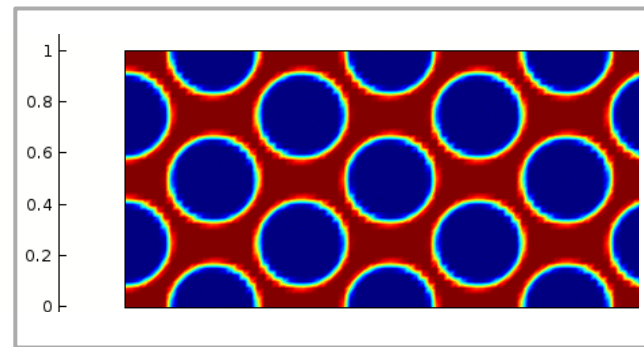
TO with the Level-set method

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- Advantages
 - ▣ Accurate prediction of interphases
 - ▣ No pressure diffusion in fluid flow problems (in XFEM & Conformal Mapping)
- Compared to Density method convergence of Level-set method is slow



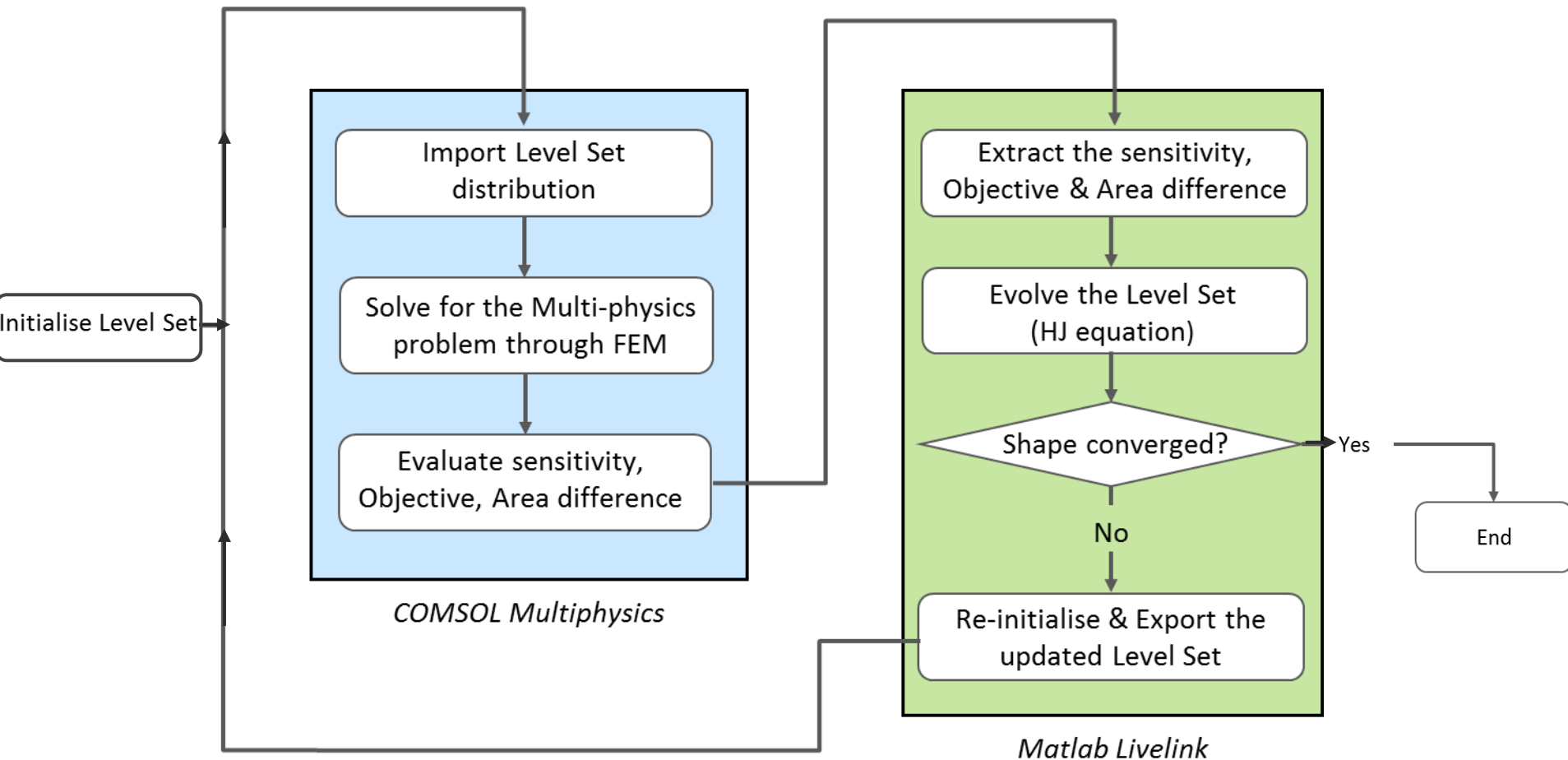
Initial level set
distribution on cantilever
beam



Optimised Shape

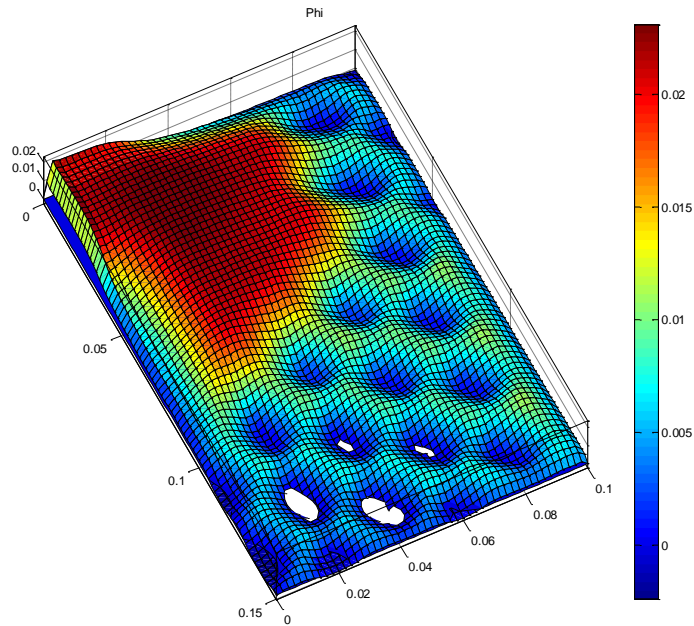
Level Set TO - Numerical Implementation

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Re-initialisation of Level sets

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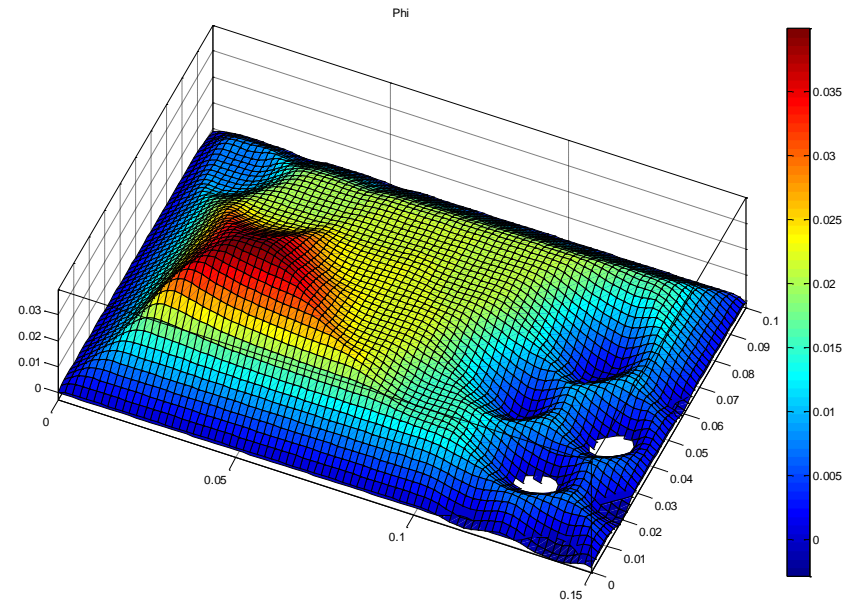
Level Set after few TO iterations,
before Re-initialisation

Eikonal Equation

$$\frac{\partial \psi}{\partial t} + w \cdot \nabla \psi = S(\psi_0)$$

$$w = S(\psi_0) \frac{\nabla \psi}{|\nabla \psi|}$$

where S is smoothed sign function



Level Set after
Re-initialisation

Heat sink Design: Problem Formulation

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Objective: Thermal Compliance: $\min \int_{\Omega} k_{gam} * [(\nabla T)^2] d\Omega$

Viscous Dissipation: $\min \mu \int_{\Omega} \left(\frac{\partial u_i}{\partial x_j}\right)^2 d\Omega$

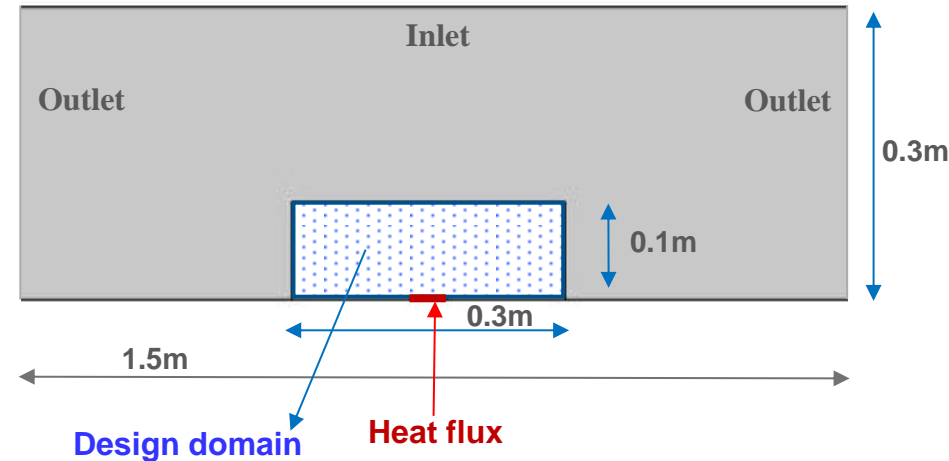
Governing Eqns:

$$\rho C_p (u \cdot \nabla) T = \nabla \cdot (k \nabla T) + Q$$

$$(\nabla \cdot \mathbf{u}) = 0$$

$$(\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p + \mu \{ \nabla^2 \mathbf{u} + (\nabla \mathbf{u})^T \} - \alpha \mathbf{u}$$

$$H(\Psi) \mathbf{u} = 0$$



Variable	Expression
K_{gam}	$(K_s - K_f) * H + K_f$
C_{pgam}	$(C_{p_s} - C_{p_f}) * H + C_{p_f}$
ρ_{gam}	$(\rho_s - \rho_f) * H + \rho_f$
α	$(\alpha_{max} - \alpha_{min}) * H + \alpha_{min}$

Material: $k_f/k_s=0.001$ High conductivity solid
 $k_f/k_s=0.1$ Low conductivity solid

Heat flux =700W/m²

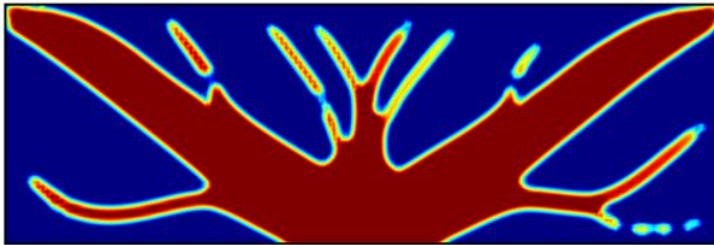
Reynolds number=600

Constraints: 40% volume constraint for solid material

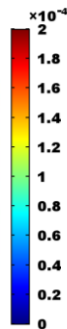
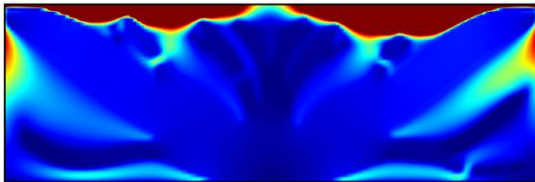
High conductivity solid- Results

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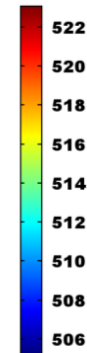
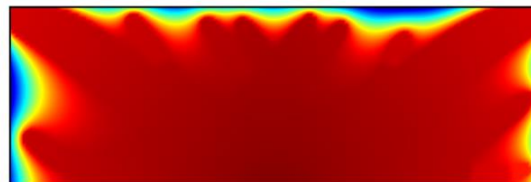
Design variable



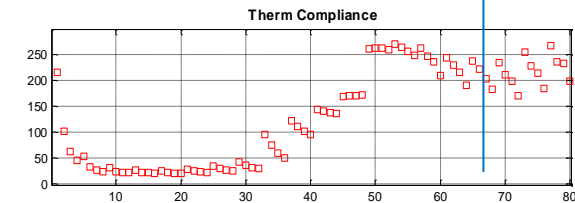
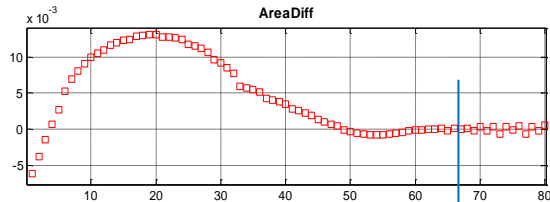
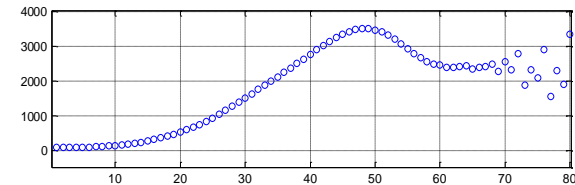
Velocity (m/s)



Temperature (K)



Lagrange Multiplier



Iteration = 67

Area Difference= 2.4384×10^{-5}

Thermal Compliance= 202.51

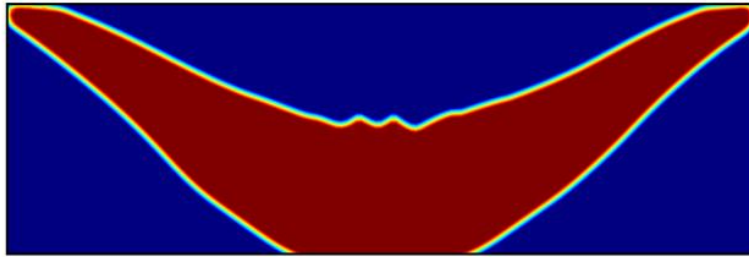
Max Temperature=523.10K

- Heat sink has tree like/Dendritic shape
- Temperature is uniformly distributed throughout the design domain

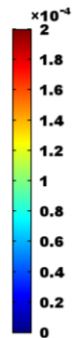
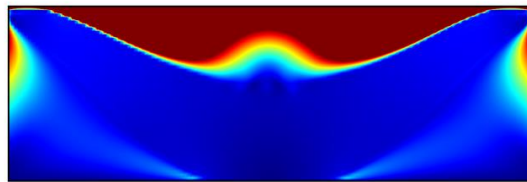
Low conductivity solid- Results

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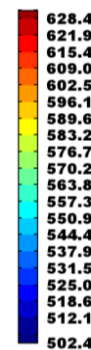
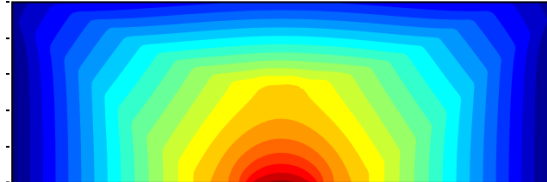
Design variable



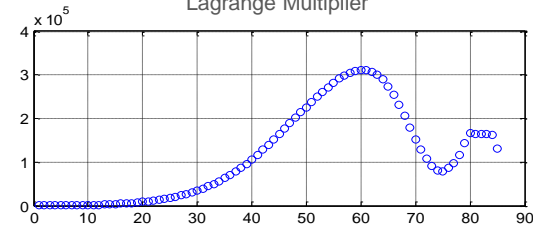
Velocity (m/s)



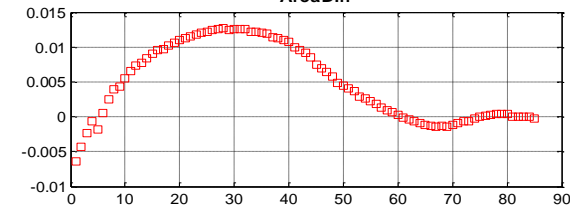
Temperature (K)



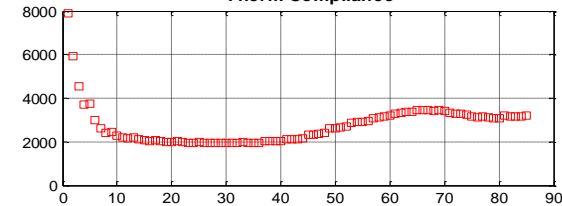
Lagrange Multiplier



AreaDiff



Therm Compliance



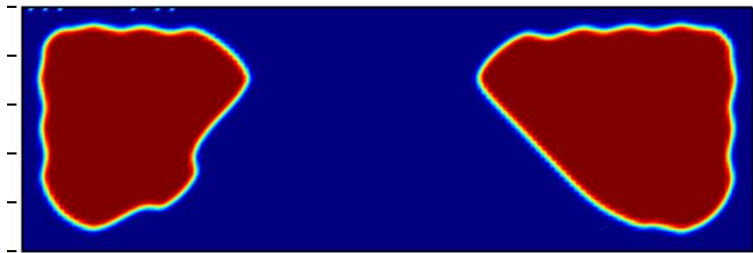
Iteration = 83
Area Difference= 6.5897e-07
Thermal Compliance= 3154.40
MaxTemperature=631.59 K

- Secondary branches have disappeared for low conductivity solid

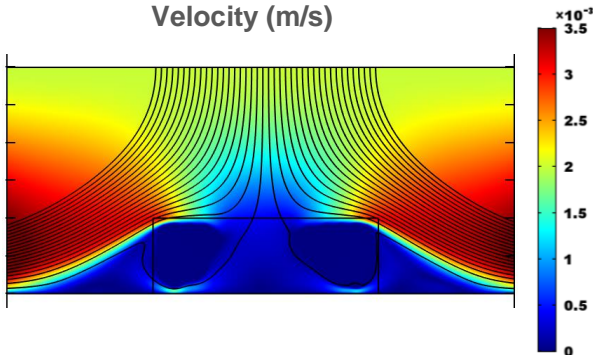
Minimum Viscous Dissipation - Results

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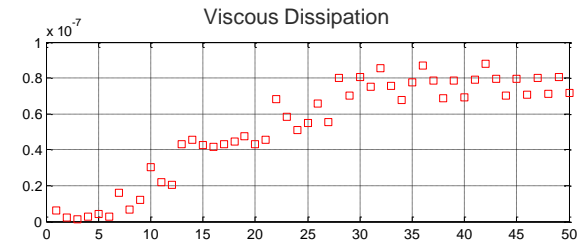
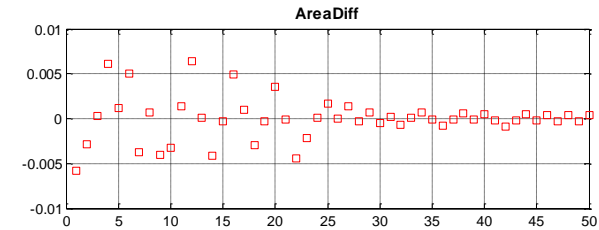
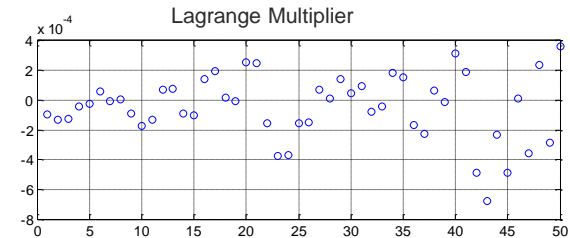
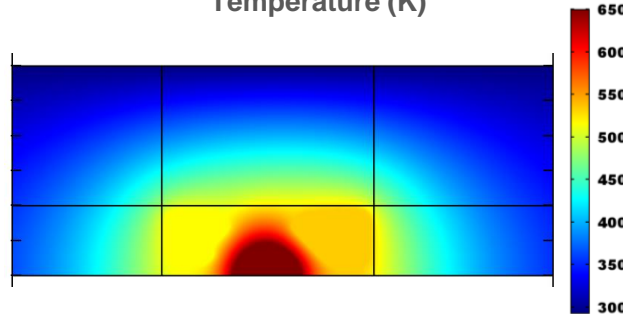
Design variable



Velocity (m/s)



Temperature (K)



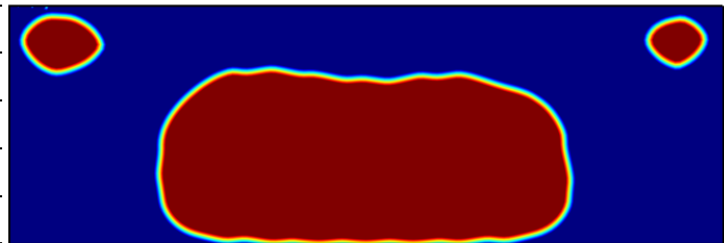
Iteration:43
Area Difference= 2.3×10^{-4}
Viscous Dissipation= 7.9642×10^{-8}

- Viscous Dissipation objective leads to a shape guiding the flow with least resistance

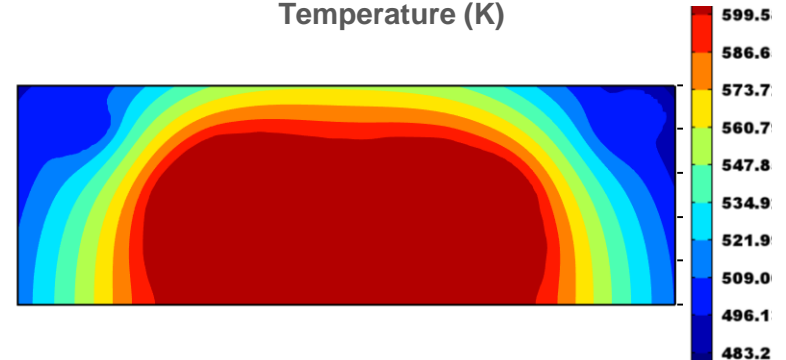
Combined Thermal Compliance and Viscous Dissipation

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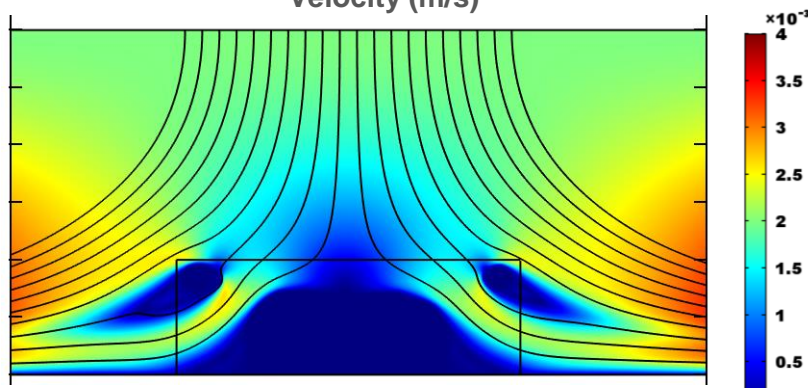
Design variable



Temperature (K)



Velocity (m/s)

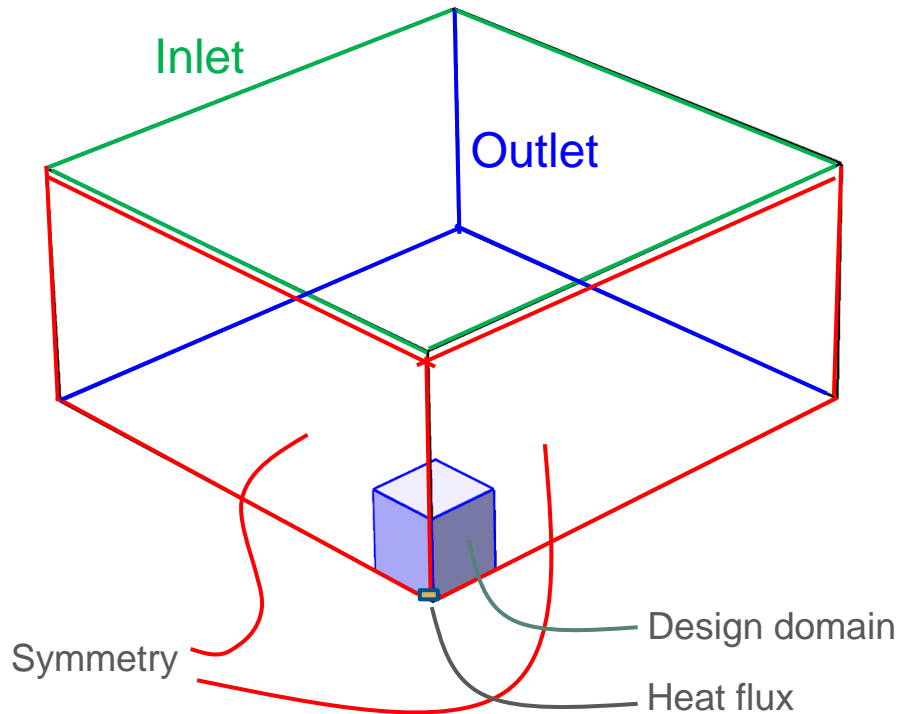


	Thermal Compliance (WK/m)	Viscous Dissipation (N/s)
(F1,F2)		
(0, 1)	14197.6 ↓	7.9642e-8 ↑
(1e-9,1)	2357.1 ↓	8.8307e-8 ↑

- Combined objective, tries to minimize both Thermal Compliance & Viscous Dissipation.

Three dimensional Heat sink design

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Computational Domain

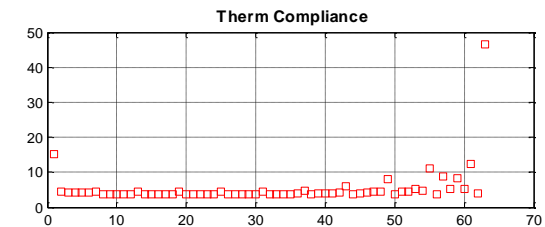
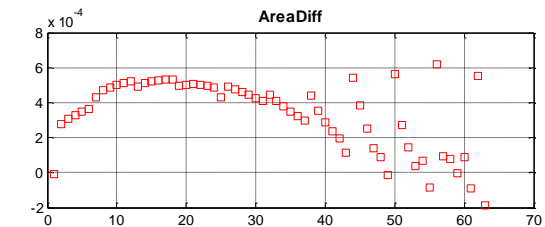
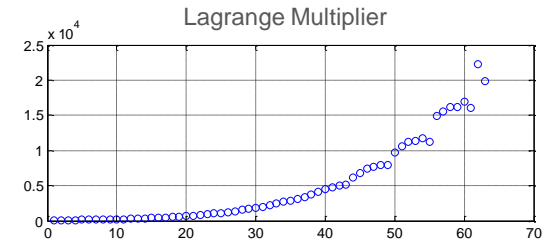
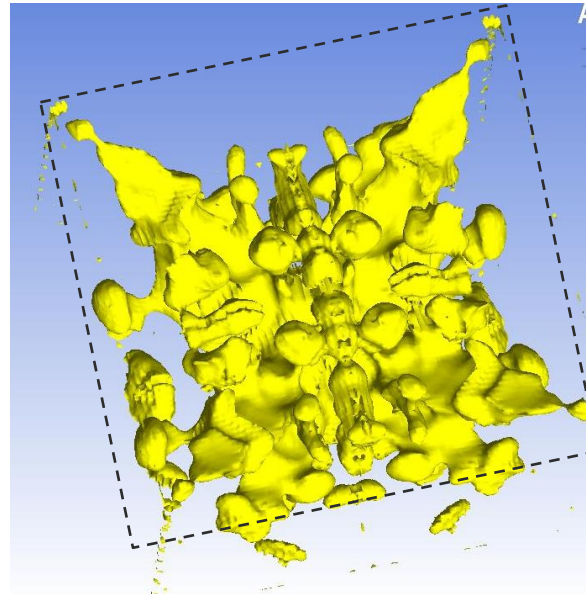
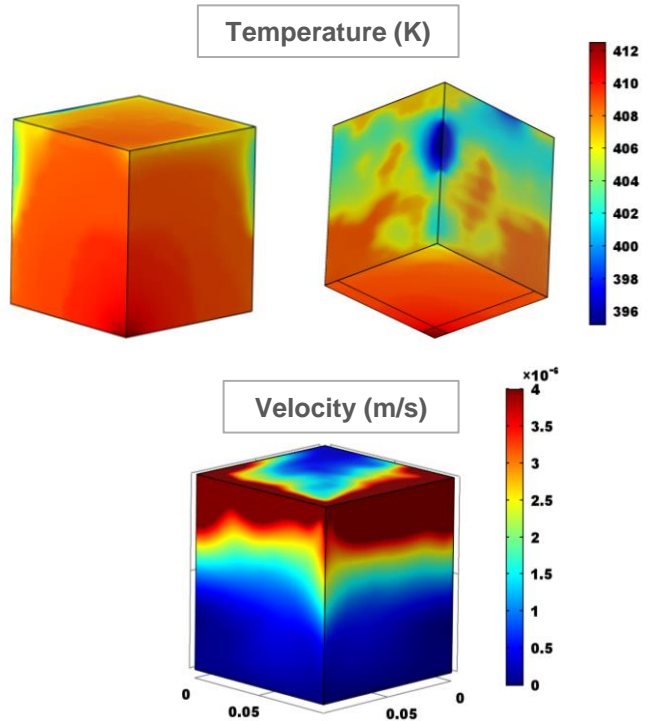
- Design domain of size $0.1 \times 0.1 \times 0.1 \text{m}$ is discretised with $43 \times 43 \times 43$ hexahedral cells
- Material: $K_f/K_s = 0.001$ (High conductivity solid)
- Heat flux = 1000W/m^2
- $Re = 8$ (vel = $4 \times 10^{-5} \text{m/s}$)

Objective: Minimizing the thermal compliance

Constraints: 25% volume constraint for solid material

Three Dimensional High conductivity solid - Results

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Therm Compliance=8.2257
Max Temp= 412.519 K

- Tree like structure with primary branches starting from heat source reaching to corners of the domain.
- Use of symmetry condition & Global optimality of the shape needs to be verified

Conclusions

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- Implemented Level set based Topology optimisation methodology with Re-initialisation in Comsol 5.2 using MATLAB Livelink® feature
- Demonstrated the application of this methodology for Heat sink designs for different objectives
- Heat sink for thermal compliance objective leads to Dendritic shape whereas for Viscous dissipation objective leads to solid shape guiding the flow with least resistance
- Three Dimensional Heat sink also designed for minimum Thermal Compliance Objective.
- Further research is needed to ensure the global optimality of the obtained shapes

Thank You

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Additional slides

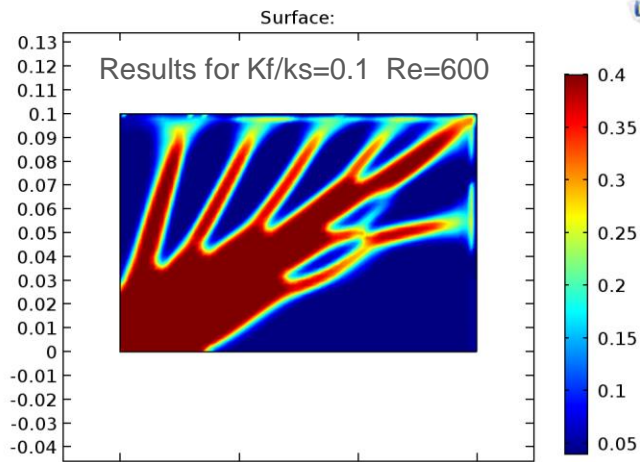
Results Comparison

Re	Pr of fluid	Kf/Ks	Heatflux	Coupled Level Set	SIMP	Re-initialized LS
60	105	0.001	700	29.5 ★ T=509K	43.7 (g=0.2) 510K	202.506 ★ 523.1K
60	105	0.1	700	2687 T=606K	2569 (g=0.7) Temp:618K	3154.4 631.59K

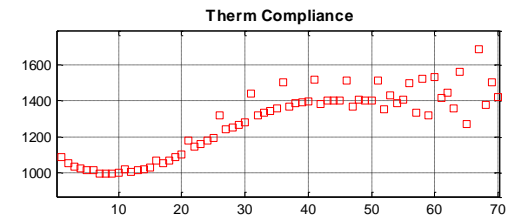
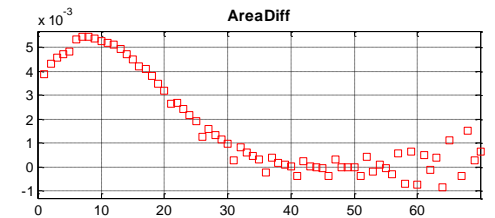
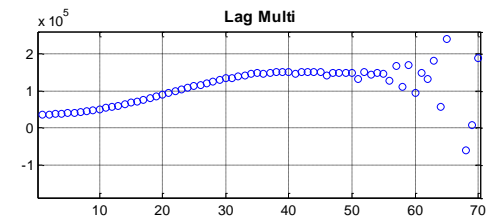
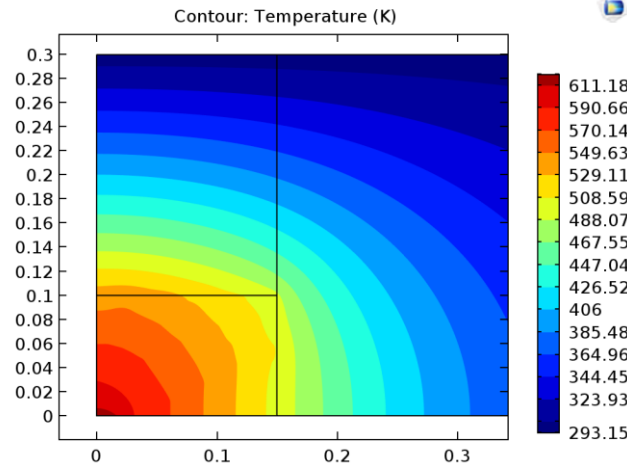
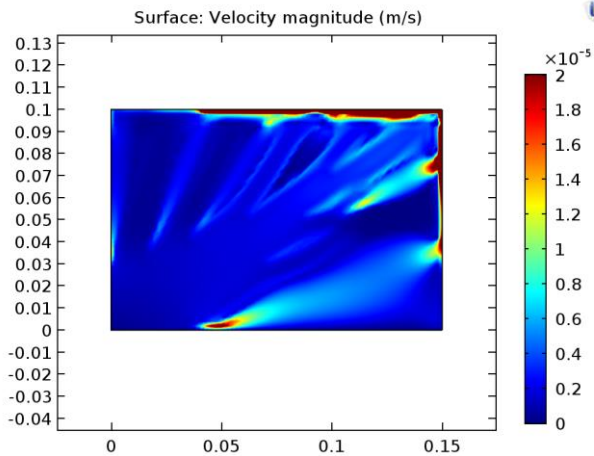
	SIMP TO	Coupled LS	Re-initialised LS
Thermal compliance (kgm ² K/s ³)	6.518	2.05 ★	8.2257 ★
Maximum Temperature (K)	383.9	378.58	412.52

- Coupled LS results show lower objective value than re-initialised LS due to presence of grey cells.
- CFD study on optimal shapes are required to validate the results

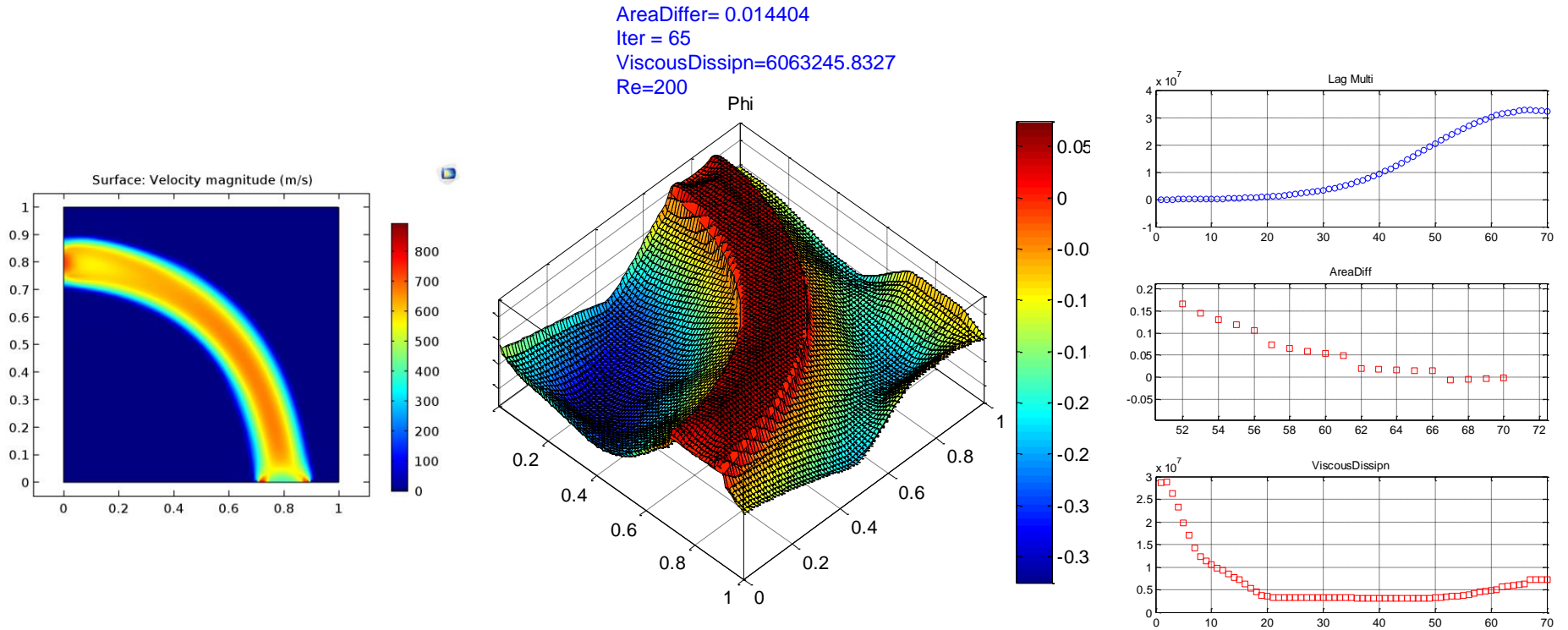
Results with Symmetry Boundary condition



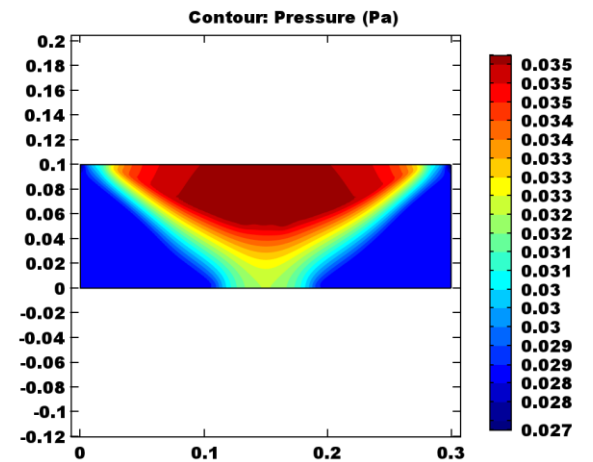
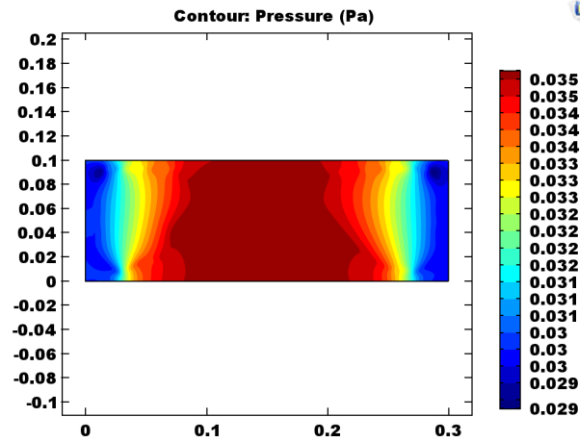
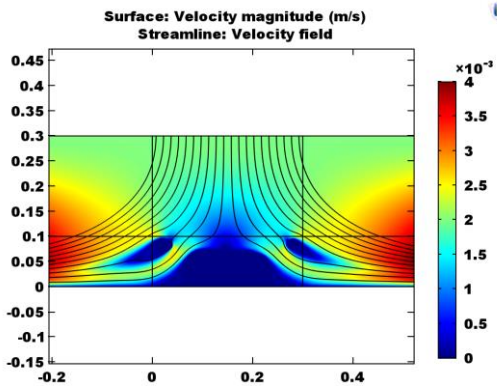
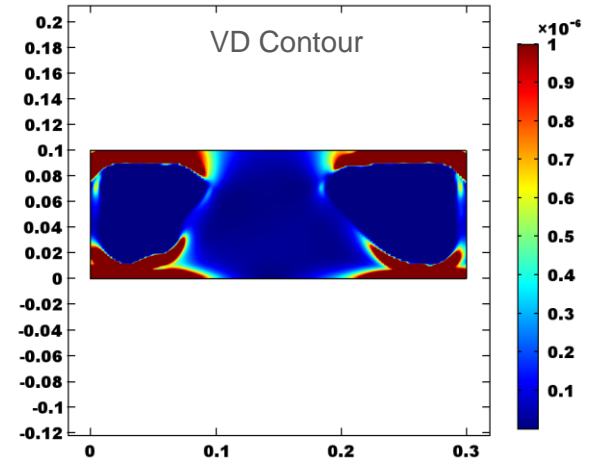
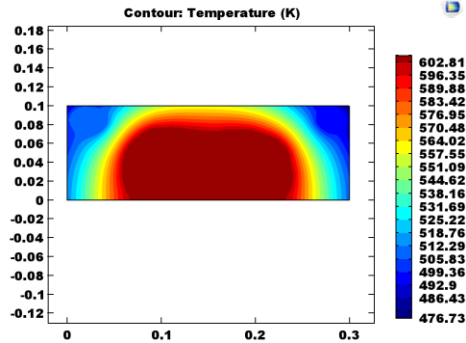
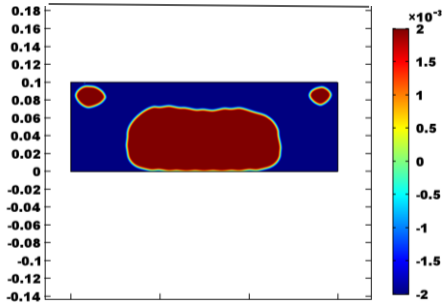
Lm_area=0.00598 (-0.3%)
 Thermcomp=1400.10
 Max T=621.44k
 Limiter=950,000

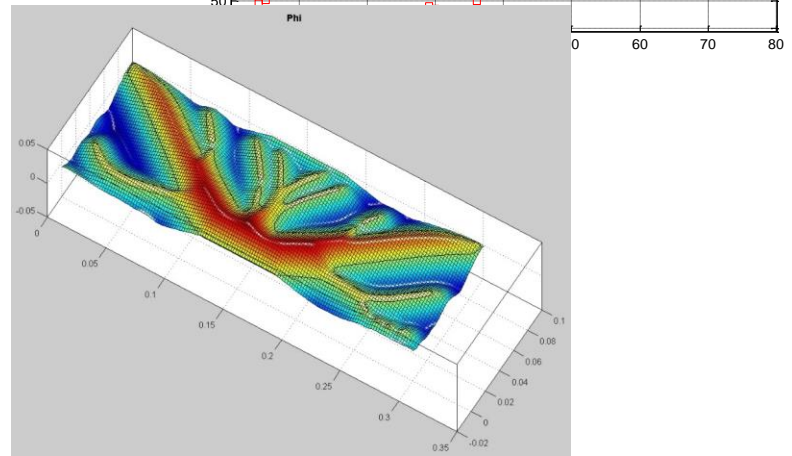
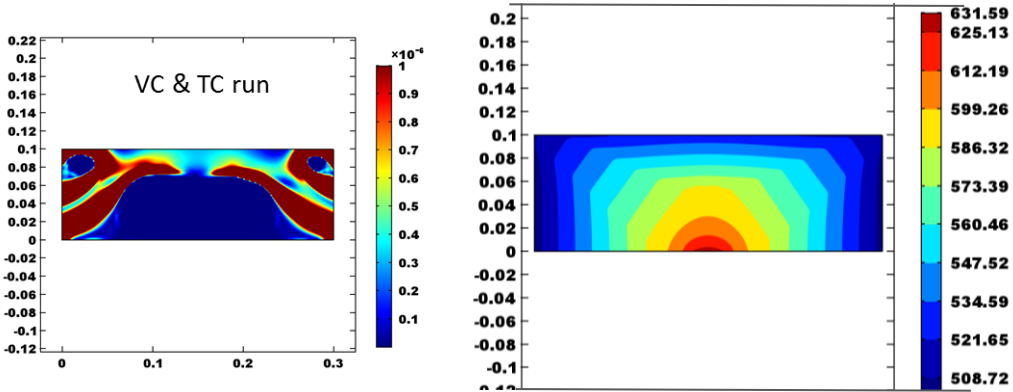
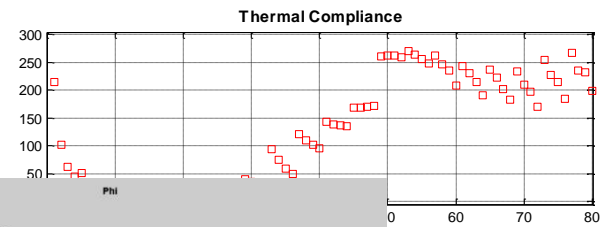
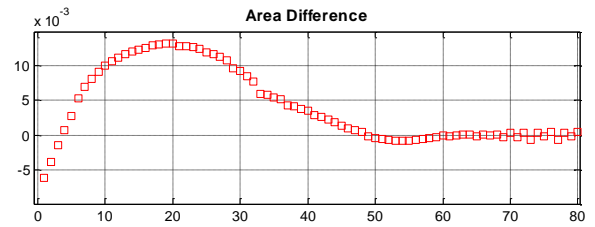
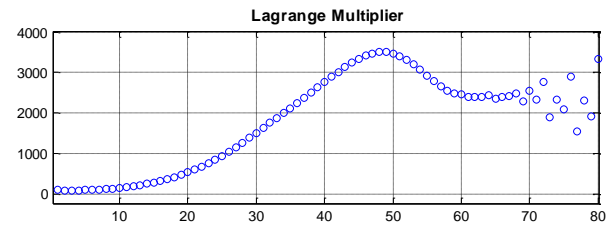
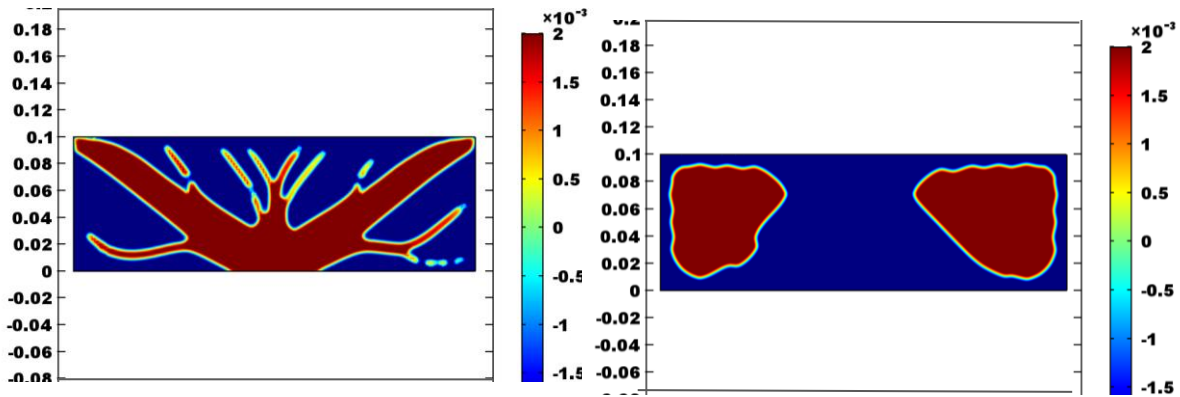


Low Reynolds number Duct flow



- Initial Values: if(H<1,0[m/s], v1) & Additional ' leaked Wall' condn with No surfaces selected. (**Leaked wall condn not necessary; *Lsnoleakwall.mph**)
- Setting this initial value imposes noslip on solid walls
- Also corrected the force (alpha) term





Level Set TO - Numerical Implementation

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