

Model of Heat and Mass Transfer with Moving Boundary during Roasting of Meat in Convection-Oven

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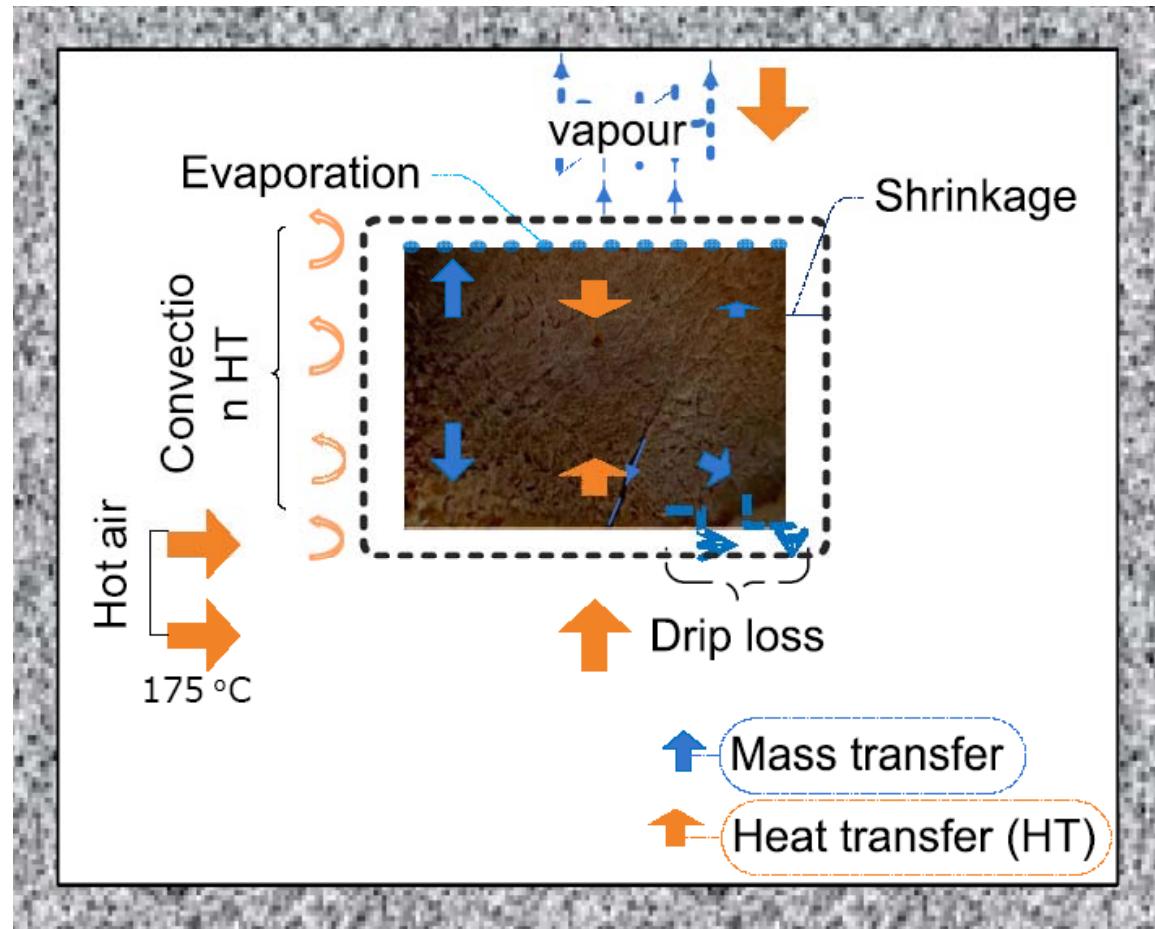
$$f(x+\Delta x) = \sum_{i=0}^{\infty} \frac{(\Delta x)^i}{i!} f^{(i)}(x)$$
$$\int_a^b \Theta^{\sqrt{17}} + \Omega \int \delta e^{i\pi} =$$
$$\infty = \{2.7182818284$$
$$x^2 \gg \Sigma !,$$

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Outline

- Introduction
- Theoretical background
- Modelling
 - Governing model equations
 - Boundary and initial condition
 - Model Solution
- Results
- Conclusion

Roasting process



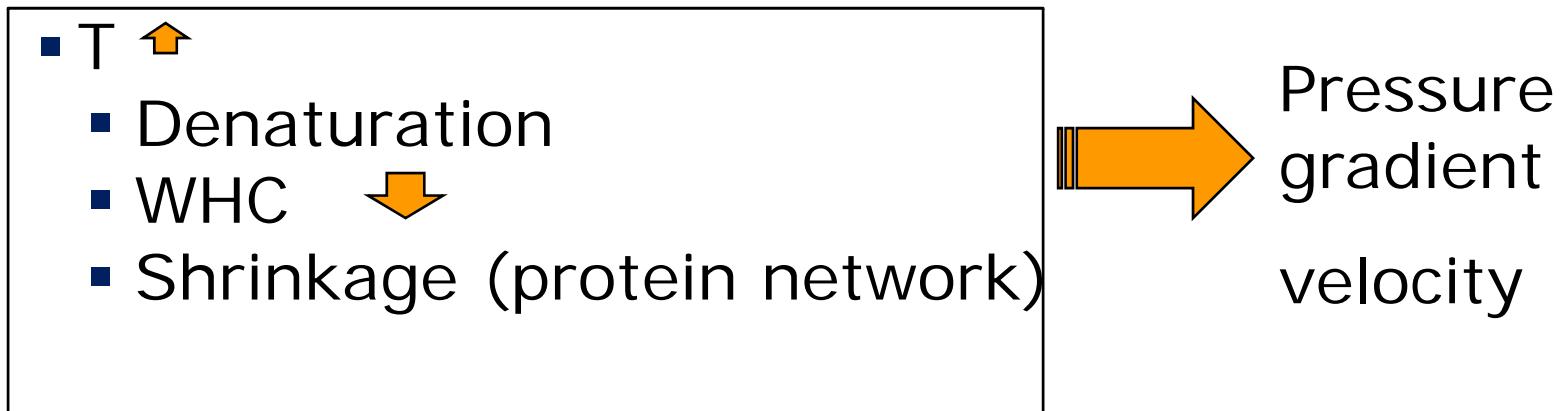
Model

- Better quantitative knowledge
- Prediction of T, C
- Quality, safety
- Minimize loss
 - Mass and energy
- Upscale
- Process control

Transport processes during oven-convection roasting

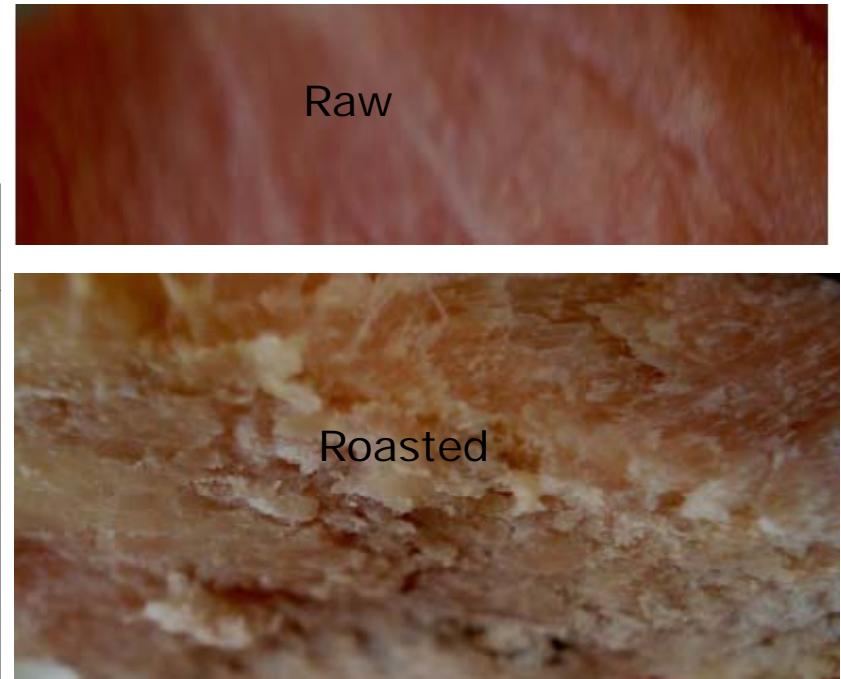
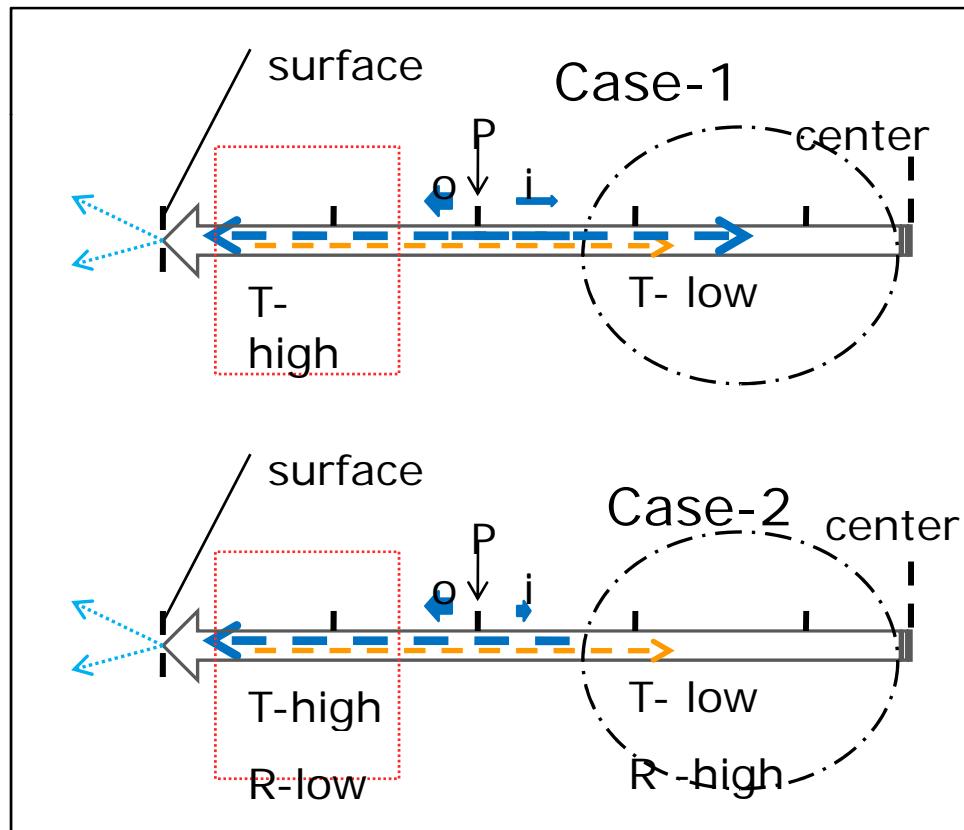
Water transport

- *Pure diffusion (often assumed)*
 - But doesn't capture pressure
- *Convective*



Change of microstructure

- Permeability(K)
- Elastic modulus (E)



Change of microstructure
during roasting
(cross-sectional view)

Assumptions

- Fat transport is negligible (lean meat)
- Evaporation takes place at the surface
- No internal heat generation and no chemical reaction
- Dissolved matter lost with water is small
- Reduction of water holding capacity and shrinkage are considered.

Governing equation of heat and mass transfer

Heat transfer

$$\rho_m c_{pm} \frac{\partial T}{\partial t} + \nabla(-k_m \nabla T) + \rho_w c_{pw} u_w \nabla T = 0$$

$$\begin{aligned}\rho_m &= f(C) \\ D &= f(T) \\ c_{pm} &= f(C) \\ \mu_w &= f(T)\end{aligned}$$

Water transport

$$\frac{\partial C}{\partial t} + \nabla(Cu_w) = \nabla D \nabla C$$

$$E_{(T)} = E_o + \frac{E_{mx}}{(1 + \exp(-E_n(T - E_D)))}$$

Velocity of water

$$u_w = \frac{-K}{\mu_w} \nabla P$$

$$P = E(C - C_{eq}(T))$$

Darcy's law

$$u_w = \frac{-KE}{\mu_w} \nabla(C - C_{eq})$$

$$C_{eq(T)} = 0.75 - \frac{0.345}{(1 + 30 \exp(-0.25(T - T\sigma)))}$$

Shrinkage /interface velocity

- Proportional to the volume of liquid water removed
- Formation of air filled pores

$$V = V_0 - \beta V_{w,l} \quad \beta = 1, \text{ no pore formation}$$

$$\beta = 0, \text{ no shrinkage}$$

$1-\beta$ = fraction of $V_{w,l}$ replaced by air

$$V = V_0 \left(1 - \frac{\beta V_{w,l}}{V_0} \right)$$

$$= \pi R_0^2 \left(1 - \frac{\beta V_{w,l}}{V_0} \right)^{2/3} Z_0 \left(1 - \frac{\beta V_{w,l}}{V_0} \right)^{1/3} = \pi R^2 Z$$

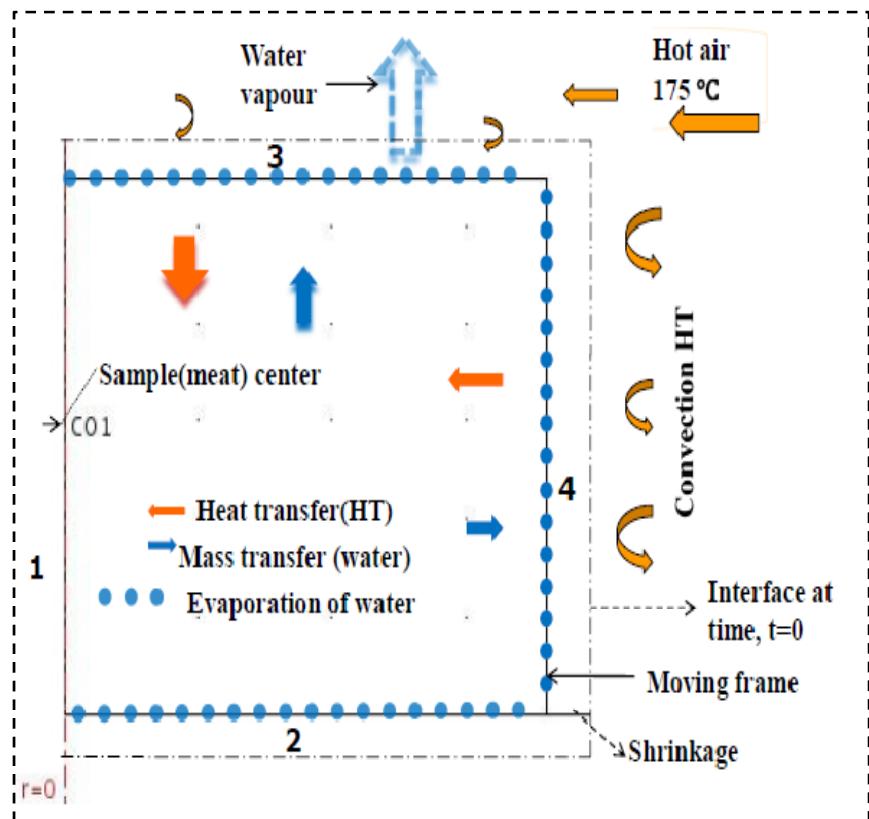
$$v_z = \frac{dZ}{dt} = -\frac{Z_0 \beta}{3V_0} \left(1 - \frac{\beta V_{w,l}}{V_0} \right)^{-2/3} \frac{d}{dt}(V_{w,l})$$

$$v_r = \frac{dR}{dt} = -\frac{R_0 \beta}{3V_0} \left(1 - \frac{\beta V_{w,l}}{V_0} \right)^{-2/3} \frac{d}{dt}(V_{w,l})$$

$$V_{w,l} = \frac{m_d(X_0 - X)}{\rho_w} = \frac{\rho_0 V_0 (1 - C_0)}{\rho_w} \left(\frac{C_0}{1 - C_0} - \frac{C_{av}}{1 - C_{av}} \right)$$

$$\frac{dV_{w,l}}{dt} = -\frac{\rho_0 V_0 (1 - C_0)}{\rho_w} \left(\frac{1}{1 - C_{av}} \right)^2 \frac{dC_{av}}{dt}$$

Boundary conditions and initial condition



■ BC 1:

Axial symmetry, $v_r=0$

■ BC (2, 3, and 4):

- HT- heat flux
- MT- mass flux
- ALE- velocity

IC:

$$T(r, z) = T_0 = \text{const} \quad \text{at } t = 0$$

$$C(r, z) = C_0 = \text{const} \quad \text{at } t = 0$$

Solution

COMSOL Multiphysics® version 3.5

2D cylindrical

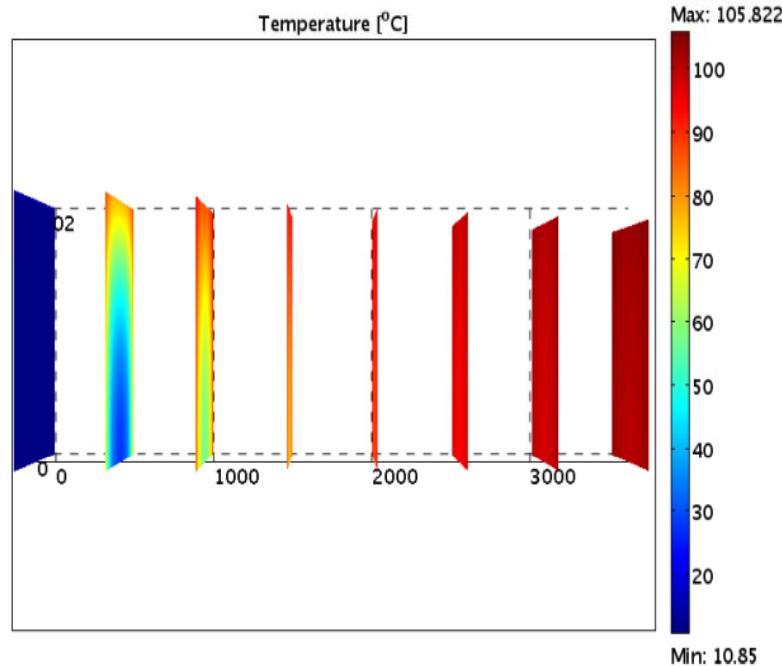
Radius of 20 mm and length of 54 mm

Chemical Engineering module

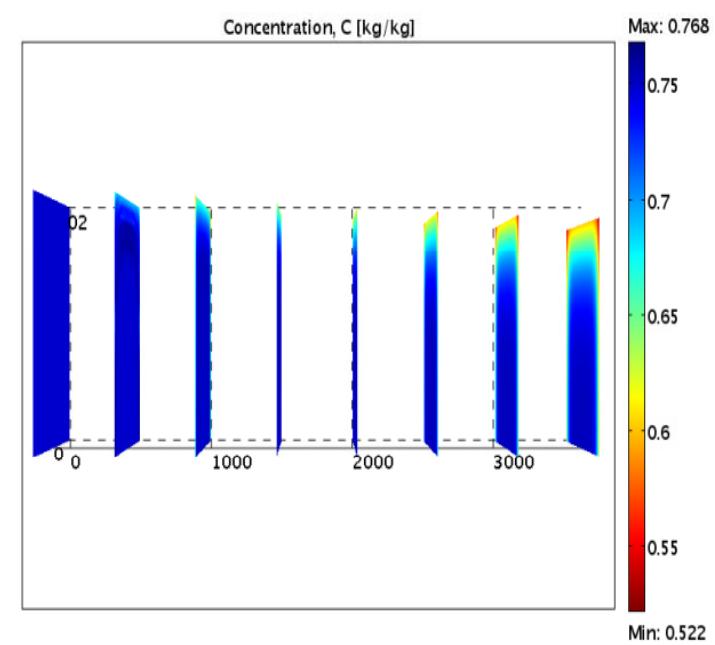
- Transient heat transfer
- Transient mass transfer

Moving mesh module (ALE)

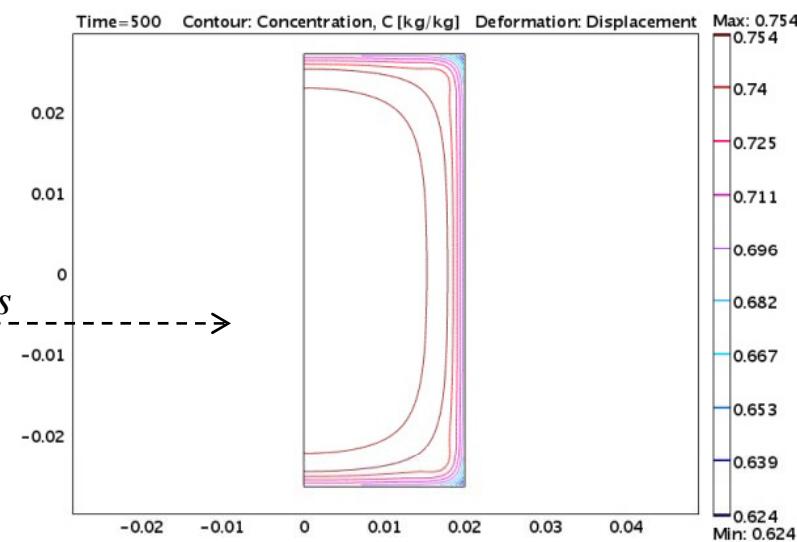
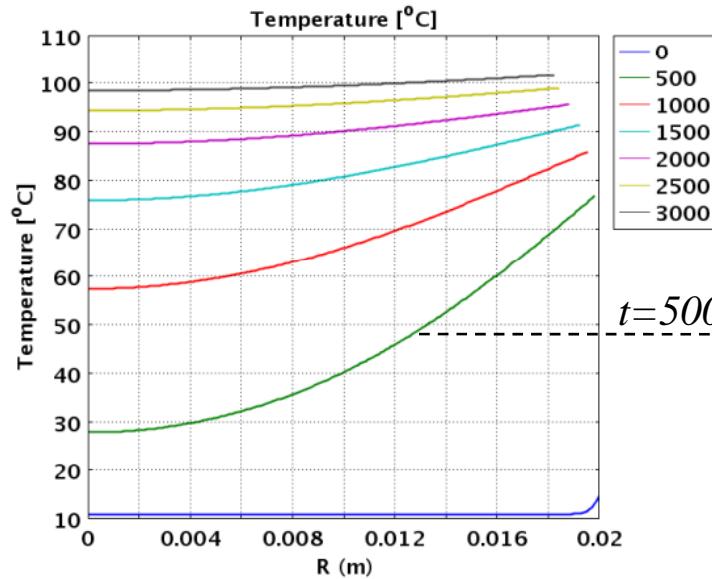
Results



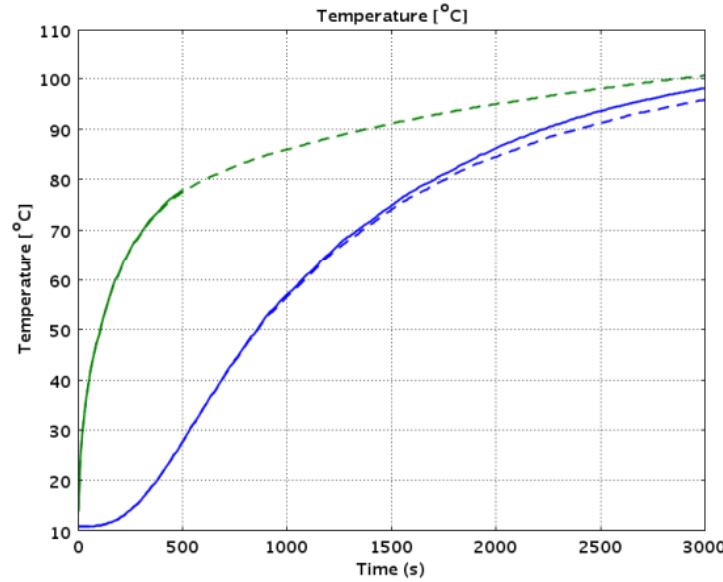
Temperature distribution



Water content distribution



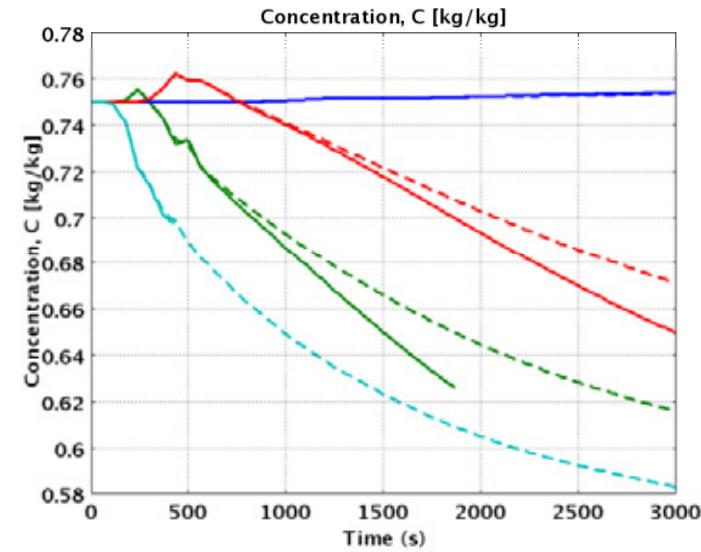
Model prediction with (-) MB vs. with FB (--)



Temperature profile

blue-center(0, 0)

green-surface ($r = 0.02, z = 0$)

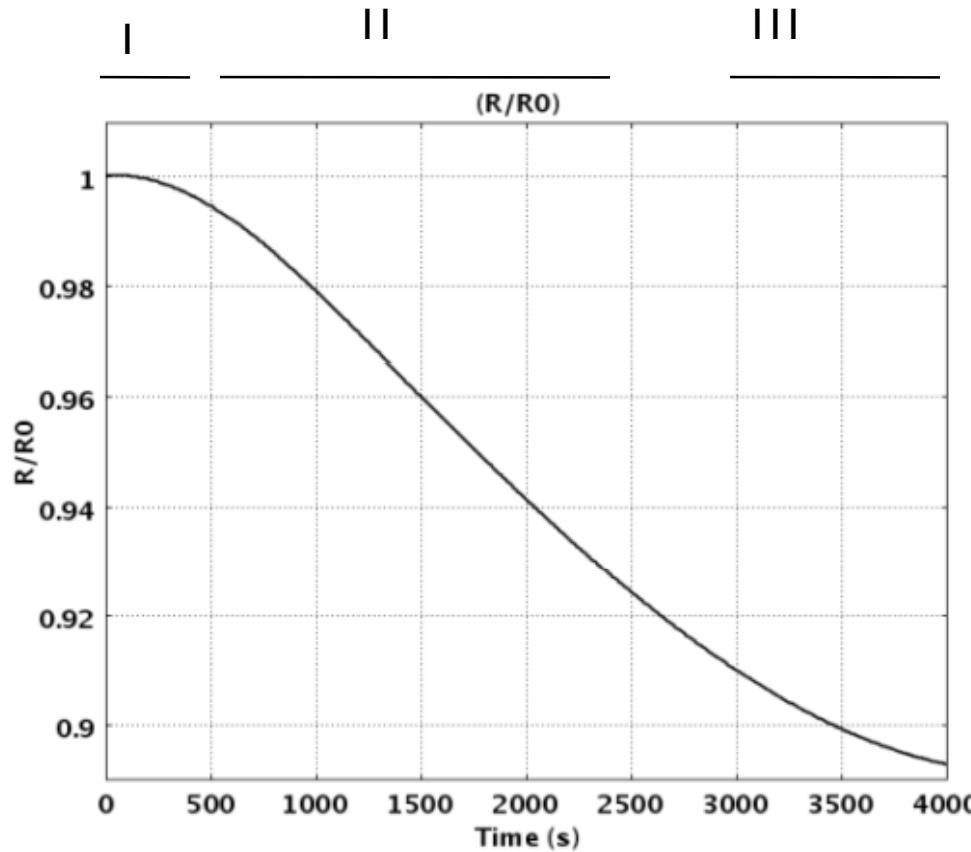


Water content profile

blue(0, 0), red (0.017, 0)

green (0.019, 0), cyan (0.02, 0)

Radial shrinkage



**Relative radius of cylinder as function of time
(R/R_0)**

Conclusion

- A 2D model of HMT with MB is developed and models equations were solved using COMSOL for convection roasting process.
- Effect of WHC and shrinkage are incorporated.
- Better insight is obtained.

ACKNOWLEDGEMENT

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Thank you for your
attention!