



Finite Element Analysis of Thermal Fatigue in Thermal Barrier Coatings (TBC)

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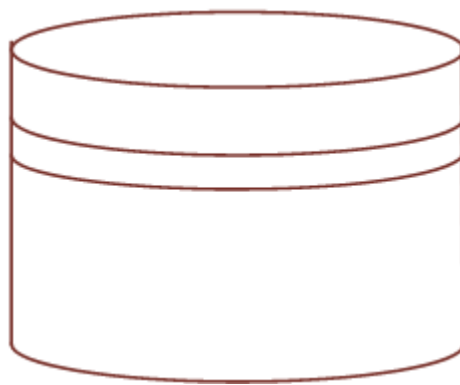
Introduction

- **Description of TBC's and thermal cycling experiments**
- **Overview of the convective heat transfer characteristic of an impinging air jet**
- **Assessment of the Thermal-Structural interaction model with COMSOL[®] multiphysics**
- **Results of the simulations**
- **Model validation through temperature measurements on real samples**



Thermal Barrier Coatings

- Used to protect metallic substrates from corrosion
- Used in energy and aero-spatial applications



Yttria-Stabilized Zirconia 8% (YSZ)
-Provides thermal stability

MCrAlY Bond Coat (BC)

M= Co, Ni, Fe

-Provides protection against substrate
oxydation

Inconel 718 Substrate



Thermal Cycling Experiments

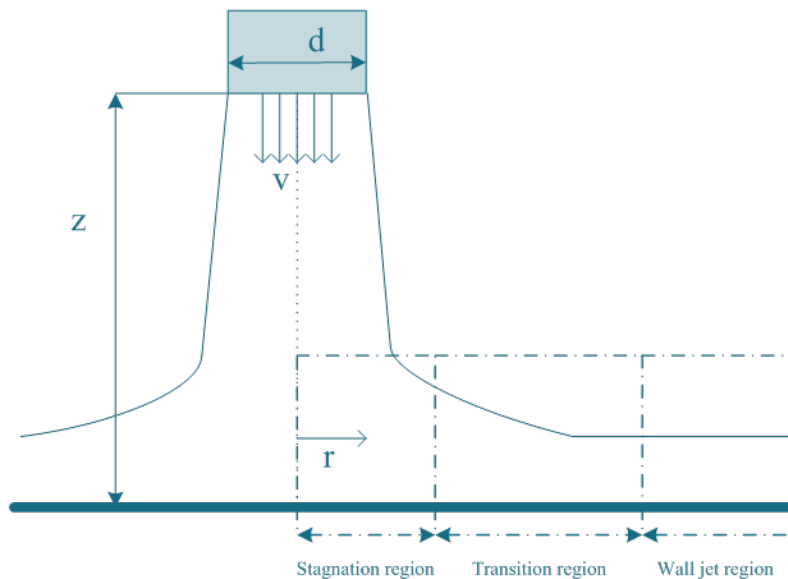
- **Used to predict the TBC's lifetime and durability**
- **Samples are warmed in a furnace and then rapidly cooled with a bath or with an impinging air jet**
- **TBC's failure is related to the stresses induced by different thermal expansion coefficient of the layers: cracking and delamination processes occur**
- **Results are largely affected by experimental set up**



Use of FEM to assess the Thermal Cycling Experiments



Heat transfer characteristic of the jet



- Stagnation region heat transfer coefficient [1]:

$$\frac{Nu}{Re^{1/2} Pr^{1/3}} = a_1 \left(\frac{z}{d} \right)^{0.11} \left(1 - \frac{\left(\frac{r}{d} \right)^2 \left(\frac{z}{d} \right)^{0.2}}{b_1} \right)^{1.2}$$

- Transition region heat transfer Coefficient [1]:

$$Nu = 0.198 Re^{0.6632} \left(\frac{z}{d} \right)^{-0.0826} \left(\frac{r}{d} \right)^{-0.3702}$$

- Wall jet region heat transfer coefficient [1]:

$$Nu = 0.0436(E) Re^{0.8} Pr^{0.333} \left(\frac{z}{d} \right)^{0.0976} \left(\frac{r}{d} \right)^{-1.0976}$$

[1] Katti V., Prabhu S.V., International Journal of Heat and Mass Transfer 51 (2008) 4480–4495



Geometry Reduction for Calculations

- Geometry was reduced to 2D for symmetry reasons
- MCrAlY bond coat was included into the Inconel substrate as they have similar thermo-mechanical properties





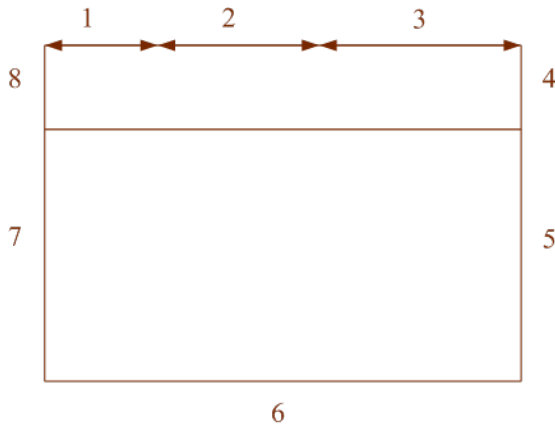
Model Assessment//

- **COMSOL®'s thermal-structural interaction axial symmetry stress-strain with thermal expansion, transient analysis model was used**

Boundary Conditions:

Thermal Analysis

Stress-Strain Model



1-4, 6 Heat Flux

$$k\nabla T = h\Delta T + h_r\Delta T^4$$

5 Thermal insulation

7, 8 Axial Symmetry

Free Boundaries



Model Assessment/II

Initial Conditions:



Thermal Analysis

**1423 K Temperature
in all domains**

Meshing

**Smaller elements at the YSZ-inconel
interface and in the stagnation point**

Stress-Strain Model

**1423 K Strain Reference
Temperature**

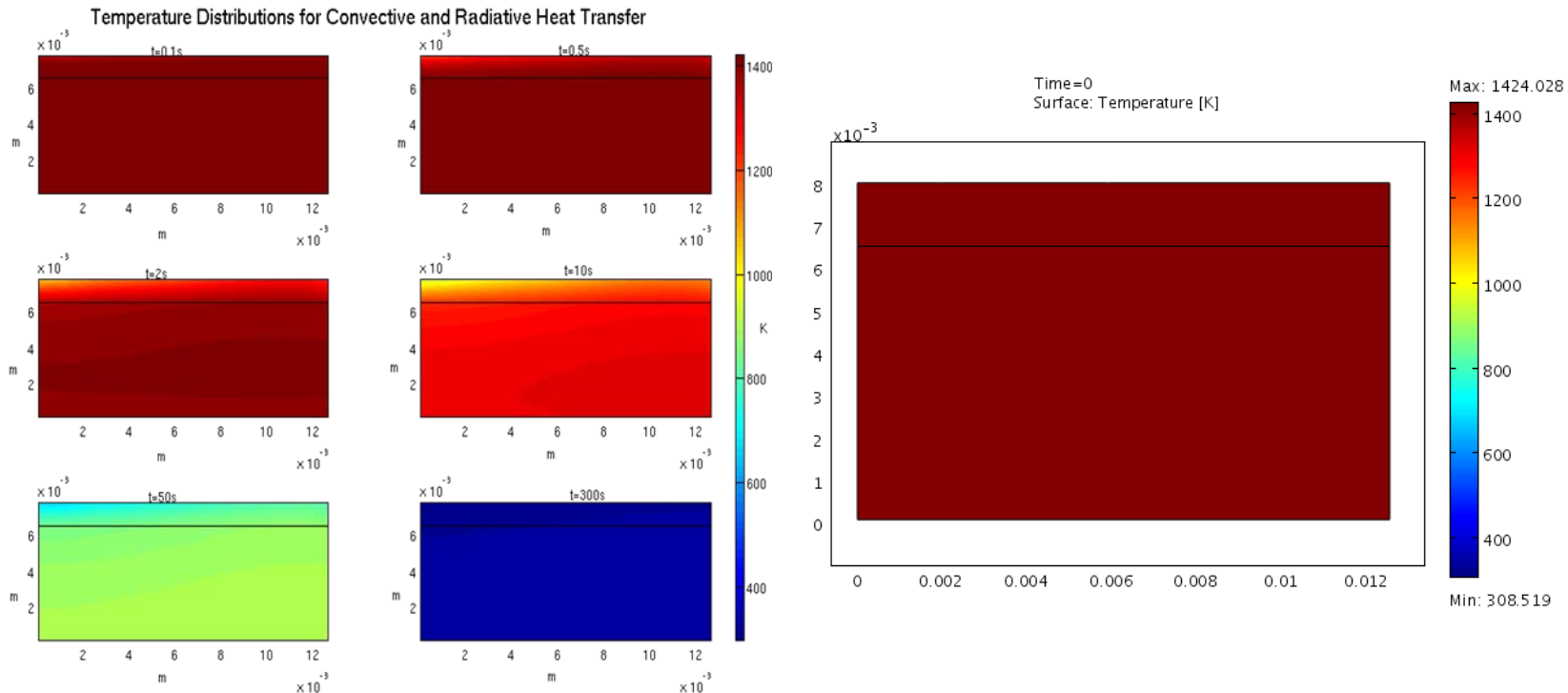
**Thermo-Mechanical
properties
of the materials**



Properties	8%YSZ	Inconel 718
Thermal Conductivity (W/m K)	2.29	15.048
Density (kg/m ³)	6000	8510
Heat Capacity at constant pressure (J/Kg K)	600	652
Poisson's Ratio	0.23	0.3
Young's modulus (Pa)	$2.05 \cdot 10^{10}$	$2 \cdot 10^{11}$
Thermal expansion coefficient (1/K)	$1 \cdot 10^{-5}$	$1.15 \cdot 10^{-5}$



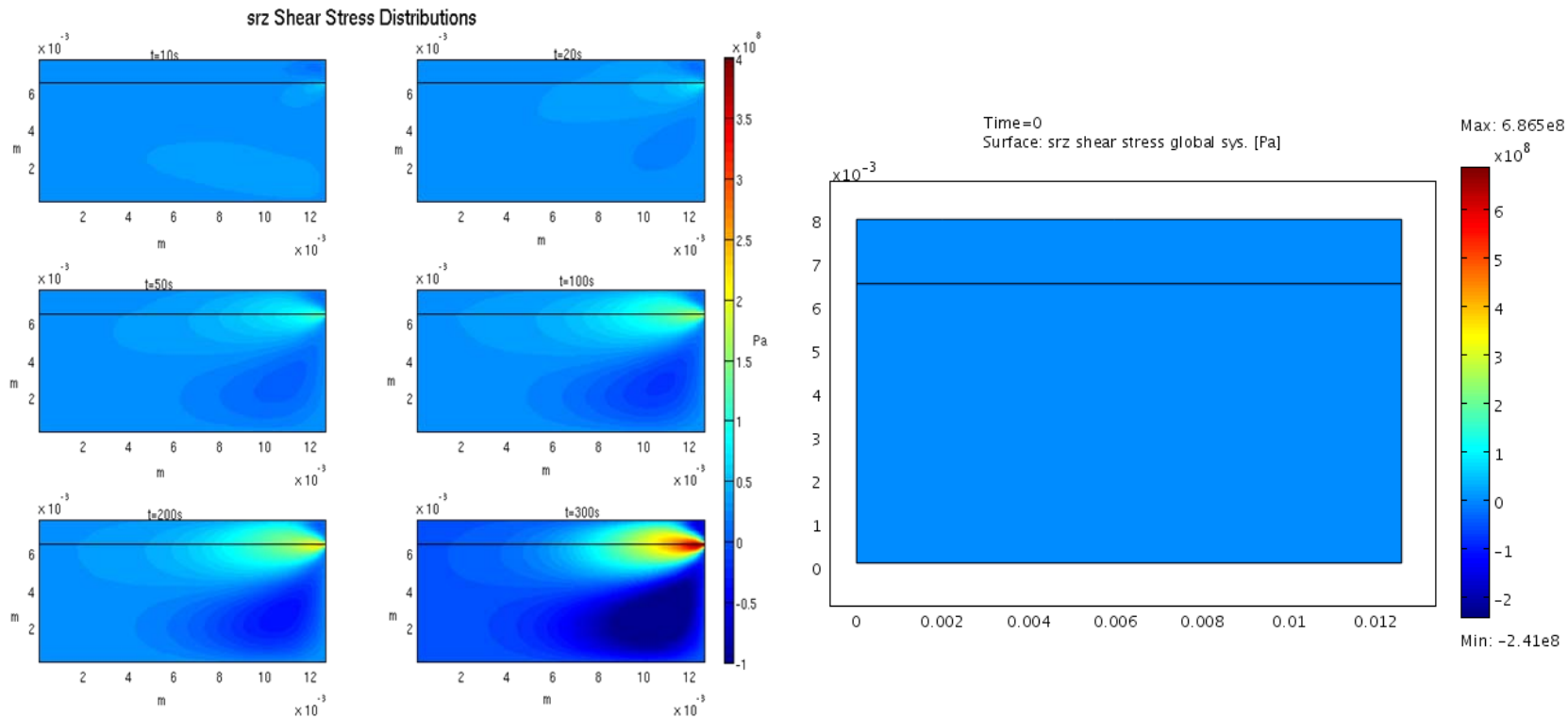
Thermal Analysis Results



- Sample reaches homogeneous temperature after about 300 seconds of cooling



Stress-Strain Results/I



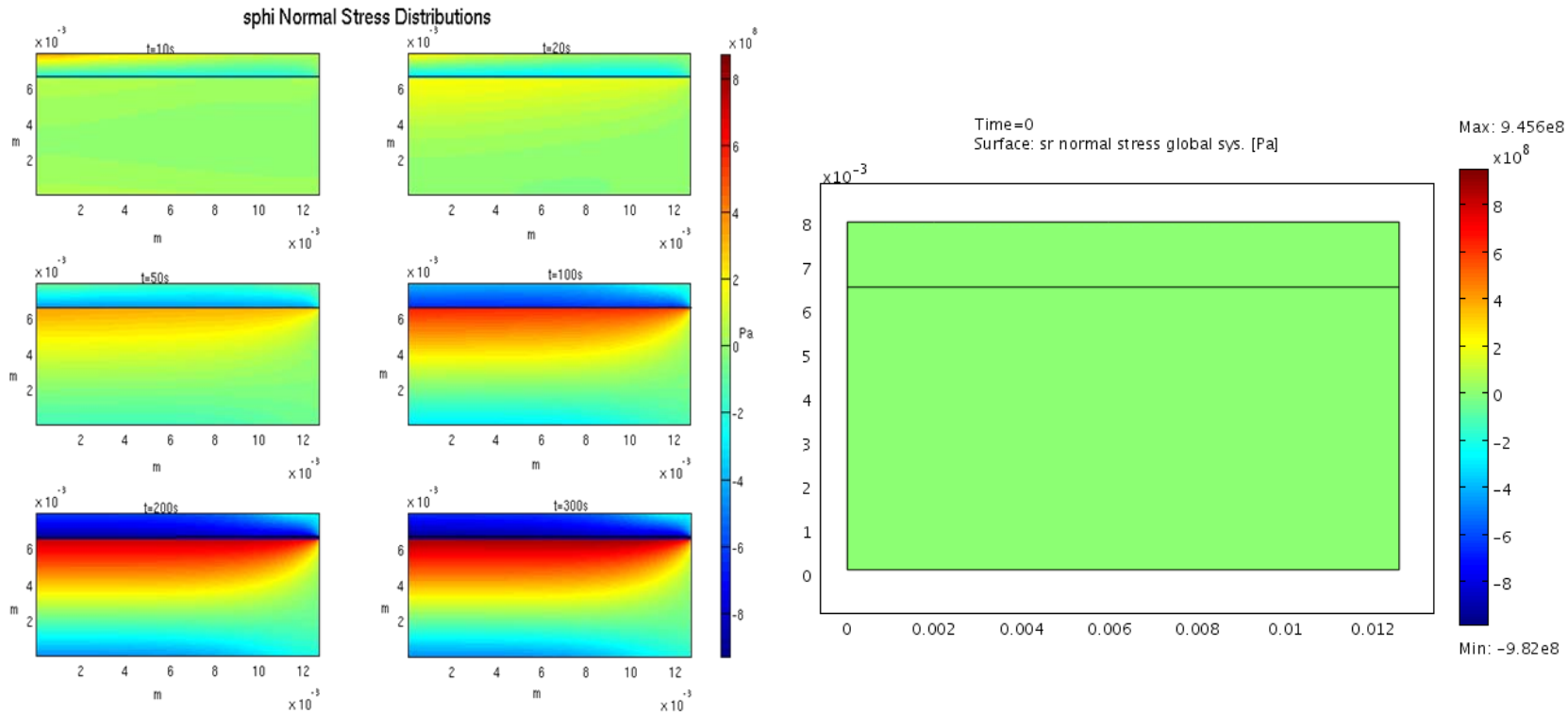
- Shear stress is responsible for the delamination processes of the sample^[2]

[2] H.Bhatnagar, S.Ghosh, M. E. Walter, International Journal of Solids and Structures 43 (2006) 4384–4406

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Stress-Strain Results/II



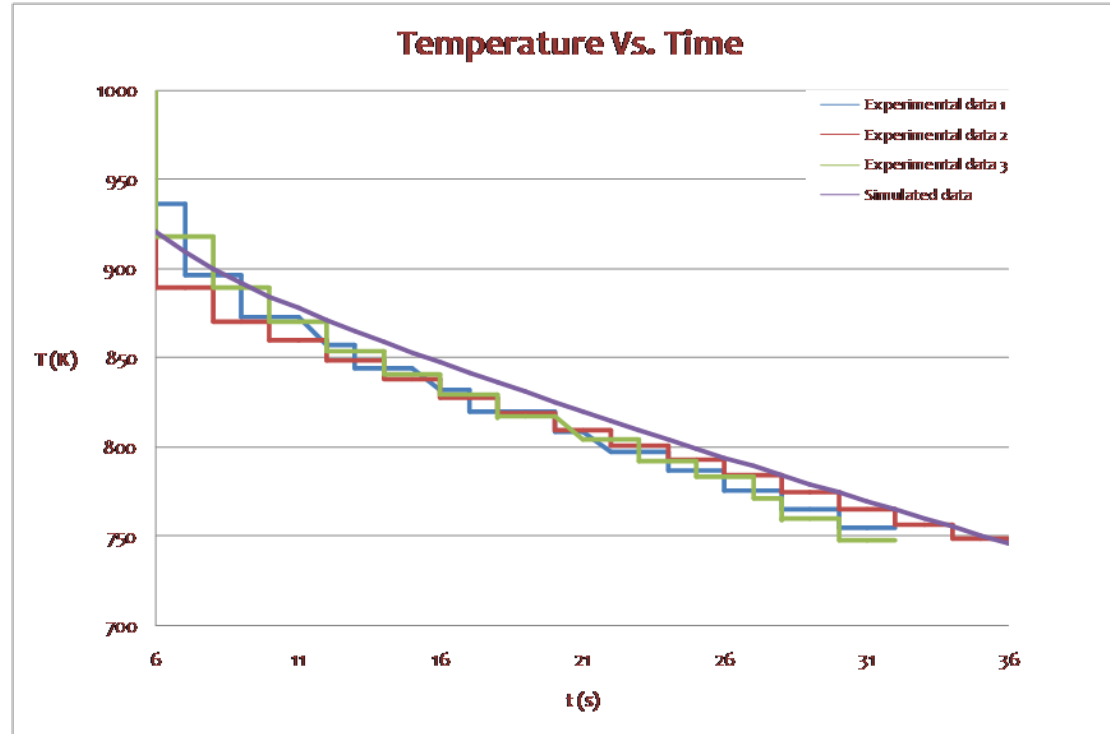
- Normal stress is responsible for the spallation processes of the sample^[2]

[2] H.Bhatnagar, S.Ghosh, M. E. Walter, International Journal of Solids and Structures 43 (2006) 4384–4406



Validation of the model

- Comparison between simulated data and temperature measurements with an infrared pyrometer on the point between the transition region and the wall jet region shows good agreement





Conclusions

- We assessed a finite element model to predict the stress generation during the cooling of a TBC under an impinging air jet
- Simulations show that the stresses are generated on the first 200 seconds of cooling
- Simulation show that the sample is completely cooled after about 300 s of cooling
- The thermal analysis' results show good agreement with the temperature measurements on real samples made by an optical pyrometer
- This kind of study could be a useful tool to predict the sample behavior during the cooling and could help to design more efficient thermal cycling experiments.



Thanks for your attention!

Questions are Welcome!