



Thickness Optimization of a Piezoelectric Converter for Energy Harvesting

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Introduction

Extensive diffusion of sensing nodes and sensing networks
(automotive, factory automation, entertainment, environment monitoring, security systems,...)

Main issue: **power supply**



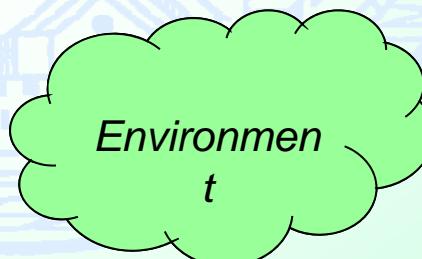
Batteries

- ⬇️ • limited lifetime
- ⬇️ • recharging/replacement/disposal
- ⬇️ • cost



Power harvesting

- ⬆️ • in principle unlimited lifetime
- ⬆️ • unattended operation
- ⬇️ • sometimes limited output power



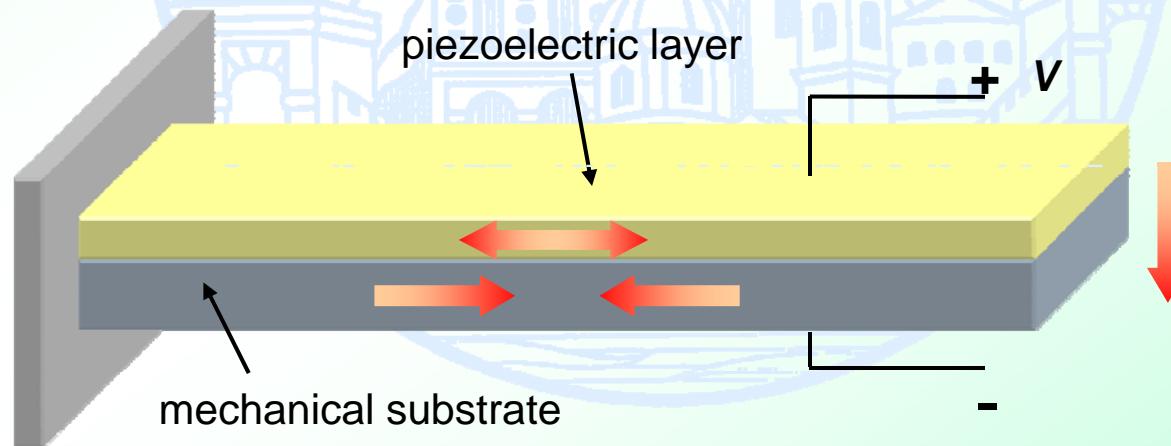
- ✓ Solar energy
- ✓ Mechanical vibrations
- ✓ Temperature gradients
- ✓ ...

Mechanoelectrical energy conversion

- Conversion techniques
 - electromagnetic (inductive)
 - electrostatic (capacitive)
 - piezoelectric**

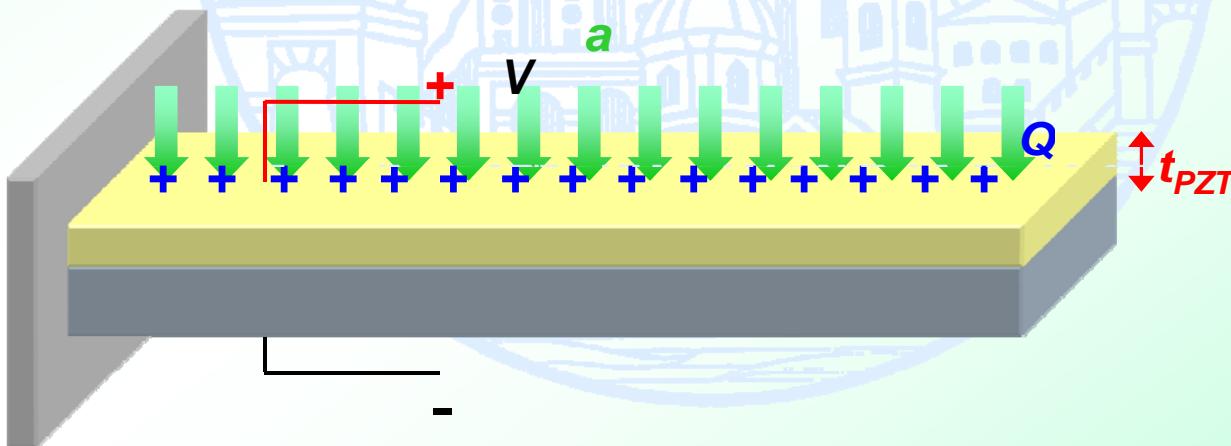
Direct piezoelectric effect: surface charge induced by a mechanical stress

- Piezoelectric energy converter
 - unimorph cantilever shape (thick-film, MEMS technologies)



Use of COMSOL

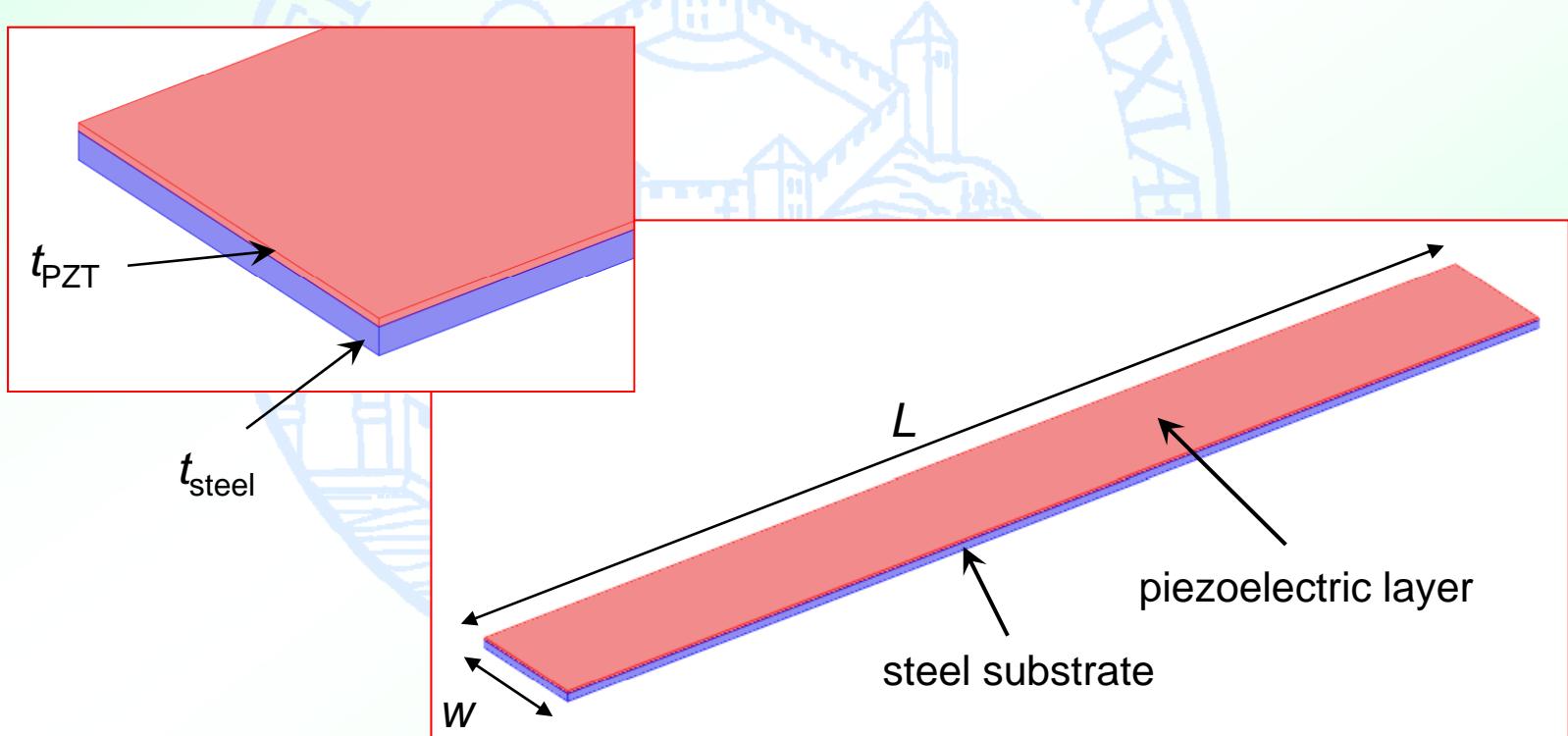
- Improvement of the converted energy
 - Optimization of the dimensions
 - piezoelectric layer thickness
- Application modes
 - piezoelectric: mechanical / electrical behaviour
 - sinusoidal vertical acceleration application
 - generated charge / voltage
 - moving mesh: thickness change



Geometry

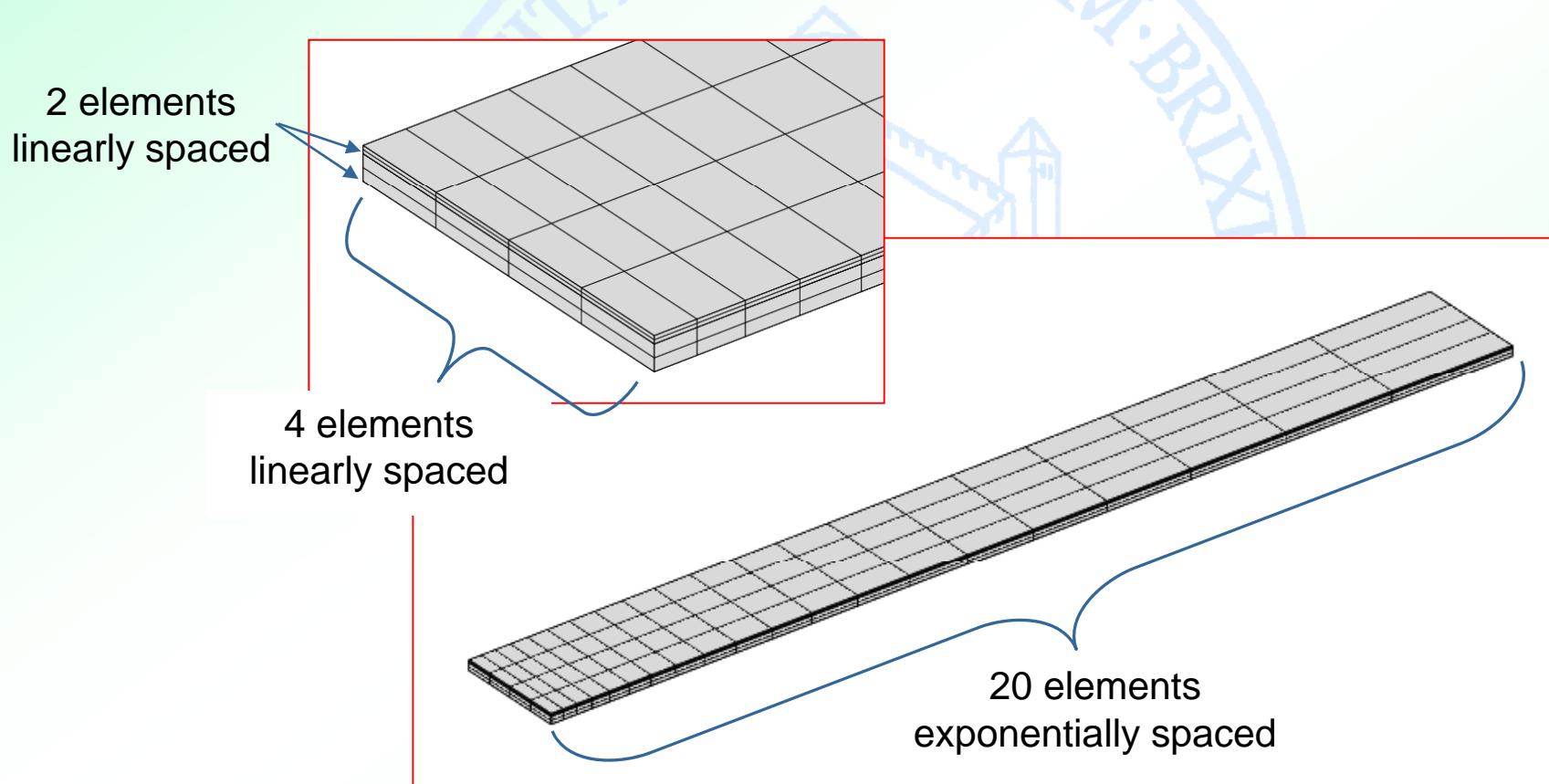
- 3D cantilever

- length $L = 27 \text{ mm}$;
- width $w = 3 \text{ mm}$;
- steel thickness $t_{\text{steel}} = 200 \mu\text{m}$;
- piezoelectric layer thickness $t_{\text{PZT}} = 60 \mu\text{m}$ (poled along thickness)



Mesh

- Mapped mesh
 - 320 quad elements; 11808 degrees of freedom



Governing equations

- Piezoelectric layer
 - strain-charge form

$$S = s^E T + d E$$

$$D = \varepsilon^T E + d T$$

- S = mechanical strain
- T = mechanical stress [N/m^2]
- s^E = elastic compliance [Pa^{-1}]
- d = piezoelectric coefficient [C/N]
- D = electric displacement [C/m^2]
- E = electric field [V/m]
- ε^T = dielectric permittivity [F/m]

- Steel layer

$$S = s T$$

$$s^E = \begin{bmatrix} 50 & -20 & -20 & 0 & 0 & 0 \\ -20 & 50 & -20 & 0 & 0 & 0 \\ -20 & -20 & 50 & 0 & 0 & 0 \\ 0 & 0 & 0 & 70 & 0 & 0 \\ 0 & 0 & 0 & 0 & 70 & 0 \\ 0 & 0 & 0 & 0 & 0 & 70 \end{bmatrix} \times 10^{-12} \text{ Pa}^{-1}$$

$$d = \begin{bmatrix} 0 & 0 & 0 & 0 & 11 & 0 \\ 0 & 0 & 0 & 11 & 0 & 0 \\ -2.5 & -2.5 & 5 & 0 & 0 & 0 \end{bmatrix} \times 10^{-12} \text{ CN}^{-1}$$

$$\varepsilon^T = \begin{bmatrix} 50 & 0 & 0 \\ 0 & 50 & 0 \\ 0 & 0 & 50 \end{bmatrix} \times \varepsilon_0$$

$$\rho = 3000 \text{ kg} \cdot \text{m}^{-3}$$

$$s = 5 \times 10^{-12} \text{ Pa}^{-1}$$

Subdomain and boundary conditions

Vertical acceleration

- Body load $F_z = a\rho$
 - $a = 0.1 g$
 - $\rho = \text{material density}$

Mechanical boundary conditions

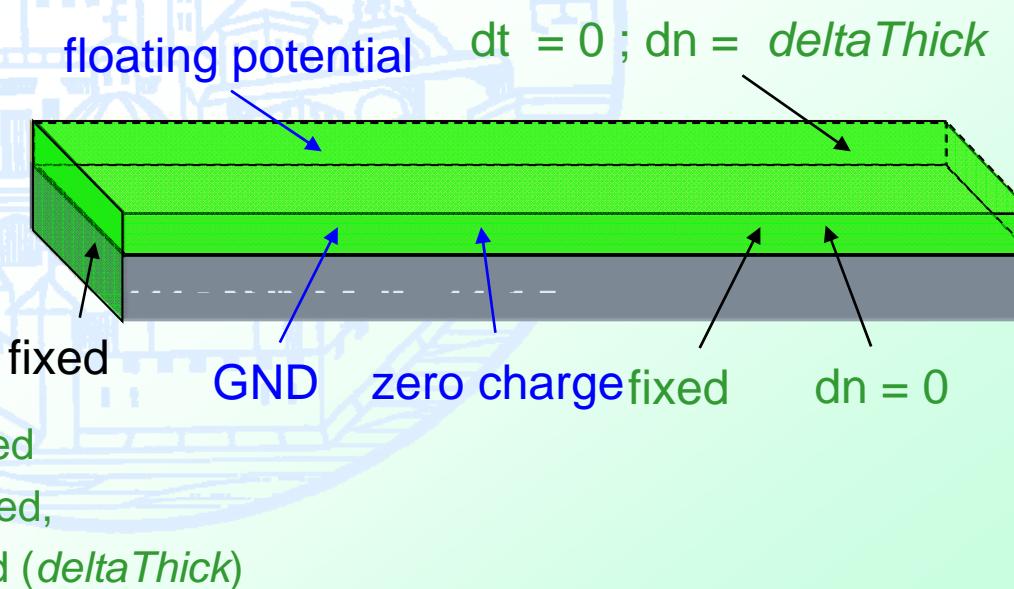
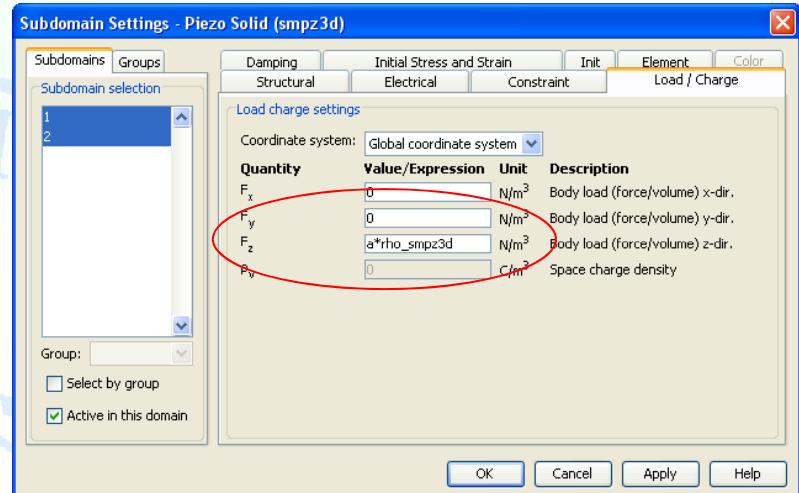
- clamped end

Electrostatic boundary conditions

- bottom surface: *grounded*
- upper surface: *floating potential*
- other surfaces: *zero charge*

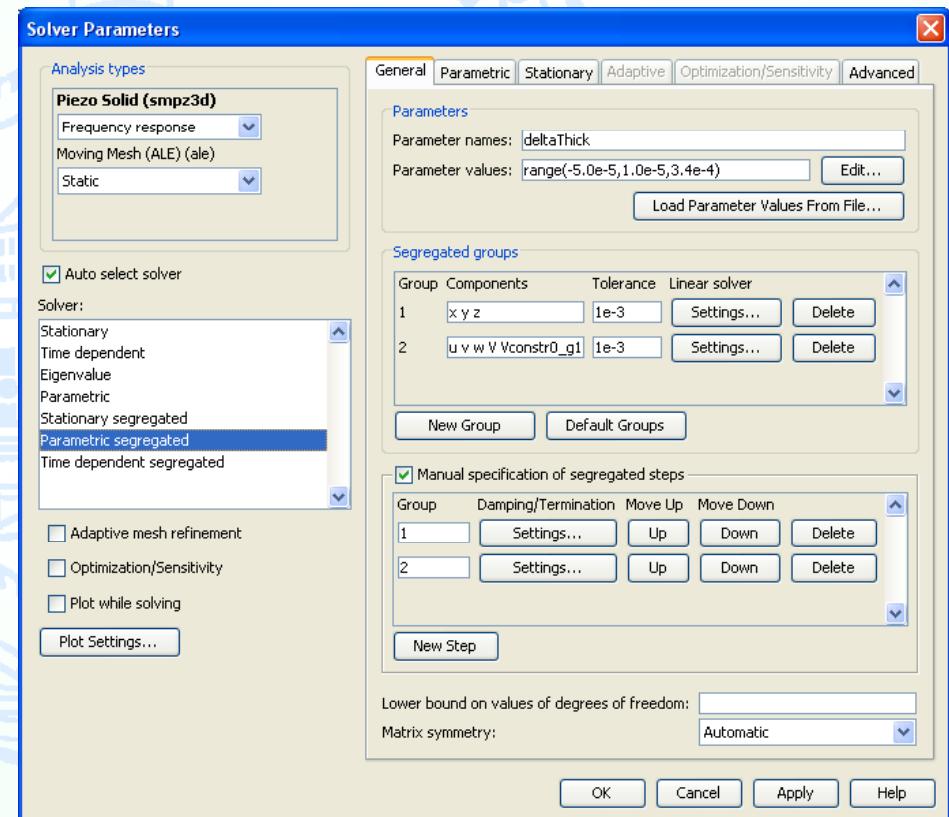
Mesh boundary conditions

- bottom surface: *clamped*
- vertical surfaces: *normally clamped*
- upper surface: *tangentially clamped, normally displaced ($\delta\text{Thickness}$)*

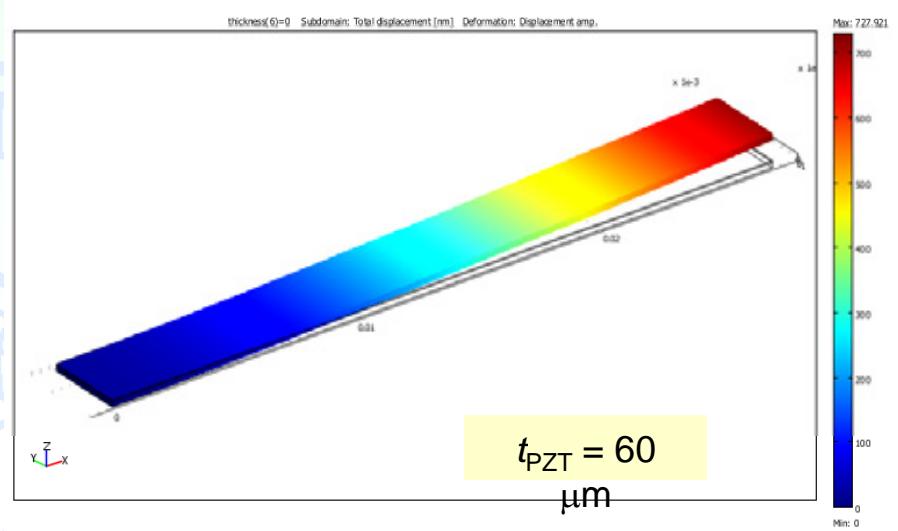
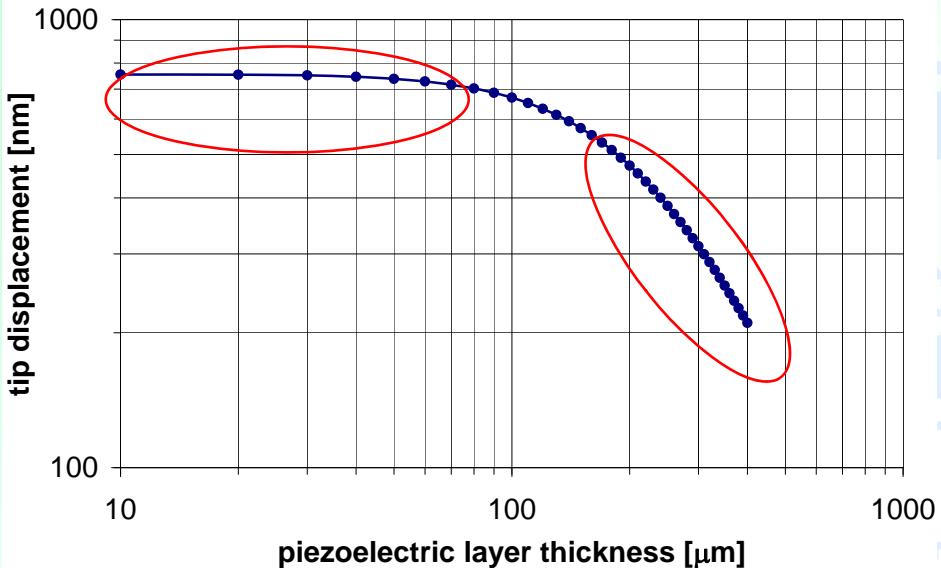


Solver parameters

- Parametric segregated solver
 - group 1: moving mesh, static analysis
 - δ_{Thick} : -50 μm → 340 μm
 - group 2: piezoelectric variables, frequency response
 - frequency = 10 Hz

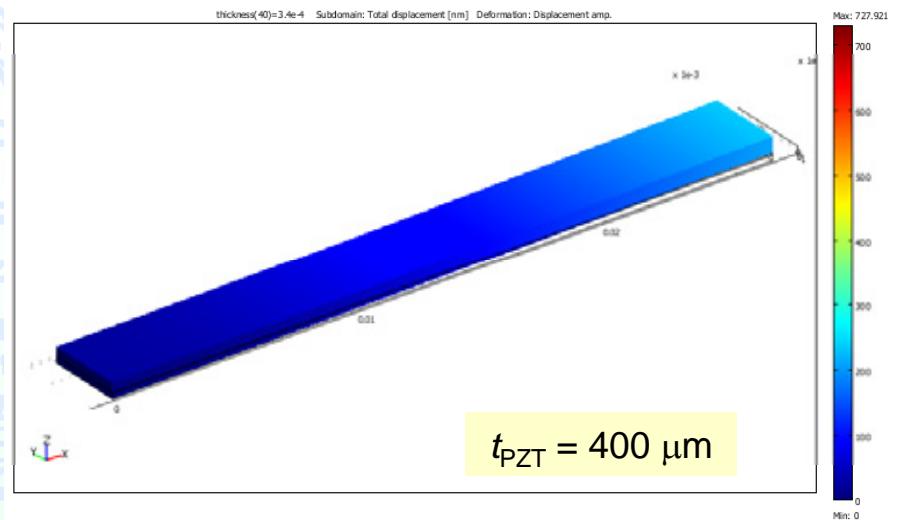


Results – tip displacement

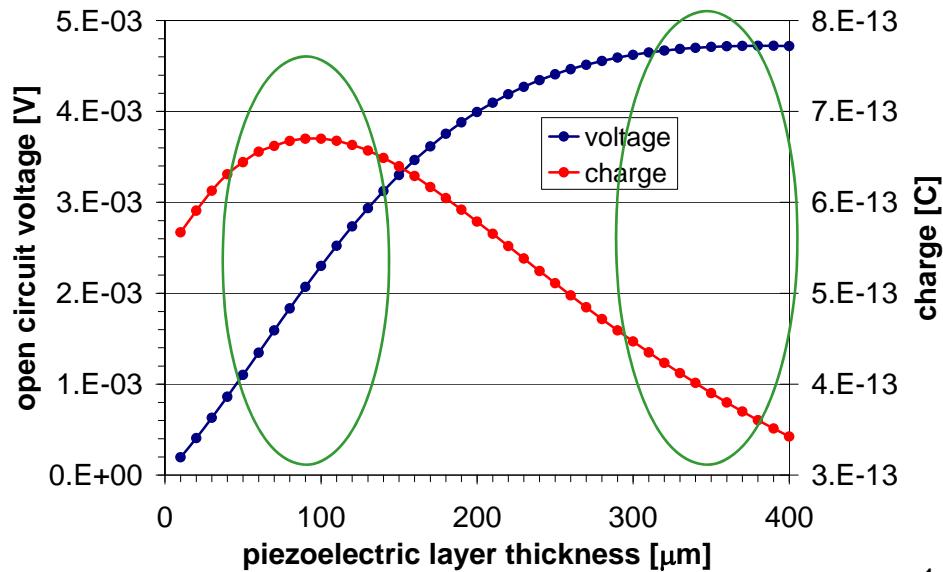


PZT rigidity << steel rigidity
tip displacement \approx const

PZT rigidity >> steel rigidity
tip displacement $\approx \frac{1}{t_{PZT}^n}$



Results – electrical output

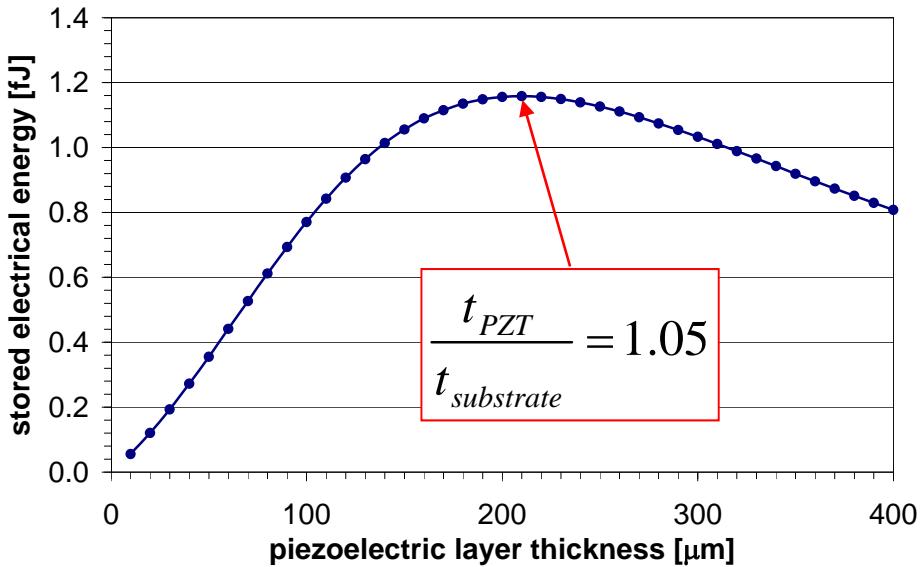


PZT rigidity << steel rigidity
charge: maximum
voltage: increases

PZT rigidity >> steel rigidity
charge: decreases
voltage \approx const

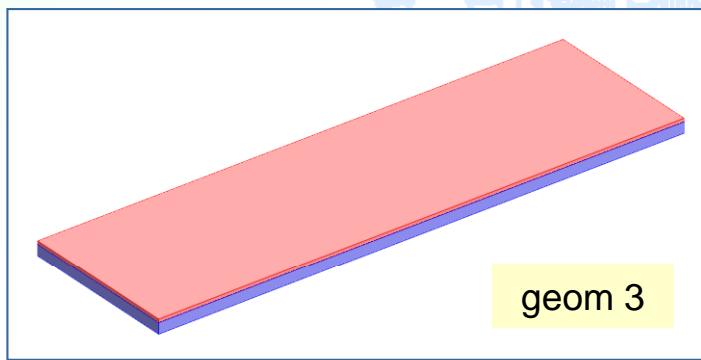
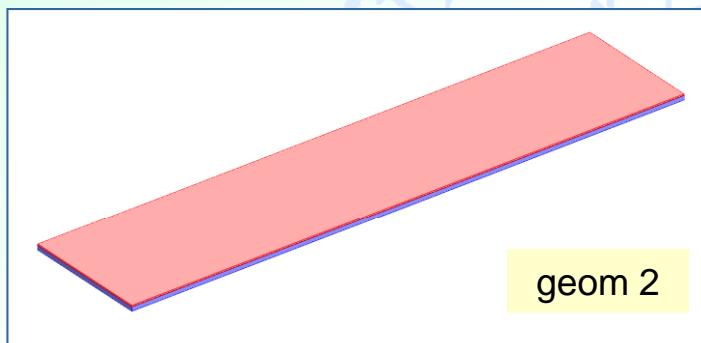
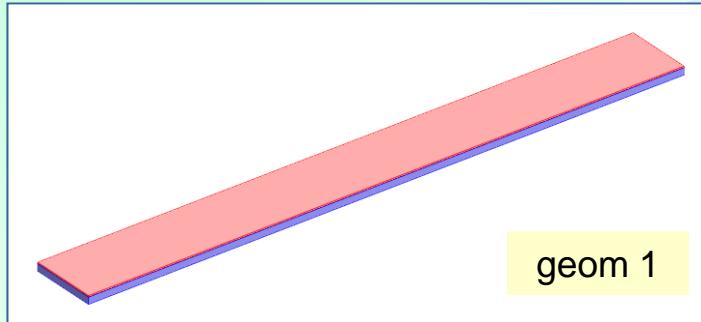
- Stored electrical energy

$$E = \frac{1}{2} QV$$

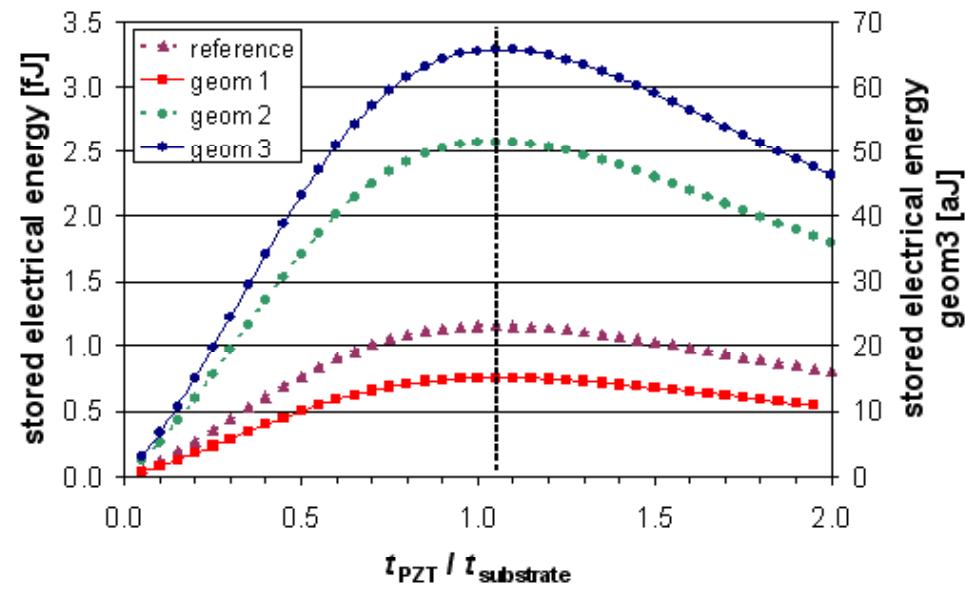


Results – influence of the geometry

- Different geometries



	Substrate thickness [μm]	Width [mm]	Length [mm]
reference	200	3	27
geometry 1	300	3	27
geometry 2	200	6	27
geometry 3	200	3	10



Conclusions

- FEM simulations used for optimizing the geometrical dimensions of a piezoelectric energy converter
- Geometry with parametrized thickness
 - piezoelectric application mode
 - moving mesh application mode
- The optimal $t_{\text{PZT}}/t_{\text{substrate}}$ was found for maximizing the electrical energy
- The optimal $t_{\text{PZT}}/t_{\text{substrate}}$ value is independent from the converter dimensions
- This model is a specific example of using moving mesh for device geometry optimization